

## MEMO

TO: Laura Woodbyrne
FROM: lan Crook

## SUBJECT: Draft High Level Review of Bridge Options

DATE: 14 February 2017

## High Level Review of Bridge Options

## Site Location and Local Geography

The proposed highway alignment crosses the River Goyt in an approximately north-south direction at approximate scheme chainage 3985 m .

The River Goyt is a Main River, with a channel width of approximately 25 m and an associated Level 3 Flood zone. The road surface level proposed as part of the Design Freeze 4A alignment is approximately 19 m above normal water level, and thus a bridge or viaduct structure will be required to cross the river.


Figure 1 - Goyt Valley Bridge - Design Freeze 4A Alignment


Figure 2-Aerial Image of Bridge/Viaduct Location


In order to minimise the impact on the river channel and associated flood plain, it assumed at this stage that the proposed highway will be supported on elevated structure over at least the plan area of the flood plain. In order to minimise the overall scale and cost of the structure, it is anticipated that a series of intermediate pier supports will be provided within the flood zone, the number and spacing of which will be driven by the selected structural form.

## Structural Forms

Based on the currently proposed alignment, an overall bridge structure length of 200 is anticipated across the River Goyt and associated floodplain.

The table below sets out initial high level options that have been considered, and the subsequent text considers the various issues in more detail:

## Table 1:

| OPTION | COMMENTARY | ADVANTAGES | DISADVANTAGES |
| :---: | :---: | :---: | :---: |
| Extended earth embankment with minimised structural span. | This solution would provide an earthworks solution running right up to the river channel, with a single span structure crossing the river with a span of approximately 26 m . <br> This solution would considerably reduce the cost of the overall Goyt Valley crossing; however the environmental impact of such a solution would be extensive. <br> Additionally, an embankment running across the floodplain would be wholly unacceptable from a hydrological perspective, with the potential for floodwaters to be retained upstream of the structure, exacerbating any localised flooding. <br> For the above reasons, this solution has been discounted and will not be considered further. | Low Cost. | - Significant adverse environmental impacts; <br> - Significant increase to flooding risk with additional land for flood capacity mitigation likely required. |
| Multi span viaduct structure. | A multi-span viaduct structure would consist of a series of discrete spans supported on intermediate piers or columns. <br> The span configuration and pier layout would require careful consideration at future design stages, but could consist of a series of regularly spaced viaduct spans, or a series of varying spans, for example with an increased span length over the river channel. <br> A multi-span viaduct offers a good compromise between addressing the various constraints of the site, whilst minimising cost. | - Minimised overall impact on flood risk in comparison with extended earth option; <br> - Reduced potential environmental impact in comparison with extended earth option; <br> - More readily accommodates the road curvature. | - Increased construction works in river valley, particularly for construction of foundations and piers; and <br> - Potential for adverse landscape, visual, ecological and potentially other environmental impacts with additional land for flood capacity mitigation likely required. |
| Single span structure. | A large single span structure across the Goyt Valley would minimise long term impacts on the river valley below. The elimination of intermediate piers would remove any potential obstruction to river flows, particularly in the flooded case, and would thus eliminate any concerns relating to scour. | - No impact on flood risk; <br> - Reduced long term | - Significant cost increase; <br> - Difficult to accommodate curvature of highway with a |

OPTION COMMENTARY ADVANTAGES

environmental impact on river valley in comparison with other two options;
A large single span structure also opens up the opportunity for inclusion of a more iconic or landmark structure within the scheme.
single span;

- Increased costs;
- Significantly more complex construction;
- Potential for an adverse landscape, visual, ecological and potentially other environmental impacts.


## Multi Span Viaduct Solution

A multi-span viaduct structure would consist of a series of discrete spans supported on intermediate piers or columns.

The span configuration and pier layout would require careful consideration at future design stages, but could consist of a series of regularly spaced viaduct spans, or a series of varying spans, for example with an increased span length over the river channel.

A variety of structural forms are available for a viaduct of this nature including steel composite box girders, steel composite ladder decks, and conventional beam and slab deck. All of these forms are commonly used on the UK highway network, and selection will depend on span lengths, which in turn will be driven by a variety of factors including aesthetics, constructability and pier positioning.

The following table sets out some of the key considerations for each of the main structural forms which might be considered, and lists advantages and disadvantages of each form:

| STRUCTURAL OPTION | FEATURES | ADVANTAGES | DISADVANTAGES | FURTHER CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Ladder Deck (Conventional) | Ladder deck bridge structures are one of the more common structural forms used in medium span structures. <br> The ladder deck form typically comprises two longitudinal main girders, cross girders and an in-situ reinforced concrete deck acting compositely steel grillage beneath. <br> For the purposes of the River Goyt crossing, with a dual 2 lane all-purpose (D2AP) carriageway and an overall structure width of approximately 28 m , two ladder deck arrangements would be required running side by side. The option exists to run the in-situ reinforced concrete slab continuously across both ladder decks, or altematively provide a longitudinal joint between the two. <br> Supports are typically provided beneath the main longitudinal girders, so in this scenario 4no. supports would be required at each pier location (to accommodate 2no. parallel deck arrangements). | - Efficient structural form, particularly for spans upwards of 35 m ; <br> - Can readily accommodate the proposed highway radius ( 1020 m ); <br> - The various spans can be made continuous, thus improving structural efficiency and allowing the superstructure to be installed using the incrementally launched method. | - Supports required beneath each main girder, potentially leading to a 'forest of columns' visual effect; <br> - Long term maintenance of steelwork (although all superstructure options are likely to involve steel); <br> - Reduced structural redundancy compared with multi-girder structures (although superstructure collision very unlikely over the river valley). | - Girders can be fabricated curved or faceted to accommodate the required curvature. Modern fabrication methods can accommodate curved sections with relative ease, and curved girders can more readily be installed using the incremental launching method. A constant curvature of viaduct is preferred for launching, which is achievable with the highway alignment as it currently stands; <br> - In terms of constructability, the site of the proposed structure is relatively remote, with little in the way of road access. On this basis, and given the environmental sensitivity of the area, it is assumed that construction access will be along the route corridor. This scenario lends itself well to providing a structurally continuous superstructure, and incrementally launching the structure from one end of the viaduct. Launching has the benefit of minimising construction operations at ground level, however attracts significant additional complexity at the design phase, as numerous additional load scenarios must be considered; <br> - Girders could be lifted from the valley floor. Crane positions, and lift weights, would need to be considered in conjunction with the relatively steep approach slopes to the site; <br> - Haunched girders (curved soffit in elevation) could be utilised to both improve structural efficiency and enhance aesthetics. Haunched girders are however very difficult to install using the incrementally launched method, thus a decision to utilise haunched girders would most likely result in significant haulage and craneage requirements within the river valley during construction; <br> - On multi-span continuous structures, uplift of ends spans must be considered, and it is usual to limit end spans to $70-80 \%$ of the adjacent intemal span. End span uplift should be considered in detail during preliminary design exercises. |
| Ladder Deck (Ladder Deck with Integral Cross Head) | This structural form is very similar to a conventional ladder deck, however pier supports are provided inboard of the main girders, with a transverse diaphragm providing a load path to the main girders. <br> The key benefit of integral cross heads is that only a single pier support is required beneath each ladder deck arrangement, hence for the two side by decks required for this scenario, only two supports are required at each pier position. | Advantages similar to a conventional ladder deck with the exceptions: <br> - The number of pier supports beneath the viaduct is halved, reducing | Disadvantages similar to a conventional ladder deck with the exceptions: <br> - A ladder deck with integral pier supports cannot be installed using the incrementally launched method, so installation | Further considerations similar to a conventional ladder deck with the exceptions: <br> - Given that a ladder deck with integral cross heads cannot be installed using the launching method, construction impacts within the river valley are significantly increased, and future |


|  |  |  |
| :--- | :--- | :--- |
| Steel composite box girders structures typically comprise one or more steel box <br> girders | Steen <br> sections, with a reinforced concrete deck slab acting compositely with the steel. |  |

substructure construction
progra
of the steelwork over the river becomes much more onerous. programme and costs,
whilst simultaneously reducing the overall visual
impact. impact.

Significantly increased span range compared with adder decks or slab decks, allowing more flexibility in pier positioning and a potential reduction in pier supports overall

- Box girders can be trapezoidal (with inclined vertical webs), which, when combined a deck cantilever at the structure impression of a more slender structure;
Can readily accommodate the proposed highway radius ( 1020 m );
The various spans can be made coninuous, efficiency and allowing the superstructure to be installed using the incrementally launched method.

Less structurally efficient in the medium span range, resulting in medium span range, resulting overall increased costs
fabrication/construction difficulties;

- Limitations on deck cantilevers Limitations on deck cantilevers
mean that at least 4 no. box girders would likely be required to support the 28 m wide carriageway;
Increased difficulty in long term inspection and maintenance (confined space access to box girders etc).
design stages would need to consider in detail how access to the river valley for haulage and craneage would be achieved.

In terms of constructability, the site of the proposed structure is relatively remote, with and given the environmental sensitivity of the area, it is assumed that construction access will be along the route corridor. This scenario lends itself well to providing a structurally continuous superstructure, and incrementally launching the structure from one end of
viaduct. Launching has the benefit of viaduct. Launching has the benefit of level, however attracts significant additional complexity at the design phase, as numerous additional load scenarios must be considered;

- Haunched box sections (curved soffit in elevation) could be utilised to both improve
structural efficiency and enhance aesthetics. Haunched box sections are however very difficult to install using the incrementally launched method, thus a decision to utilise haunched sections would most likely result in significant haulage and craneage construction;
- On multi-span continuous structures, uplift of ends spans must be considered, and it is usual to limit end spans to $70-80 \%$ of the
adjacent intemal span. End span uplift should be considered in detail during preliminary design exercises
- Multi beam structures typically comprise even numbers of beams to facilitate lifting in brace pairs. Any multi-beam proposal is therefore regardless of construction methodologies or other considerations;
- For a launched structure, significant bracing For a launched structure, significant bracing
(in addition to that required for a crane erecte (in addition to that required for a crane erecte
structure) would be required to provide both structure) would be required to provide both
global sway stability and local buckling stability during the various design cases for the launch;
On multi-span continuous structures, uplift of ends spans must be considered, and it is usual to limit end spans to $70-80 \%$ of the adjacent intemal span. End span uplift should
- 

| Pre-stressed beam and slab deck | A pre-stressed beam and slab deck comprises a number of pre-stressed pre-cast beams, acting compositely with an in-situ deck slab. | - Very common structural solution with reduced design complexity; <br> - Low maintenance (although see disadvantage relating to mechanical bearings); | - Increased construction depth compared with steel/concrete composite solutions; <br> - Available span lengths reduced compared with steel composite solutions, thus requiring greater number of intermediate supports; <br> - Potential heavy appearance of the viaduct; <br> - Cannot be delivered to site in shorter lengths and spliced; <br> - Significant design/construction complexity added if structure is made continuous across supports; <br> - Mechanical bearings required if structure is made continuous across piers; | - For long term durability reasons, a continuous structure across the pier supports is likely to be a client requirement; |
| :---: | :---: | :---: | :---: | :---: |
| Post-tensioned concrete box girders | A post-tensioned box structure would typically comprise 2 or more post-tensioned boxes with deck cantilevers and an in-situ joint between units. | - Potentially more economic if longer span lengths selected; <br> - Low maintenance; | - Significant additional cost compared with other options; <br> - Significant additional construction complexity compared with other options; | - Box sections can be either pre-cast or cast insitu; <br> - For spans of up to 60 m , it is common for concrete to be cast in sections span by span supported by falsework from the ground or with a truss spanning between the piers; <br> - Where the bridge alignment is straight or on a constant radius curve, launched single cell box girders may be used to overcome access problems or to avoid obstructions at ground level. Commonly used for spans of up to 60 m , the technique has been used for longer spans of up to 100 m with help of temporary piers placed to reduce the effective span during launching. Launching, however, creates further complexities of design and construction during generation of many intermediate stages; <br> - Precast concrete segmental box girders are found to be very economical for long bridge lengths due to the savings associated with maximising repetition in factory conditions. They allow rapid construction with minimum on site work. They do have disadvantages including the costs of setting up the casting yard and the special erection equipment needed. Span lengths vary typically up to |

## High Level Structural Alternative

As an alternative to the current highway alignment over the Goyt valley (Design Freeze 4A), an alternative alignment could be considered which places the highway alignment at a higher vertical level.

Under the present alignment (Design Freeze 4A), extensive cuttings are required on both approaches to the river crossing. A higher alignment would reduce magnitude of these cuttings, thus reducing the overall impact on the surrounding landscape and reducing land take for the scheme.

The trade-off for such an amendment is an increase in overall viaduct length across the river valley, although as no design alignment for such an option is available at this stage, it is not possible to provide an exact overall structure length.

Two principal options exist for such a high level structure:

1. Span the valley with a large single span, or a small number of spans;
2. Span the valley with a series of shorter spans, with supports provided to the valley floor.

## Option 1:

Structural solutions exist for even the largest potential span lengths across the Goyt Valley. For example, steel arch solutions exist for spans in excess of 500 m , and a cable stayed structure could comfortably achieve the required span lengths (although a large tower would need to be constructed).

The construction of a large scale structure across the Goyt valley would require considerable temporary support and staging from the valley floor beneath, and the complexity plus localised impact of the construction works would be significantly greater than other options. The cost of such a structure, both in terms of capital costs and whole life maintenance cost would also be significantly higher than other solutions.

It is considered unlikely that a very large scale structure would be visually appropriate within this setting, and this, combined with the overall cost of such a structure makes it unlikely to be an appropriate choice.

Option 2:
As an alternative to the option for a large scale structure as discussed above, a structure with a series of shorter spans could be considered.

Although higher in elevation than the structural forms considered for the Design Freeze 4A alignment, and with commensurately taller piers, a structural solution for such an alignment could be developed along much the same lines as the solutions considered Design Freeze 4A above.

The higher level structure, combined with the relatively difficult access across the river valley, would lend itself well to the incrementally launched method. The various considerations highlighted within Table 2 above relating to launching of the structure would also be applicable to this site.

PARSONS BRINCKERHOFF

In developing any highway alignment for a high level alignment across the Goyt Valley, attention should be paid to maintaining a constant horizontal and vertical curvature as far as possible, in order to accommodate any subsequent launching proposals.

## Foundations

In the absence of detailed geotechnical information, and given the sensitivity of multi-span continuous structures to differential settlement, it is assumed at this stage that foundations will be piled to an appropriate depth (or bedrock).

## Constructability

In general terms, construction of a four lane highway bridge across the Goyt Valley whilst minimising environmental impacts on the valley below will present a considerable challenge.

A large span structure at this location would generate significant construction complexities, which would inevitably require extensive temporary support and haulage routes to the river valley below.

In order to minimise localised environmental impacts during the construction phase, it is assumed that construction access would generally be made along the route corridor. The relatively steep slopes of the Goyt Valley at this location do not lend themselves to large haulage movements (for example large craneage equipment or delivery of bridge beams), and for this reason a construction sequence based around incremental launching of the bridge girders has been considered against each structural option. The use of the proposed alignment as a haul road for construction, would minimise disruption to the surrounding highway network, however careful programming and co-ordination with adjacent construction activities will be required.

Notwithstanding the above, a structure with smaller spans would require a series of intermediate pier or column supports across the river valley, which in itself would require construction access. It is likely then, that as the design develops, a pier solution will be adopted which minimises the requirement for large pre-cast or pre-fabricated structural elements, relying instead in in-situ methods.

Other aspects of constructability specific to the structural solutions considered are discussed within Table 2.

## Maintenance

In the permanent case, access to the underside of the structure for inspection and maintenance using a ground based MEWP could not easily be made, due to the relatively steep sides of the valley and the mature woodland covering each bank.

Permanent access gantries are employed on some large structures to facilitate ready access; however these structures in themselves require ongoing inspection and maintenance. Furthermore, a multi-span solution would require an access gantry to be provided beneath each span, further increasing the installation and ongoing maintenance costs. For these reasons, it is anticipated that permanent access gantries would not be employed.

Underbridge inspection units are becoming increasingly popular for access to the underside of viaduct structures, and consist of a mobile temporary gantry which extends beneath the

PARSONS BRINCKERHOFF
structure, mounted on a purpose built vehicle situated in the nearside lane or hard shoulder. As the design progresses, a number of factors should be considered in order to facilitate future use of underbridge inspection units:

- Avoid placing lighting columns on the outer stringcourse of the structure (otherwise an underbridge unit would need to be re-deployed between each pair of lighting columns);
- Minimise the depth of main girders, as excessively deep main girders can prevent touching distance access to the bridge soffit from underbridge units;
- Avoid closely spaced piers/columns/abutments along the span, as a minimum working length is required for an underbridge gantry to rotate into position beneath;
- Maintain a clearance envelope around the structure into which trees and other vegetation are not permitted to infringe.

In addition to specific considerations for underbridge units, the following more general considerations should be made with regards to inspection and maintenance access:

- Provide a hardstanding area around the base of each pier/column/abutment to facilitate future erection of scaffolding (for inspection, bearing replacement etc.);
- Provide jacking stiffeners and jacking points to substructures to facilitate future bearing replacement;
- Consider provision of permanent anchors to substructures to facilitate inspection via roped access;
- Design loading and fixing considerations for future scaffold and painting enclosures.


## Materials

The primary construction materials for the proposed structure are likely to be high yield structural steel and reinforced concrete.

The combination of steel and concrete for the superstructure would provide a highly efficient structural solution, and concrete substructures provide an efficient and geometrically flexible solution whilst minimising long term maintenance.

For superstructures constructed from structural steelwork, it is typically possibly to split the beam lengths into smaller lengths and to then splice the steelwork elements together on site using bolted splices prior to erection, in order to reduce the steelwork lengths and weights for transportation.

Concrete substructures also afford the opportunity for bespoke 'feature' finishes, which could be explored at future design stages as part of ongoing stakeholder consultation. Carefully designed feature finishes can also inhibit the proliferation of graffiti.

A key consideration during material selection is corrosion protection to any structural steelwork. Modern paint systems can provide up to 25 years of protection before the first major maintenance (re-application), however the this does not account for any localised mechanical damage to the system (impact during inspection activities etc.). Re-application of the paint system to a structure in this location will inevitably incur major cost and

PARSONS BRINCKERHOFF
disruption, however the choice of colour associated with a paint system can be a benefit in terms of aesthetic impact and stakeholder objection.

An alternative to a conventionally painted structure exists in Weathering Steel. Weathering steel is a high strength low alloy steel which has the ability to form a protective rust patina that inhibits further corrosion. Weathering steel is becoming an increasingly popular choice for steel structures for difficult access, as future maintenance associated with paint coatings is eliminated. Weathered steel structures exhibit a 'rusty' appearance, which darkens in colour with time to achieve a dark brown appearance.

Weathering steel, if selected would require very careful detailing to ensure water run-off from the steelwork does not lead to staining of reinforced concrete substructures. BD 7/01 Weathering Steel for Highway Structures provides further guidance on the use of weathering steel.

## Cross Sections and Headrooms

The cross section of the Goyt Valley Bridge should be developed in line with the requirements of TD27/05 Cross-Sections and Headrooms. In practice, the proposed highway alignment is at least 18 m above the River Goyt, so even accounting for relatively large construction depths, the headroom constraints above the river are unlikely to be a limiting factor.

To the north side of the river, the proposed alignment crosses an existing access track (Dark Lane). The proposed highway alignment at this location sits 8.7 m above the existing track surface, so again, even for relatively large construction depths, appropriate headroom is achievable. The available headroom at this location should be monitored as the design develops to ensure required headrooms are maintained.

## Design Standards

As a member of the European Union, the UK is required to comply with the Construction Products Directive (CPD) and the Public Procurement Directive (PPD), which mandate the use of European Standards in member states.

Any structural design undertaken as part of a publicly funded scheme should therefore be undertaken in accordance with the suite of structural Eurocodes.

In addition the above, HE (formerly HA) Interim Advice Note 124/11 (IAN 124/11) provides guidance and requirements for the use of Eurocodes for the design of highway structures on the strategic road network.

## Safety

With regards to safe design, the following general points applicable to the whole scheme are noted:

- Structures should be safe by design, from construction, through maintenance to eventual demolition;
- The principle of prevention to eliminate, reduce and control risks in accordance with the CDM Regulations 2015 should be adopted (and is a legal requirement); and
- The safe construction and maintenance of the individual elements of a structure varies greatly by span arrangement, material and form. The individual impacts
associated with any design option choice need to be considered in relation to the overarching construction strategy and programme for the scheme.

Author's Name - Ian Crook<br>Author's Title/Role - Associate (Bridges)



PEDESTRIAN AND CYCLE PROVISION REVIEW

## SEMMMS A6-M60 RELIEF ROAD: STAGE 2 STUDY

## REVIEW OF PEDESTRIAN AND CYCLE PROVISIONS DRAFT

TECHNICAL NOTE NO 002: MARCH 2017

QUALITY MANAGEMENT

| Job Number | Date | Author | Checked | Authorised |
| :--- | :--- | :--- | :--- | :--- |
| 70019764 | March 2017 | Mark Hetherington | Laura Woodbyrne | Stuart Atkin |

## 1.1

1.1.1 The development of Stockport Metropolitan Borough Council's cycle network is focused upon appropriately managing existing highway, right-of-way, permissive routes and creating new links within the existing network.
1.1.2 The A6 to M60 Relief Road Scheme will provide 8.5 km of new 2-lane 50 mph dual carriageway on a north - south route from the M60 Junction 25 at Bredbury (north east of Stockport) to the A6 near Hazel Grove (south east Stockport). It will also provide a link road to Stepping Hill of 1.1 km allowing improved access to Stepping Hill Hospital.
1.1.3 The initial scheme design was undertaken in 2003 since then the popularity of cycling/walking has increased, therefore the standards have changed and design will need to adhere to the latest TfGM - Stockport cycling guidelines.
1.1.4 The proposed scheme will allow road traffic to bypass the heavily congested routes to the M60 that presently pass through Hazel Grove, Stockport town centre, Offerton and Bredbury in both directions also bypassing local districts and centres. It will provide much needed connectivity for key strategic routes into the North, the North West, and the wider Greater Manchester conurbation and specifically to Manchester Airport; including traffic from the A6, A523 and A34 - all of which are key routes for business, leisure travel and freight.

PARSONS BRINCKERHOFF

## SEMMMS A6-M60 RELIEF ROAD: STAGE 2 STUDY

## REVIEW OF PEDESTRIAN AND CYCLE PROVISIONS DRAFT

TECHNICAL NOTE NO 002: MARCH 2017

## 1.2

1.2.1 A review of the provisions put forward in the current version of the design for pedestrian and cyclists is provided below. The design is subject to development at later stages in the scheme, therefore the provisions may be amended, developed or the detail changed from that discussed below. A plan indicating associated locations of the provisions is also shown in figure 1. An overview plan showing the locations at which pedestrian and cycle provisions are present is shown in Drawing no. A6-M60-WSP:PB-1-ZZ-DR-J-0003. Cross sections at some key points incorporating the shared cycleway/footways are shown in Drawing nos. A6-M60-WSP:PB-1-ZZ-DR-J-0004 to 0007.
A. The start of the route from Stockport Road West above the tunnel provides a 460 m long 3 m wide shared use facility along the alignment of the new road however adjacent routes are 2 m wide with a cycle lane on the carriageway of Stockport Road West. Design refinement will be required to detail how cyclists travelling north to Ashton Road will cross the road to enter the cycle lane safely and how cyclists travelling north and turning left on to Stockport Road West will access the cycle lane with minimal conflict with pedestrians.
B. Where the route crosses Osborne Street/Kingsway, consideration to the crossing type will be required as the current proposed crossing appears to be uncontrolled with a refuge island in the centre of the carriageway. Also, no provision has been detailed for cyclists turning onto Osborne Street/Kingsway as the footways are 2 m wide on both sides of the road and no cycle lane markings are shown on the carriageway.
C. The route along the alignment of the proposed road from the end of the tunnel to the junction for Marple Road provides a 2.3 km long 3 m wide shared use facility with a 2 m verge between the carriageway and footway/cycleway. This excludes the section over the proposed Goyt Valley Bridge where the footway/cycleway is adjacent to the carriageway with a 1 m wide hard strip only.

On Marple Road Bridge the northbound approach for the footway/cycleway is 3 m wide turning left onto Marple Road, this narrows to 2.2 m wide with a cycle lane provided on the carriageway. A detailed proposal will be required for how cyclists will join the carriageway safely at this location.

There is a bus stop located near the junction for Marple Road, where the footway/cycleway is 5 m wide allowing for a shelter to be installed and providing the acceptable minimum width for cyclists to pass.

## SEMMMS A6-M60 RELIEF ROAD: STAGE 2 STUDY

## REVIEW OF PEDESTRIAN AND CYCLE PROVISIONS DRAFT

TECHNICAL NOTE NO 002: MARCH 2017
D. There is a bus stop proposed just north of the new junction for the Stepping Hill Link with a footway width of 5 m then narrowing to 2 m at the end of the lay-by. The 2 m wide part of footway is 41 m long but it is currently unclear if it is access for maintenance or whether it is superfluous. Stepping Hill link has a 3m wide footway/cycleway provision along the route adjacent to the junction for the supermarket car park, the footway narrows to 1.8 m with a 1.5 wide verge. If the verge was removed, the 3 m width for the shared use footway/cycleway could be maintained up to the junction.
E. On Offerton Road, the shared use footway/cycleway switches from the north side of the proposed A6 M60 road to the south side with access via a bridge with 3 m wide shared use footway/cycleway.
F. The access from the proposed A6 M60 road to the Golf course access road is assumed to be for maintenance/inspections of structure only and not for general use.

The A6 MARR roundabout provides a shared pedestrian/cycle route across the western arm with the 3 m wide shared route continuing along the A6 MARR road. The crossings in the current version of the design are shown as 3 m wide.

The northern footway on the western arm of the A6 roundabout provides a 3 m wide shared route for 300 m where it then reduces to 2 m wide, there is no provision provided on the southern side of the A6.

The current design does not show any pedestrian/cycle provisions along the eastern arm of the roundabout.

The pedestrian/cycle route on the western side of the A6 MARR road provides a 3 m wide footway/cycleway for 205m from the crossing point at the roundabout, where it then widens to 5 m adjacent to the layby of the A6 MARR road. The pedestrian/cycle provision south of the layby is 2.5 m wide.

There is no continuous footway/cycleway provision provided on the eastern side of the A6 MARR road. There is a 2 m wide footpath leading to a 90 m long footway on the eastern side of the A6 MARR road however this does not connect to any other footway on the A6 MARR road.

Figure 1-1 Plan indicating associated locations of provisions - A6 - M60 Relief Road

## SEMMMS A6-M60 RELIEF ROAD: STAGE 2 STUDY

## REVIEW OF PEDESTRIAN AND CYCLE PROVISIONS DRAFT

## TECHNICAL NOTE NO 002: MARCH 2017



## SEMMMS A6-M60 RELIEF ROAD: STAGE 2 STUDY

## REVIEW OF PEDESTRIAN AND CYCLE PROVISIONS DRAFT

## TECHNICAL NOTE NO 002: MARCH 2017

1.3.1 The majority of adjacent paths to the main A6 M60 relief road are 2 m wide which is the acceptable minimum for off-carriageway route (TA90/05 para. 7.16). The main alignment provides a width of 3 m which is the preferred width of a shared facility. A review of the cycle flow should be undertaken to determine if the 2 m widths of the side routes is sufficient for the number of users.
1.3.2 Alignment; Assumed design speed lower than 30kph therefore transitions from one width to another should have a taper of $1: 5$ (TD90/05 para. 7.9). The minimum radius for 10 kph design speed is 4 m ; the minimum radius used in the proposed design is 6 m .
1.3.3 Crossing widths are 3 m wide at all junctions. The ideal for toucan crossings is 4 m as stated in LTN2/95. LTN2/95 also states that 3 m wide crossing widths have been used, however a review of the pedestrian and cycle flow should determine the width proposed in this scheme.


A6 TO M60 LOCAL MODEL VALIDATION REPORT

## Client A6 to M60 Client Board

## Project A6 to M60 Relief Road

Subject HFAS Report 1907: A6 to M60 Local Model Validation Report
This Report describes the production and validation of the 2015 A6 M 60 M odel. The model validation follows guidelines in Webtag Unit M3-1 Highway Assignment Modelling issued by the Department for Transport (DfT).

The Report describes the development of the highway networks and trip matrices, and presents the results of the link flow and journey time validation.


Transport for Greater M anchester Highways Forecasting and Analytical Services have prepared this document for the titled project or named part thereof. It should not be used or relied upon for any other purpose without prior written authority from TfGM HFAS and without an independent check of its suitability. TfGM HFAS accepts no responsibility or liability for the consequence of using this document for a purpose other than for which it was commissioned.

## CONTENTS

Page

1. Introduction ..... 4
The Report ..... 4
A6 M 60 Scheme Background ..... 4
The Original A6 M60 Relief Road Scheme ..... 5
A6 M 60 Strategy Objectives ..... 6
Specific objectives for the A6 to M anchester Airport Relief Road scheme ..... 7
Description of New Relief Road ..... 8
2. Modelling Background ..... 10
Overview ..... 10
A6 M 60 SATURN M odel ..... 10
Highway Networks ..... 10
Trip M atrices ..... 11
3. The A6 M60 SATURN M odel Zoning ..... 12
Background to Model Zoning ..... 12
Derivation of A6 M 60 SATURN M odel Zoning ..... 12
4. A6 M 60 SATURN Network Development ..... 16
Overview ..... 16
Spigot and Zone Centroid Coding ..... 17
Area of Influence. ..... 17
Traffic Signal Data ..... 20
Checks and Adjustments to Networks ..... 21
Link Length Crow Fly Checks ..... 22
Bus Data ..... 22
Adjustments to Link Cruise Speeds ..... 22
M otorway Flow Delay Curves ..... 23
Times in the External Network. ..... 24
Generalised Cost Parameters ..... 24
Netw ork Statistics ..... 26
5. Development of the Prior $M$ atrices ..... 27
Overview ..... 27
6. M atrix Estimation ..... 47
Introduction ..... 47
Traffic Count Data ..... 47
Count Checks ..... 48
Cordons and Screenlines ..... 48
Point Zone Counts ..... 49
M anchester Airport Car Park Counts ..... 49
M atrix Estimation Results ..... 51
7. Traffic Flow Validation ..... 67
Introduction ..... 67
Network Convergence ..... 67
Assignment Validation Guidelines ..... 68
GEH Statistic ..... 68
Link Flow Comparisons for M atrix Estimation Counts. ..... 69
M atrix Estimation Cordons and Screenlines ..... 69
Link Flow Comparisons for Independent Counts ..... 76
Independent Screenline North of M 60 ..... 76
All Independent Counts ..... 76
Regression Analysis ..... 77
8. Journey Time Validation ..... 81
Introduction ..... 81
Journey Time Validation Guidelines ..... 81
AM Peak Hour Journey Time Validation Results. ..... 84
Inter-Peak Hour Journey Time Validation Results ..... 86
PM Peak Hour Journey Time Validation Results. ..... 88
Commentary on Journey Time Outliers ..... 90
Commentary on Journey Time Outliers Error! Bookmark not defined.
Conclusions of Journey Time Validation ..... 91
9. Conclusions ..... 92
10. References ..... 93
Appendix 1 Example Calculation of Generalised Cost ..... 94
Appendix 2 Prior and Estimated Matrix Comparisons by Sector ..... 99
Appendix 3 - Journey time Graphs ..... 103

## 1. Introduction

## The Report

1.1 This report describes the development of the 2015 A6 to M 60 SATURN model and presents the results of the link flow and journey time validation using the criteria set out in Webtag Unit M 3.1).
1.2 The report has nine main sections:

Section 1- Introduction and scheme background
Section 2-M Model background
Section 3- Model zoning
Section 4 - Development of the 2015 (model) highway networks
Section 5- Production of the prior trip matrices
Section 6- Matrix estimation to enhance prior matrices and improve the fit between modelled and observed flows

Section 7- Traffic flow validation results
Section 8 - Journey time validation results
Section 9- Conclusions.
1.3 Further details of the validation are contained in the Appendices, including prior and estimated matrix compariso ns by sector, and link flow validation results by vehicle type.

## A6 M60 Scheme Background

1.4 The Government Transport Policy review in the late 1990s included consideration of the trunk road building programme; culminating in the "New Deal for Trunk Roads in England" report. The report recommended that the trunk road network, which is the responsibility of the Highways Agency (HA), should be greatly reduced. In the south east Greater Manchester, the A6 and A523 were recommended for de-trunking.
1.5 The "New Deal" also recommended that future road schemes associated with detrunked routes be withdrawn from the road building programme, as they were no longer a HA responsibility. In south east Greater M anchester (GM ) such schemes were:

- A6 (M) Stockport North-South Bypass (including the Stepping Hill Link)
- A523 / A555 Poynton Bypass
- A555 M anchester Airport Eastern Link Road (MAELR)
- A555 M anchester Airport Link Road West (M ALRW).
1.6 The schemes have been identified in plans dating to the 1930's and various residential and employment developments in the area have been predicated on their delivery. All three corridors are protected in respective local authority strategic plans. Progress included agreed preferred routes and, following a Public Inquiry in 1988, appropriate procedures for the A6 (M).
1.7 The central section of the A555 MAELR was constructed as part of a local authority A34 bypass scheme, with HA and developer contributions, and assuming that the remaining route would be built shortly afterwards; the HA having presented strong supporting evidence.
1.8 The final relevant recommendation of the New Deal was that a multi modal study should be conducted across south east $M$ anchester to consider existing transport problems and develop a long-term (20-year) strategy for addressing them; the South East M anchester Multi Modal Study (A6 M60) was commissioned and managed by the Government Office for the North West (GONW), which created a Steering Group (including relevant local authorities and transport organisations) and a wider reference group (to reflect local interests). Consultants were appointed to undertake the study, which began in January 2000 and completed in September 2001 when a final report, including a recommended strategy, was published.
1.9 Within multimodal study process, the package of recommendations was assessed using the GOM M MS methodology and the potential options were assessed against the Strategy objectives before recommendations were made. The local authorities, AGMA, the North West Regional Bodies and the Government, supported the strategy. A number of public consultations were also held during the process, to identify issues. A final consultation on the proposed strategy showed it had strong public support


## The Original A6 M 60 Relief Road Scheme

1.10 The wider A6 M 60 strategy included the concept for a Relief Road, comprising 21.5 kilometres of new road from M 60 Junction 25 to M 56 Junction 5, of dual carriageway standard and with two single carriageway link roads - the Stepping Hill Link and Poynton Bypass. The central 3.9 kilometres of the A6 M 60 relief road has already been constructed as part of the A555 and A34 bypass scheme.
1.11 Three local authorities, Stockport, M anchester City Council and Cheshire (now Cheshire East) jointly produced a Major Scheme Business Case bid for funding the A6 M60 New Relief Road, which was formally submitted to the DfT in July 2004. Over the next few years, further information was submitted to the DfT, including an investigation into the possibility of Private Finance Initiative (PFI) funding.
1.12 In July 2007 the DfT's considered response stated that the Relief Road scheme provided value for money, but limited funding capabilities meant it could not funded as a single scheme, so consideration should be given to phased delivery. Three potential phases of the scheme were identified by the local authorities, and were submitted to the DfT for consideration in 2007/ 08:

- M60 to the A6, including the Stepping Hill Link
- $\quad$ A6 to $M$ anchester Airport with Poynton Bypass
- A6 to Manchester Airport without Poynton Bypass (A6 M60 A6 to Manchester Airport Relief Road).
1.13 Local Authority officers examined the key policy drivers and transport problems in the area and decided that the A6 to Manchester Airport section was the priority scheme due to the potential economic impact on Manchester Airport (and therefore the City Region) of delaying access improvements, which in turn could constrain future growth.
1.14 Following the Eddington (Access to International Gateways) study, which highlighted transport's pivotal role in supporting the future economic success of the UK, reforms of the planning, funding and delivery of transport interventions were recommended. The study recognised the need to maximise sustainable returns from investment, whilst improving the environmental performance of transport.
1.15 Eddington also recognised the importance of connecting inter-regional routes as part of the network. This role is played by the A6, A523 and A34, linking Greater M anchester with Cheshire, Derbyshire and Staffordshire. Eddington considered a number of road schemes including the A6 M60 Relief Road and recognised that it provided good value for money. Application of the Eddington criterion for Benefit Cost Ratios (BCR) raised the A6 M 60 Relief Road BCR slightly to 5.6.


## A6 M60 Strategy Objectives

1.16 The A6 M60 strategy was developed and accepted in 2000/01. The original strategy was developed on a 20-year timescale to deal with the existing and predicted transport problems in the area.
1.17 Five core objectives were adopted in the strategy:

- The promotion of environmentally sustainable economic growth;
- The promotion of urban regeneration;
- The improvement of amenity, safety, and health;
- The enhancement of the regional centre, town centres and local and village centres and the Airport; and
- The encouragement of the community and cultural life of the neighbourhood and of social inclusion.
1.18 The five core objectives have clear linkages to transport issues that were identified within a series of defined sub-objectives. These were broken down into five priority themes:
- Improvements to public transport to promote sustainable economic growth, the improvement of neighbourhood community and cultural life, and the encouragement of social inclusion;
- Making better use of existing road space through the reallocation among transport users, to form part of the broader promotion of urban regeneration and improved amenity, safety and health;
- The encouragement and facilitation of behavioural change to enable people to reassess their transport needs and promote sustainable modes of transport. This element of the strategy had a wide-ranging focus, looking beyond immediate transport issues to examine the needs of schools and businesses and helping them to understand how they could benefit from a change in travel mind-set.
- The promotion of urban regeneration, to improve the streetscape and public realm, and address the impacts
- The development of the package of complementary highway works, in particular the major highway schemes identified in the A6 M 60 strategy, was addressed fully in direct discussions between the DfT and the three authorities (Cheshire County Council, M anchester City Council, and Stockport Metropolitan Borough Council) charged by the Secretary of State with the development of the schemes. Other highway works included the longer-term objective of reducing the impacts of freight traffic on the A6 M 60 area, through appropriate freight route designation and the promotion of alternative modes (e.g. rail).


## Specific objectives for the A6 to Manchester Airport Relief Road scheme

1.19 Whilst transport policy has moved on since the A6 M60 strategy was developed, the underlying objectives and principles remain equally valid today as in 2001. The findings from Eddington and Stern strengthen the case as presented in the A6 M 60 strategy, with its emphasis on sustainable economic growth, regeneration of deprived areas, reduced environmental degradation, and general improved quality of life. Sustainable transport and behavioural change - both of which were integral to the A6 M60 strategy - are seen as key tools in addressing current transport challenges.
1.20 Nevertheless, there are changes required to ensure that the objectives remain directly relevant to the current policy goals; most notably, the need to take explicit account of carbon emissions, and emphasise the importance of M anchester Airport as an international gateway and potential hub of economic development and regeneration in its own right.
1.21 Whilst the objectives for A6 M60 A6 to Manchester Airport Relief Road have been primarily developed around the existing problems, it is important to note that the A6 to M60 scheme is considered an integral part of the overall SEMMMS strategy. Just as important is the demonstration that the objectives of the current scheme closely mirror those of the original A6 M60 Relief Road scheme. With these issues in mind, the A6 to Manchester Airport Relief Road Scheme objectives are set out below:

- Promote sustainable economic development through the provision of efficient surface access to, from and between Manchester Airport, the Airport Enterprise Zone and the local, town and district centres and employment sites
- Reduce the productivity losses to business, and provide an improved route for freight, by limiting the conflict between local and strategic traffic
- Reduce the impact of traffic congestion on local air and noise pollution
- Regenerate the local communities and encourage community, cultural and social inclusion through reduced severance and improved accessibility to, from and between key centres of economic and social activity


## Description of New Relief Road

1.22 The A6 to M60 Relief Road includes a new 2-lane dual carriageway connecting the A6 (at the end of the A6M ARR scheme) to the M60 at Bredbury with a spur to Stepping Hill Hospital The scheme bypasses Stockport Town Centre, Hazel Grove, Offerton and Bredbury.
1.23 Through the connection to the A6M ARR the scheme improves access to / from Manchester Airport and its employment areas as well as Hazel Grove, Newby Road, Bramhall Moor Lane, Poynton and Stanley Green employment areas. Access to a number of regeneration areas is also improved by the scheme, including Stockport Town Centre M60 Gatew ay, and Wythenshawe.
1.24 The proposed scheme consists of approximately 7.5 km of new dual 2-lane carriageway and will include two new junctions and amendments to junctions at the A6 and at the M60/A560 roundabout at Bredbury as well as a new junction with the A6 at Stepping Hill.
1.25 The location and extent of the scheme is shown in Figure 1.1.
1.26 The scheme has been designed to Department for Transport standards and adheres to the Design Manual for Roads and Bridges (DM RB). Any departures from approved standards will be authorised by the Director of the Overseeing Organisation.


Figure 1.1 Location of Proposed Scheme

## 2. Modelling Background Overview

2.1 The A6 M60 Relief Road SATURN model has been developed from the Greater Manchester SATURN M odel (GM-SATURN). The GM-SATURN model was validated to a base year of 2014 and updated to 2015 using counts post 2013 factored to an average October weekday in 2015.
2.2 Geographically, the A6 to M60 model is focussed on the area surrounding the proposed scheme namely Stockport, South Manchester (including Manchester Airport) and Cheshire East, (principally Wilmslow, Alderley Edge and Poynton) and an extension to cover the Bollington, New Mills, Disley and Whaley Bridge. It uses the GM-SATURN model area in full, but with the addition of a significant area of additional simulation network covering the northern part of Cheshire East. The model also incorporates a representation of the rest of Great Britain, albeit in less detail with increasing distance from the A6 M 60 area.
2.3 Separate versions of the A6 M 60 SATURN model have been built for the morning peak hour 08000900, the evening peak hour 1700-1800 and an average inter-peak hour for the time 09:30-16:00.

## A6 M60 SATURN M odel

2.4 The A6 M 60 SATURN model has two main components comprising:

- The highway networks, which represent the roads and junctions used by traffic and bus services
- The trip matrices, which represent the demand for travel and the flow of vehicles between the zones in the model.
2.5 There are, however, a number of subsidiary files associated with the model, including:
- A 'KNOBS' data file, which contains additional data items for network links, such as the road class and number and the locations of zebra crossings

A node-zone file, which is used for count-based validation, and gives details of the traffic zone in which each node lies

- A GIS file, used by SATURN to display links as curves rather than straight lines
- Inter-peak and PM peak 'X-files', to store supplementary link and turn data for the interpeak and PM peak networks
- Mapınfo node and link tables, to allow the network to be viewed in M apInfo.
2.6 Details of the highway networks and trip matrices are given below.


## Highway Networks

2.7 The highway networks used within the model represent all roads of traffic carrying significance within the area through which the proposed scheme will run - Stockport, South M anchester and the north of Cheshire East - and the remainder of Greater M anchester, including all motorways, A-roads and B-roads. The networks also include all of the yellow coloured roads on the Ordnance Survey's Landranger maps of the area, and all roads carrying known bus services. The network
outside the county is represented in much less detail, and becomes increasingly less dense with increasing distance from the county boundary.
2.8 The entire network within Greater M anchester and the northern part of Cheshire East and High Peak is coded in full SATURN simulation format, allowing the interaction of traffic at junctions and the resulting delays and queues to be accurately modelled. Outside of this area, the network is coded in SATURN buffer format, so that junction delays and queues are not explicitly modelled in this part of the netw ork.
2.9 The information required for the simulation coding is much more detailed than buffer coding and includes, for example, the link length and cruise speed, the permitted movements at junctions, saturation flows and lane usage (including locations of bus lanes), details of traffic signals and settings, including stages, cycle times, green splits, inter-greens and off-sets. Details of traffic signal settings are obtained from information supplied by the Greater M anchester Urban Traffic Control Unit (GMUTC).
2.10 Buses are represented in the model as fixed loads, with routes defined as chains of nodes in the simulation and buffer networks.

## Trip M atrices

2.11 The A6 M60 trip matrices contain representations of all vehicle trips with an origin or destination inside the A6 to M60 scheme area and the remainder of Greater M anchester, and all external-toexternal trips that cross the county boundary. The matrices do not, however, represent intrazonal trips that take place entirely within the same zone.
2.12 Separate matrices are maintained for car, Light Goods Vehicle (LGV) and Other Goods Vehicle (OGV) trips, for the morning peak hour (0800-0900), the evening peak hour (1700-1800) and an average inter-peak hour for the period 1000-1530.
2.13 For cars, matrices are available for 12 journey purposes (see Chapter 5 for details). For assignment purposes, however, the matrices are aggregated to form 5 'user classes', comprising:

- $\quad$ Commuting cars (home-to-work plus work-to-home car trips)
- Employer's business cars (home-based plus non-home-based employer's business car trips)
- $\quad$ Other cars (all other car trips)
- LGVS (all purpose LGV trips)
- OGVS (all purpose OGV trips).


## 3. The A6 M60 SATURN Model Zoning

## Background to M odel Zoning

3.1 The zoning system for the new A6 to M60 SATURN M odel had to fulfil several requirements.
3.2 Firstly, the zoning system for the whole modelling system was based on local authority areas and, within these, wards (as of 2001).
3.3 This was done to:

- Facilitate the compilation of input data, such as population and employment totals
- Provide a well-understood framework for summarising and reporting model outputs.
3.4 Secondly, there was a need to represent the actual origins and destinations of trips and traffic within the area surrounding the proposed scheme realistically and in detail. This was facilitated by developments in the demand modelling incorporated within the A6 M60 VDM that allowed more zones to be represented than in the "parent" GM-SATURN model. However, some caution was applied in defining zones to ensure that the usefulness of the model was not compromised by having so many zones that processing times became excessively long.
3.5 Finally, the focus of interest was the A6 to M 60 area, and the zoning is therefore most detailed within this. The zones in that area are therefore smaller than or of a similar size to those in the remainder of Greater Manchester. Elsew here, zone sizes increase with distance from the Greater $M$ anchester boundary.


## Derivation of A6 M60 SATURN M odel Zoning

3.6 The original GM -SATURN model contained 993 analysis zones of which 864 are within Greater M anchester. The original GM-SATURN model zoning is shown in Figure 3.1.
3.7 For the A6 M 60 SATURN model, zoning both within and outside the county was reviewed. Within Greater M anchester, GM-SATURN zones within Stockport, South M anchester and East Trafford were checked and existing zones were disaggregated to better represent key generators and future development sites.
3.8 The area surrounding $M$ anchester Airport was looked at in detail and the zoning in that area was reworked based on local knowledge and with reference to several documents. The latter included 'M anchester Airport Masterplan' (reference 2), 'M anchester Airport Ground Transport Plan' (reference 3) and Manchester Airport: The Need for Land' (reference 4). Together, these outline Manchester Airport's future development proposals and parking requirements in some detail.
3.9 Outside Greater Manchester, in the original GM-SATURN model the zones in Cheshire East were significantly larger than those within GM. As a certain proportion of Cheshire East is now coded in simulation detail and is in close proximity to the proposed A6 to M 60 scheme the zoning was reviewed and disaggregated.
3.10 In particular, the more built up areas around Wilmslow, Alderley Edge and Poynton required a more extensive rezoning to better reflect loading points on the network. As in Greater $M$ anchester all zones in Cheshire East nest within ward boundaries.
3.11 The additional zoning within the Area of Influence and Cheshire has resulted in an increase in the number of zones in the A6 to M 60 SATURN model to 1097 analysis zones. The revised zoning for the A 6 to M 60 SATURN model is shown in Figure 3.2.



## 4. A6 M60 SATURN Network Development

## Overview

4.1 Within the A6 to M60 SATURN model, the A6 to M60 Area of Influence (see paragraph 4.11 on) is represented at detailed node-based 'simulation' level; roads represented include motorways, A/B-roads, and other roads of traffic significance.
4.2 The information required for simulation coding is detailed; it includes the following items for each link / turn:

- Link length and cruising speed, usually taken as the speed limit
- Permitted movements, and the saturation flows and priorities for each movement
- Lane usage and lane sharing
- Flare lengths and stacking capacity
- Gap acceptance for opposed movements
- For traffic signals, the staging, timings and offsets
4.3 The starting point for the A6 to M60 networks were the 2014 GM-SATURN networks. These networks represent the whole of Greater $M$ anchester is in simulation detail. The simulation area was extended to include the northern part of Cheshire East and High Peak.
4.4 The coding for Cheshire East and High Peak within the A6 to M60 AOI was taken from work undertaken for A6 to Manchester Airport Relief Road and was added into the 2014 network in place of the previous buffer network. This extra simulation network broadly covers the area bounded by the GM Boundary to the north, the A523 to the east, the A537 to the south and the A34 to the west. HFAS review ed the coding supplied for this area using recent aerial photographs undertaken in site visits, and amended the coding as required.
4.5 The GM-SATURN networks for 2014 were further enhanced to include all local traffic management schemes that HFAS were aware of that might affect network capacity (and consequently the routing and travel times of vehicles). These schemes were identified using information from a variety of sources including:
- Changes reported by Districts and HFAS staff
- Local knowledge
- Aerial photographs
- Discrepancies between the modelled and actual road system highlighted by the counts and accident validation procedures.
4.6 Those roads outside the A6 to M60 area (and the remainder of Greater Manchester) are represented by an extensive link-based 'buffer' network that represents surrounding motorways, A-and B-class roads, but with density diminishing with distance. The buffer network is represented by links, rather than as a series of junctions, with capacity restraint being modelled using flow-delay curves.


## Spigot and Zone Centroid Coding

4.7 In accordance with best practice (to aid transparency of loading points), all zone centroids are connected to the model network via spigots. Spigots are links that join the centroid or centre of gravity of the zone to a node on the model network. In the case of point zones such as superstores accessed via a single junction, the spigot representation of a zone is realistic because the junction to which it connects exists and can therefore be coded as a simulation junction. However, in most cases, traffic for a zone joins / leaves the real network at many different points within the zone, and the centroid and spigot representation in the model is a simplification. In particular, the node to which it connects does not exist as a real junction.
4.8 Centroids for each zone were generated in HFAS's network information system (GM NIS) using Mapinfo; the software can identify the centre of gravity of a bounded area, e.g., a SATURN zone. Then, for zones where in practice the traffic joins / leaves the coded network at a number of different locations but where the model had to use a single access point, spigot nodes were created on the model network to attach the link (i.e., the spigot) to / from the centroid. This was done where needed, i.e., for all zones except point zones across the network.
4.9 Note that the spigot nodes are junctions in the model, but most of them are not junctions on the real network. To avoid modelling delays at such nodes, they were coded using a template that included additional lanes and maximum saturation flows for the turns into and out of the spigot with no priority markers. For point zones, however, where the spigot represents the site access road, the spigot node represents a real junction, and is coded appropriately.

## Area of Influence

4.10 The A6 to M60 model covers all of Greater Manchester and the northern part of Cheshire East and, in progressively decreasing level of network and zone detail, the remainder of the mainland UK. The A6 to M60 scheme in its current form on the section between M56 (at the airport) and A6 (at Hazel Grove) is intended to have relatively local influence, and is being designed as such.
4.11 The A6 to M60 modelling team set out to identify an 'Area of Influence' (AOI) for the scheme. Although checks will be made of wider model validation, the AOI will define the area over which detailed checks will be carried out to ensure that it represents traffic patterns and volumes within the area well. In particular, we will focus attention on aspects such as network coding and network density, explicit representation of significant traffic generators, and compliance to DfT criteria (including base assignment validation) within the AOI.
4.12 The AOI was initially identified using a 2032 forecast year based on the modelling undertaken for A6M ARR, comparing assignments with and without the scheme added to identify significant flow changes. Although work to identify an AOI is typically carried out using a base year model, future year forecasts from the A6 M60 work were available in this case, allowing us to assess the AOI with the higher level of traffic that will be present in later years.
4.13 We used two measures to identify the AOI of the scheme:

- traffic flow changes equivalent to a GEH value of 5.0 or greater, which mirrors the Department for Transport criteria for flow validation, where a comparison of two flows that generates a GEH value of 5.0 or greater is considered to represent a significant flow difference
- Absolute flow changes; changes were analysed in steps of 50 pcus from 100 to 250 pcus).
4.14 The results of the analyses undertaken were examined by the modelling team and it was agreed that the AOI would be defined based on flow changes of +-250 pcus and a GEH of 5.0 , which is consistent with the criteria used to define the AOI for the A6 M60 scheme. The resulting definition of the AOI was adjusted to follow highway model zone boundaries. In all cases, the AOI was extended outwards where identified impacts only extended a small distance into a zone to ensure that the resulting area fully encompasses the likely impacts of the scheme.
4.15 Two key points to note about how the AOI will be reflected in the model development and forecasting are:
4.16 For the purposes of model validation, we will use the full model as this will enable us to include screenlines and cordons across Greater M anchester to monitor the wider validation of the model and ensure that the patterns and volumes of traffic entering the AOI are realistic.
4.17 For forecasting, the model will be cordoned both to speed up model runtimes and to exclude the impacts of assignment 'noise' in areas of the model remote from the scheme that could adversely affect the reliability of results from the economic appraisal.
4.18 The AOI severs the M60, so we will also include an intermediate step in the forecasting process where a set of scheme forecasts will be produced based on a wider cordoned model that includes the full extent of the M 60 . This will allow us to understand and quantify any impacts on use of the M60, particularly any potential for longer distance traffic to switch between using the clockwise and anticlockwise routes around the M60. Based on our experience from other projects (and from this AOI work) we do not expect this to be a significant effect of the scheme, but running the intermediate forecast will provide us with evidence about its magnitude. Subsequently, the model can be cordoned down to the defined AOI for all appraisal main forecasts and sensitivity tests.
4.19 The AOI for the morning and evening peak hours are shown in Figures 4.1 and 4.2 respectively.



## Traffic Signal Data

## Overview

4.20 The traffic signal data in the A6 to M 60 SATURN model is obtained using information supplied by the Greater M anchester Urban Traffic Control Unit (GM UTC) and Cheshire East Council.
4.21 The signal times at all junctions within the A6 to M60 AOI were reviewed in Spring 2010 and updated where required from the latest information available.

## Pedestrian Crossing Data

4.22 Due to the number of individual crossings in the model and the time therefore required to monitor/source individual call data, model timings at pedestrian crossings were derived via a programme which identified the location of each pedestrian crossing in the simulation area and allocated green and inter-green (i.e. red to traffic) times which reflected the probable use of the crossing.
4.23 The crossings were split into groups using M aplnfo. The locational criteria used varied by time period. In the AM peak crossings meeting one of three locational criteria were assumed to be called once every five minutes, namely:

- Those within 500 m of a secondary school and 300 m of a primary school
- Those within 500 m of a hospital; and
- $\quad$ Those within 500 m of a Census Special Output Area (SOA) zone centroid with greater than 500 employees.
4.24 In the inter-peak, crossings called once every five minutes were assumed to be those:
- Within 500 m of a hospital
- Within 200 m of a supermarket
- Within 200 m of a health centre
- Within 500 m of a university or college of further education.
4.25 In the PM peak, crossings meeting the following criteria were called once every five minutes:
- Within 500 m of a hospital
- Within 200 m of a supermarket
- Within 500 m of a SOA zone centroid with greater than 500 employees
- Within 500 m of a university or college of further education.
4.26 Crossings not meeting the five minute call criteria in the three time periods were assumed to be called once every 10 minutes.
4.27 The signal timings used were:
- For a five minute call interval, cycle time 300 seconds, green to traffic 277 seconds, intergreen time (green to pedestrians) 23 seconds
- For a 10 minute call interval, cycle time 600 seconds, green to traffic 577 seconds, intergreen time (green to pedestrians) 23 seconds.
4.28 These times are based on best-practice times for a Pelican crossing located on a 10 -metre wide carriageway. They also assume that no vehicles proceed through the crossing during the flashing amber period.
4.29 During further calibration of the model, additional adjustments were made to various pedestrian crossings as required to reflect observed journey times.


## SCOOT/MOVA Controlled Junctions

4.30 Within the Greater Manchester part of the AOI there are a significant number of signals and pedestrian crossings under SCOOT (Split Cycle Offset Optimisation Technique) operation.
4.31 SCOOT is a fully adaptive traffic control system that uses data from vehicle detectors and optimises traffic signal settings to reduce vehicle delays and stops. SCOOT provides a fast response to changes in traffic conditions and enables a response to variations in traffic demand on a cycle-by-cycle basis.
4.32 As the operation of SCOOT sites changes with traffic demand, signal timings at these junctions were obtained from GMUTC for an entire day in October 2015. The timings in each of the peaks were then averaged to give as accurate a representation as possible in the SATURN Network.
4.33 In addition to the SCOOT sites there are a number of signal-controlled junctions that are under MOVA operation. MOVA (M icroprocessor Optimised Vehicle Actuation) is a well-established strategy for the control of traffic light signals at isolated junctions - i.e. junctions that are uncoordinated with any neighbouring signals.
4.34 MOVA is designed to cater for the full range of traffic conditions, from very low flows through to a junction that is overloaded. MOVA operates in a delay minimising mode; if any approach becomes overloaded, the system switches to a capacity maximising procedure.
4.35 Again signal timings at MOVA sites are changeable and therefore timings were derived by entering the flows as derived from counts into the SATURN model and optimising the signal times to best represent the most likely green times at each of the junctions.

## Checks and Adjustments to Networks

4.36 A series of network checks were done after the network had been built and preliminary trip matrices had been assigned. For example, cases were investigated where the coded capacity was less than the traffic count and/ or where modelled delays were above a threshold.
4.37 In addition, coding on journey time routes within the Area of Influence was checked to better simulate observed travel times and delays on the network. Further to this selected trees (routes from a zone (origin) within the A6 to M60 AOI to other zones (destinations) within the AOI) were followed and checked.
4.38 As part of the update from A6 to M 60 a comprehensive network audit was undertaken focussing particularly on the key areas along the A6 corridor and Manchester Airport. The audit was informed by site visits and detailed inspection of recent aerial photography.

## Link Length Crow Fly Checks

4.39 As part of the network build process a sample of crow-fly warning messages ( 1 in 10) was examined to check that there was no systematic error in link length measurement and to ensure that those errors that were 'flagged' were not significant. No systematic errors were identified and any significant errors were corrected.
4.40 Within the A6 to M60 Area of Influence the lengths of all simulation links in the final 'built' network were examined by comparison against OS mapping. Those with link length discrepancies in excess of 30 m were checked in detail and the reasons identified. Of the 3,178 links in the AOI that were checked, 2,961 (93\%) were within 10 m of the mapped link length and only 59 (1.8\%) were found to have a discrepancy in excess of 30 m .31 of these links were found to have the correct link length coded, the discrepancy being due to, for example, node coordinates being slightly incorrect. Of the remaining 28 links only 2 were found with an error in excess of 100 m , while 8 had an error of 50 m or less.

## Bus Data

4.41 Buses are represented in the model as fixed link loads, with routes defined as chains of links in the simulation or buffer networks.
4.42 For the most part, information about bus services and frequencies in the $A 6$ to $M 60$ model is based on data from the TfGM bus service database, the Northwest Journey Planner website and bus timetables for North Cheshire.

## Adjustments to Link Cruise Speeds

4.43 In the SATURN networks as originally coded, the link cruise speeds coded were set to the posted speed limit for the link in question. However, during development of GM-SATURN, the model was found to be running too fast during the early stages of calibration/validation.
4.44 To slow the network down, tests were carried out to assess the impact on speeds of calling all pedestrian crossings (as described above) and reducing link speeds. The rationale behind reducing link speeds was that in the peak periods in particular, there are considerable 'friction' effects acting on the network, such as vehicles loading and unloading, drivers making short stops at local shops, buses stopping more frequently than at other times of the day etc. These activities have an impact on the cruise speed and will tend to reduce it below the speed limit.
4.45 For A6 to M60, a number of sensitivity tests were undertaken to determine the appropriate adjustments to link cruise speeds to match observed travel times on the network in the Area of Influence.
4.46 For the morning and evening peak hours, it was found that factoring Regional and District centre speeds by 0.75 and all other simulation links (except those with limits of 60 mph or more) regardless of location by 0.80 gave the closest approximation to observed travel times.
4.47 For the inter-peak, it was found that factoring Regional and District centre speeds by 0.85 and all other simulation links (except those with limits of 60 mph or more) regardless of location by 0.90 gave the closest approximation to observed travel times.
4.48 No speed adjustments were applied to motorway links.
4.49 It was noted that travel times in the rural network within Cheshire were generally too fast in initial model runs. These roads are generally outside both regional and district centres and built up areas and therefore were not factored via the process described earlier.
4.50 The fast travel times on these roads was attributed to the nature of the network where many roads have sharp bends and where visibility is poor or where friction effects occur. As a result the speeds were reduced using local knowledge of the network and aerial photos to better match observed times on those routes.

## M otorway Flow Delay Curves

4.51 In the development of GM-SATURN, it was noticed that speeds on the motorways appeared to be too fast in relation to observed journey times.
4.52 It was decided that flow delay curves would be added to motorway links in order to accurately model delays resulting from a reduction in motorway speeds when the link is reaching capacity
4.53 Motorway flow delay curves were derived from work undertaken by MVA with the Sheffield SATURN M odel, using COBA flow delay curves for motorways and suburban roads.
4.54 The standard flow-delay curves are most commonly applied to an 'average' stretch of motorway, with a standard carriageway width, no sharp bends and a distance of greater than 2 miles between junctions.
4.55 The motorway network in Greater Manchester, and in particular the M 60 and M 56 that pass through the A6 to M60 AOI, have several 'non-typical' sections of motorway. These sections have one (or more) of the following features;

- A 50 mph restriction due to a sharp bend;
- $\quad 2$ or 3 narrow lanes;
- $\quad$ Several merges / diverges within close proximity; and
- Junctions within approximately 1 mile of each other.
4.56 These characteristics require some sections of motorway to have different flow delay curves from normal, to reflect slower free flow speeds.
4.57 Even following the application of these flow-delay relationships, in the A6 to M 60 SATURN model it was found that particular sections of the motorway network were running too fast. Notably these were in areas with a 50 mph restriction for design reasons and/or where junctions are very closely spaced. To better represent the delays on these sections of motorway the free flow speed and speeds at capacity were reduced as part of calibration.


## Times in the External Network

4.58 In the SATURN model, travel times on links in the buffer network outside the A6 to M60 AOI and Greater Manchester are estimated using capacity restraint.
4.59 To determine the capacities the following processes were undertaken:

- All buffer links were coded with link capacities with 99,999 in all three time periods
- $\quad$ The network was converged
- $\quad$ Capacities were reset to be 1.2 times the demand flow using the maximum link flow in any time period which results in a single capacity used for each link across all time periods
4.60 The process of estimating capacities and calculating demand flows was iterative, and was repeated until there was no significant change in the calculated capacities from one assignment to the next. The overall change in link capacities was found to be less than $2 \%$ in five iterations.


## Generalised Cost Parameters

4.61 The generalised cost parameters used in the assignment process are derived using an Excel spreadsheet prepared by Systra. They are consistent with data taken from TAG Unit 3.5.6 (November 2016).
4.62 In line with current guidance the values of time for employers business are separated for short and long distance trips. The values of time for employers business have been calculated using a weighted average as per the DfT spreadsheets.
4.63 User inputs to the spreadsheet consist of:

- Average network speed, used in the calculation of vehicle operating costs
- Proportions of distance travelled by each of three car-based user classes (i.e. commute, employers business and other) as output from a five user class assignment; these are used in the calculation of the cost parameters for the all-car user class (i.e. as a weight).
4.64 All other inputs (e.g. values of time, fuel consumption parameters and fuel costs, fuel price grow th rates etc) were taken directly from the appropriate section of WebTAG.
4.65 The 2015 values of time (pence per minute - PPM) and distance (pence per kilometre - PPK) as output from the spreadsheet and used in the assignments are shown in Table 4.1 below.
4.66 A worked example showing a generalised cost calculation for PPM \& PPK Employer's Business Car AM Peak Hour has been provided in Appendix 1.

Table 4.1 2015 Generalised Cost Parameters Used in the Assignments

| Period | User Class | PPM | PPK |
| :--- | :--- | ---: | ---: |
| AM Peak Hour | Commuting Car | 20.20 | 6.38 |
|  | Employer's Business Car | 30.17 | 14.18 |
|  | Other Car | 13.95 | 6.38 |
|  | LGV | 21.23 | 13.62 |
|  | OGV | 21.67 | 53.10 |
| Inter-Peak Hour | Commuting Car | 20.56 | 5.86 |
|  | Employer's Business Car | 30.97 | 12.90 |
|  | Other Car | 14.85 | 5.86 |
|  | LGV | 21.23 | 13.45 |
|  | OGV | 21.67 | 51.79 |
| PM Peak Hour | Commuting Car | 20.38 | 6.26 |
|  | Employer's Business Car | 30.71 | 13.89 |
|  | Other Car | 14.60 | 6.26 |
|  | LGV | 21.23 | 13.45 |
|  | OGV | 21.67 | 51.79 |

DRAFT

## Network Statistics

4.67 Table 4.2 shows the overall network statistics.

Table 4.2 A6 to M60 SATURN Model Network Statistics (Version 21)

| Nodes |  |
| :--- | :---: |
| Type | Number |
| Simulation Nodes | 9,808 |
| Of which: |  |
| $\quad$ External Nodes | 1,610 |
| $\quad$ Priority Nodes | 5,394 |
| Roundabouts | 378 |
| Traffic Signals | 1,393 |
| $\quad$ Signalised Pedestrian | 1,033 |
| Crossings |  |
| Buffer Nodes | 1,791 |


| Links |  |  |
| :--- | :---: | :--- |
| Type | Number | Type |
| Real Simulation Links | 19,766 | Real Simulation <br> Links |
| Spigot Connector Simulation Links | 3,091 | Spigot Connector <br> Simulation Links |
| Buffer Network Links | 5,410 | Buffer Network <br> Links |
| Total | 28,267 | Total |
| Notes |  |  |

1. The figure for priority nodes includes a number of 'exploded' roundabouts i.e. large roundabouts broken down into a series of priority junctions.
2. The 2014 Saturn model was validated using SATURN Version 11.3.12U Level N3 (Multi-Core).
3. Development of the Prior Matrices

## Overview

5.1 This report describes the production of the prior trip matrices developed for use with the Greater Manchester Saturn M odel (GM SM ). This model informs the development of transport and land-use policies within Greater Manchester, and provide inputs to support the appraisal of transport infrastructure schemes under different economic scenarios.
5.2 The assignment matrices were mainly built using origin destination (OD) data collected from mobile phones during the Greater Manchester Mobile Phone OD Data Project (Reference1). Other data sources that have been used for the matrix development include:

- 2011 census journey to work data, to infer mode of travel
- Movements from the pre-existing 2012 and 2013 highway and PT assignment matrices, to infill movements that were not observed in the mobile phone study
- Travel diary data
- Intercept data from the 2010 Greater Manchester Area Transportation Surveys (2010 GM ATS) for PT modes.
5.3 The assignment matrices were built in two stages:
- First, initial matrices were formed from the mobile phone data.
- Next, movements from the mobile phone matrices were compared with movements from the pre-existing highway and PT matrices and were then assigned to the transport models to assess the accuracy of the link flow validation. The movements in the mobile phone matrices were adjusted as part of this process to correct for any perceived biases in the data and to improve the validation of the prior matrices.


## Mobile Phone Data

5.4 The objectives of the M obile Phone project were to obtain up-to-date information on trip making for use with the Greater M anchester Highway, Public Transport and Variable Demand Models. It was hoped that the study would provide a 'Proof-of-concept Dataset', which would provide information about trip making within the County which was as least as good as could be obtained from traditional intercept surveys, at a fraction of the cost.
5.5 The main points relating to the data are as follows:

- Data was collected for a four weeks period, comprising the weeks beginning Monday $13^{\text {th }}$ May 2013, M onday $20^{\text {th }}$ May 2013, Monday $10^{\text {th }}$ June 2013 and M onday $17^{\text {th }}$ June 2013
- Data was, however, only processed for 19 days, (due to data collection and storage problems), and has been averaged for weekdays, Saturdays and Sundays
- Data was collected for all movements within Greater Manchester and the surrounding area
- The weekday source data is based on a sample of over 69 million trips
- Data was anonymised, to protect privacy, with device IDs being re-set each day
- Data was zoned to a 631 zone sectoring system, (representing aggregations of transport modeling zones), comprising 503 sectors inside Greater Manchester and 128 sectors outside the County
- The start and end times of trips were aggregated to the nearest hour
- Intra-sector movements were only partially observed in the dataset and therefore have to be 'infilled' using information from pre-existing matrices or other sources.


## Mode Allocation

5.6 Trips were allocated to 3 modes comprising:

- Highway modes, which includes cars, Light Goods Vehicles, Other Goods Vehicles, Buses/ Coaches and M otor Cycles
- Rail, which includes M etrolink
- Slow modes (walk and cycle).
5.7 M ovements were allocated to modes using information about:
- The speed of trips and trip lengths. (Devices travelling at slow speeds and making short journeys were assumed to be slow modes, other non-rail trips were classified as Highway).
- Rail/Metrolink trips were classified by identifying cell tower handover pairs that had patterns associated with groups of people on the same route travelling at nearly the same time and speed and identifying these as train lines. Devices that 'handed over' from one cell of such a pair to another were classified as train/tram trips.


## Home Sectors

5.8 The home ends of trips were inferred based the time at which each device (mobile phone) was first 'seen':

- If the device was seen before 4 pm , it was assumed that the location of the first point of observation was the home end
- If the device was not seen before 4 pm , it was assumed that the location of the last point of observation was the home end.


## Expansion Process

5.9 The mobile phone data was expanded using population data from the 2011 census. The expansion was carried out in two stages:

- Firstly, the population data was used to derive controls for the observed movements
- Next, 'person type' adjustment factors were applied, (to try to correct for any person type bias in the data), based on the characteristics of trips made by different individuals (mode or travel, time of first trip, trip length etc.)


## Limitations of the Data

5.10 Whilst OD data collected from mobile phones has some strengths compared to data collected using traditional intercept surveys, including the ability to obtain very large sample sizes with a minimum amount of disruption to traffic flows and travelers, there are a number of known limitations with the data including:

- Difficulties defining what a trip is and identifying short distance trips
- Spatial accuracy - the accuracy with which phone locations can be determined is dependent on antenna/cell tower coverage. Locations should be most accurate in areas with a high density of cell towers, typically comprising town centres and areas with high population, but will be less accurate elsewhere.
- The data only provides limited information about travel mode (highway, rail, slow modes)
- Data does not provide any information about travel purpose
- Data is relatively cheap (and it is possible to obtain very large sample sizes), but we need to be aware of/learn about its shortcomings.


## Overview of the Matrix Building Process

5.11 Assignment matrices were built for an average weekday for three time periods comprising:

- The AM peak hour (0800-0900)
- An average inter-peak hour (defined to be the average of the 1000-1600 time period)
- The PM peak Hour (1700-1800)
5.12 The key steps in the matrix building process are illustrated below in Figure 5.1. These involved:
- Checking the data and learning about its weaknesses
- Building the assignment matrices
- Making adjustments to the matrices to correct for apparent problems, to create the final set of matrices.


2. Check Data
3. Build Highway/PT Assignment Matrices

4. Prior Trip Matrices

Figure 5.1 Matrix Building Process

## Data Checks

5.13 Basic checks were carried out on the mobile phone data prior to building the assignment matrices to learn about its properties and to identify any issues that might be of concern. These included:

- Checks on hourly flow indices
- Checks on home versus non-home trips
- Checks on weekday trip totals and mode share proportions
- Checks on rail and M etrolink trip totals.
5.14 Figure 5.2 compares the proportions of trips in the mobile phone data beginning in each of the hours between 6 o'clock in the morning and 10 o'clock in the evening for the average weekday with similar profiles for ATC data.
5.15 The results appear to be sensible, with movements in the mobile phone data peaking between the hours of 7 and 10 o'clock in the morning and 4 and $60^{\prime}$ clock in the evening. There also appears to be quite a good match between the two profiles, which have similar shapes, although it does appear that the mobile phone data might contain too many trips in the morning peak period and too few trips in the inter-peak period.


Figure 5.2 Weekday Average Hourly Flow Indices
5.16 Table 5.1 compares the proportions of weekday Home and Non-Home trips in the mobile phone dataset. Once again, the results appear to be plausible, with the majority of trips having an origin as home in the morning and a destination as home in the evening. The proportions of from home trips in the morning do, however, appear to be a little low. It also looks like there might be a lack of symmetry over the whole day, with approximately $43 \%$ of trips having an origin as home and only $32 \%$ of trips having a destination as home. It might be expected that these figures would be fairly similar.

Table 5.1 MPOD Data All Origins vs All Destinations (Weekday, All M odes)

| Total Trips | AM Peak <br> Period | Inter-Peak <br> Period | PM Peak <br> Period | All Day |
| :--- | :---: | :---: | :---: | :---: |
| Where Origin is Home | $66 \%$ | $37 \%$ | $25 \%$ | $43 \%$ |
| Where Origin is Not Home | $34 \%$ | $63 \%$ | $75 \%$ | $57 \%$ |
| Destination is Home | $14 \%$ | $32 \%$ | $52 \%$ | $32 \%$ |
| Where Destination is Not Home | $86 \%$ | $68 \%$ | $48 \%$ | $68 \%$ |

5.17 Table 5.2 shows weekday trip totals from the mobile phone data for the period 07001900 broken down by mode, for trips with an origin and destination inside Greater Manchester. The table shows that almost $98 \%$ of trips have been allocated to the highway mode. The percentages of rail and walk trips appears to be low, with only about $0.6 \%$ of trips in the M obile Phone data being allocated to rail and $1.6 \%$ of trips to walk or cycle.

| Table 5.2 | MPOD Data 0700-1900 Weekday Trip Totals By Mode for Trips with an <br> Origin and Destination Inside GM (Person Trips) |  |  |
| :--- | :---: | :---: | :---: |
|  | $0700-1900$ |  |  |
|  | Trips | Percentage |  |
| Highway | $4,874,522$ | $97.7 \%$ |  |
| Rail | 30,821 | $0.6 \%$ |  |
| Walk/Cycle | 81,686 | $1.6 \%$ |  |
| Total | $4,987,029$ | $100.0 \%$ |  |

Highway Matrix Building
5.18 The highway matrices were built to the 993 zone system used with the GM SM .
5.19 A summary of the matrix building procedure is presented in Figure 5.3. Briefly, it involved 8 steps, as follows:
i. First, movements for the Highway and Rail modes from the mobile phone data were combined and 631 zone matrices built (at the mobile phone data sector level) for the AM peak period 0700-1000, the PM peak period 1600-1900 and the inter-peak period 1000-1600.
ii. Next, the 631 zone matrices were disaggregated to the 993 zone system used with the Saturn model. (During this process, trips between sectors comprising several GM SM zones were allocated to their constituent Saturn zones on a proportional basis, using row/column weights calculated from all-purpose trip end totals derived from the 2012 Saturn model vehicle matrices, Reference 2).
iii. Next, the 993 zone all mode matrices were disaggregated into rail, bus and other highway trips. This was done on a cell-by-cell basis using information from TfGM's 2011 census journey-to-work matrices to estimate mode share.

The method was as follows:
If, for example, there were 100 trips between zones i and j in the disaggregated mobile phone matrix, and there were 50 car, (i.e. car driver plus car passenger),
and 10 bus, (i.e. bus passenger) and 5 rail trips in the 2011 census matrix, then the estimated number of rail trips between zones i and j from the mobile phone data was calculated to be:
$7.69=100 \times[5 /(50+10+5)]$
The estimated number of bus trips was calculated to be:
$15.38=100 \times[10 /(50+10+5)]$
The estimated number of other highway trips, (which were assumed to comprise car, Light Goods Vehicle and Other Goods Vehicle trips), was calculated to be:
$76.93=100-(7.69+15.38)$
iv. Next, vehicle occupancy factors were used to convert person trips to vehicle flows. For simplicity, average car, LGV and OGV values derived from WebTAG were used, as shown in Table 5.3.
v. Next, period to hour factors calculated from traffic counts were applied to convert the all vehicle flows for the chosen periods to modelled hours, as shown in Table 5.4.
vi. Next, the all vehicle flows were disaggregated into separate car, LGV and OGV flows, (on a cell by cell basis), using vehicle proportions from the existing 2012 GMSM assignment matrices.

The method was as follows:
If, for example, there were 100 highway trips between zones $i$ and $j$ in the disaggregated mobile phone matrix, and there were 70 car, 10 LGV and 5 OGV trips in the corresponding cells of the 2012 GM SM matrices, then the estimated number of car trips from the mobile phone data between zones $i$ and $j$ was calculated to be:
$82.35=100 \times 70 /(70+10+5)$
The estimated numbers of LGV and OGV trips would be:
$11.76=100 \times 10 /(70+10+5)$ and

$$
5.89=100 \times 5 /(70+10+5) \text { respectively. }
$$

vii. Finally, 'marker matrices' were used to zeroise cells corresponding to intrasector movements in the mobile phone matrix, (which were only partially observed in the mobile phone dataset), and to update these cells with movements from the 2012 Saturn vehicle matrices.

| Table 5.3 Highway Matrix Vehicle Occupancy Factors |  |  |  |
| :--- | :---: | :---: | :---: |
| Time Period | Vehicle Occupancy Factor |  |  |
|  | Car | LGV | OGV |
| AM Peak Period | 1.34 | 1.23 | 1.00 |
| Inter-Peak Period | 1.23 | 1.23 | 1.00 |
| PM Peak Period | 1.42 | 1.23 | 1.00 |


| Table 5.4 | Highway Matrix Period to Hour Factors |
| :--- | :---: |
| Time Period | Factor |
| AM Peak | 0.37 |
| Inter-Peak | 0.167 |
| PM Peak | 0.36 |



Figure 5.3 Highway Assignment Matrix Building Procedure

## Highway Matrix Adjustments

5.20 Following the production of the initial matrices, the matrices were assigned to the 2014 GM SM highway networks. Comparisons of link flows with counts were then made for each vehicle type and time period to assess the performance of the model. Comparisons were also made with movements from the pre-existing 2012 GM SM matrices to compare trip totals, sector-to-sector movements and trip length distributions. A series of adjustments were then made to the mobile phone matrices to try to improve the validation, comprising:

- Adjustments to point zone trips
- Adjustments to trip length distributions
- Trip distribution and journey purpose adjustments


## Point Zone Trips

5.21 The GM Saturn model contains approximately 100 'point zones', representing large developments such as superstores, hospitals and industrial estates.
5.22 To try to ensure that the point zone entry and exit volumes in the prior trip matrices were as accurate as possible, it was decided to apply row and column adjustment factors to the 2014 car matrices, (separately by time period), to reproduce the trip end totals from the 2012 GM SM matrices. (Information about point zone trip end totals in the 2012 matrices had been derived from traffic count data for zones where vehicle counts were available and trip rates from the TRICS database for zones where counts were not available, as described in Reference 2. Traffic counts were available for approximately 40 sites).

## Trip Length Distributions

5.23 The charts in the left hand side of Figures 4.3-4.5 compare the trip length distributions for the Mobile Phone matrices with the trip length distributions for the 2012 GM SM matrices for the AM peak, inter-peak and PM peak hours respectively, for car, LGV and OGV trips with an origin or destination inside Greater Manchester. The comparisons appear to show that the mobile phone matrices under-estimate short distance trips and over-estimate medium and longer distances trips, especially in the inter-peak hour.
5.24 A second series of adjustments factors were therefore applied, (by distance band), to improve the fit between the mobile phone and 2012 GM SM trip length distributions, as shown in Table 5.5.

Table 5.5 MPOD Highway Matrix Trip Length Adjustment Factors

| Travel <br> Distance $(\mathrm{km})$ | AM Peak Hour |  |  | Inter-Peak Hour |  |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Car | LGV | OGV | Car | LGV | OGV | Car | LGV | OGV |  |
| $0-7.5$ | 1.00 | 0.93 | 0.71 | 1.22 | 1.22 | 0.95 | 1.06 | 0.86 | 0.62 |  |
| $7.5-15.0$ | 0.79 | 1.00 | 0.55 | 0.80 | 1.07 | 0.72 | 0.85 | 0.86 | 0.44 |  |
| $>15.0$ | 0.75 | 1.82 | 1.13 | 0.65 | 2.00 | 1.60 | 0.77 | 1.33 | 0.91 |  |

5.25 These factors served two purposes:

- Firstly, they helped to improve the fit between the trip length distributions
- Secondly, they helped to correct for discrepancies between the numbers of trips in the two sets of matrices, by controlling the trip totals in the mobile phone matrices to match those in the 2012 GM SM matrices, by travel distance band.
5.26 The trip length distributions for the adjusted matrices are shown in the right hand side of Figures 5.4-5.6.


Figure 5.4 AM Peak Hour Trip Length Distributions

Note: The charts in the left hand side of the Figure show the un-adjusted trip length distributions. The charts in the right hand side of the figure show the adjusted trip length distributions.

Highways Forecasting and Analytical Services
DRAFT A6 to M60 Relief Road
A6M 60 LMVR


Figure 5.5 Inter-Peak Hour Trip Length Distributions

Note: The charts in the left hand side of the Figure show the un-adjusted trip length distributions. The charts in the right hand side of the figure show the adjusted trip length distributions.


Figure 5.6 PM Peak Hour Trip Length Distributions

Note: The charts in the left hand side of the Figure show the un-adjusted trip length distributions. The charts in the right hand side of the figure show the adjusted trip length distributions.

## Journey Purpose Adjustments

5.27 The final step in the matrix building procedure involved disaggregating the all-purpose car matrices to form separate purpose matrices for modelling. Separate matrices were formed for 12 car journey purposes comprising:

- Home-to-work
- Work-to-home
- Home-to-education
- Education-to-home
- Home-to-shopping
- Shopping-to-home
- Home-to-employers' business
- Employers' business-to-home
- Home-to-other
- Other-to-home
- Non-home-based employers' business
- Non-home-based other
5.28 For assignment, however, the separate purpose matrices were aggregated to form 5 'user classes' comprising:
- Commuting cars (home-to-work plus work-to-home car trips)
- Employers' business cars (home-based plus non-home-based employers' business car trips)
- Other cars (all other car trips)
- LGVs (all purpose LGV trips)
- OGVs (all purpose OGV trips).
5.29 Initially, a simple approach was adopted, which involved using the purpose splits from the 2012 GMSM car matrices to disaggregate the all-purpose mobile phone trips on a cell-by-cell basis.
5.30 If, for example, there were 100 car trips between zones $i$ and $j$ in the mobile phone matrix, and there were 70 car trips in total in the corresponding cells of the 2012 GM SM all-purpose car matrix, and there were 10 home-to-work trips in the GM SM home to work car matrix, then the estimated number of trips between zones $i$ and $j$ in the disaggregated home to work mobile phone matrix was calculated to be:

$$
14.2=100.0 \times(10.0 / 70.0)
$$

Average default proportions calculated across the whole matrix were used to disaggregated movements between cells where there were no trips in the GMSM matrix but where trips did exist in the all-purpose mobile phone matrix.
5.31 The procedure was repeated for each OD pair and journey purpose category in turn to build up the disaggregated matrices. A cumulative rounding procedure was adopted when implementing the process to preserve matrix totals.
5.32 Basic checks were carried out to ensure that the journey purpose mixes were plausible. A regression analysis was also performed to compare the relationship between the number of from home trips beginning in each zone and the number of residential address. The correlation coefficients were lower than had been expected, however, with $R^{2}$ values of 0.73 for the AM peak hour, 0.59 for the inter-peak hour and 0.54 for the PM peak hour. By comparison, the corresponding figures for the 2012 GM SM car matrices were 0.72 , 0.78 and 0.71 respectively, which suggested that the distribution of trips in the mobile phone matrices was different to that in the existing GM SM matrices, and that the spatial accuracy of the trip origins and destinations might not be as good as hoped at the transportation zone level.
5.33 In the light of these results it was decided to investigate a slightly different approach to allocating journey purposes to the mobile phone matrices, which involved compressing the matrices back to the mobile phone sector level before applying the GM SM purpose splits. The compressed (separate purpose) matrices were then expanded back to the transport zone level by using the number of residential addresses in each zone as weights to disaggregate home based trips between GM SM zones and weights calculated from the all-purpose trip end totals from the 2012 Saturn vehicle matrices for other trip purposes, similar to the procedure described in Section 4.3.
5.34 The steps in carrying out the procedure were as follows:
i. Compress the adjusted mobile phone matrices 4.4 .7 back to the 631 zone mobile phone sector level
ii. Compress the separate purpose 2012 GMSM car matrices to the mobile phone sector level
iii. Use the purpose splits from the compressed GM SM matrices to disaggregate the all-purpose mobile phone trips between journey purposes, at the sector level
iv. Disaggregate the separate purpose 631 zone (sector) matrices back the 993 zone system by allocating trips to their constituent GMSM zones on a proportional basis, using row/column weights calculated from the number of residential addresses in each zone to apportion trips where the trip origin or destination purpose is home, or the number of all-purpose trip end totals derived from the 2012 Saturn car matrices as weights where the trip origin or destination purpose is not home.
5.35 The regression analysis for the updated matrices confirmed that there was a stronger relationship between the number of from home trips beginning in each zone and the number of residential address, with $\mathrm{R}^{2}$ values of $0.85,0.83$ and 0.84 for the AM peak, PM peak and inter-peak hours respectively.
5.36 Table 5.6 shows trip totals for movements with an origin or destination inside Greater Manchester for the adjusted mobile phone matrices and the percentage differences between the corresponding totals for the 2012 GM SM post matrix estimation matrices by user class, vehicle type and time period.

| 5.6 Adjusted Highway Matrix Totals |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Class | AM Peak Hour |  |  | Inter-Peak Hour |  |  | PM Peak Hour |  |  |
|  | $\begin{gathered} 2014 \\ M P \end{gathered}$ | $\begin{gathered} \hline 2012 \\ \text { GM SM } \end{gathered}$ | $\begin{aligned} & \hline \% \\ & \text { Diff } \end{aligned}$ | $\begin{gathered} 2014 \\ M P \end{gathered}$ | $\begin{gathered} 2012 \\ \text { GMSM } \end{gathered}$ | $\begin{gathered} \hline \% \\ \text { Diff } \end{gathered}$ | $\begin{gathered} 2014 \\ \text { MP } \end{gathered}$ | $\begin{gathered} 2012 \\ \text { GM SM } \end{gathered}$ | $\begin{gathered} \hline \% \\ \text { Diff } \\ \hline \end{gathered}$ |
| Commute Car | 173,708 | 164,798 | +5\% | 38,912 | 34,965 | +11\% | 142,739 | 138,442 | +3\% |
| EB Car | 16,915 | 16,304 | +4\% | 28,372 | 27,487 | +3\% | 20,086 | 18,798 | +7\% |
| Other Car | 153,737 | 165,017 | -7\% | 212,303 | 220,402 | -4\% | 190,840 | 196,609 | -3\% |
| All Car | 344,360 | 346,120 | -1\% | 279,588 | 282,854 | -1\% | 353,665 | 353,848 | 0\% |
| LGV | 42,356 | 40,678 | +4\% | 40,931 | 39,534 | +4\% | 34,242 | 33,628 | +2\% |
| OGV (PCU) | 19,372 | 18,841 | +3\% | 20,874 | 20,079 | +4\% | 9,205 | 8,765 | +5\% |
| Total (PCUS) | 406,088 | 405,639 | 0\% | 341,393 | 342,468 | 0\% | 397,112 | 396,241 | 0\% |

## Expansion from 993 Zone to 1097 Zone System

5.37 The 2014 matrices from the GM SATURN M odel are based on a 993 zone system. The zoning system utilised for the A6M ARR model and subsequently the A6 to M60 M odel is a more detailed and the number of zones is increased to 1097 zones.
5.38 The zones in the 1097 A6 to M 60 model nest within the 993 zone GM SM zoning system. As such the trips allocated in the 993 zone system were split pro rata as per the splits in the A6 M ARR model to produce a revised 1097 zone matrix.

## 6. Matrix Estimation

## Introduction

6.1 The validation results for the prior PCU matrices indicated that only about $24 \%$ of the counted links across Greater Manchester had a GEH value of less than 5 in the AM peak hour. The corresponding figures for the PM peak and inter-peak hours were $23 \%$ and $21 \%$ respectively, indicating that matrix estimation using counts would have to be used if the assignment validation was to be significantly improved.
6.2 Separate matrix estimation runs were carried out for the car, LGV and OGV matrices for each of the modelled time periods. A total of four rounds of matrix estimation were carried out for each run, to ensure that the updated matrices did not change significantly between successive iterations, and that he procedure was satisfactorily converged. The method was as follows:

- Assign the prior matrix to the highway network to produce paths
- Run matrix estimation to produce a revised (estimated) demand matrix
- Assign the estimated demand matrix to produce revised paths
- $\quad$ Re-run matrix estimation using the prior matrix and the revised paths from above to produce a further estimate of the demand matrix
- Repeat
- Matrix Estimation stops once a degree of matrix 'stability' is reached


## Traffic Count Data

6.3 The traffic count data for the matrix estimation runs was obtained from five sources:

- M anual classified counts from HFAS's traffic counts database (GM Counts)
- $\quad$ Automatic Traffic Counts (ATC) from HFAS's counts database
- ATC counts from the Highways Agency's TRADS database
- ATC and manual counts supplied by Cheshire East Council; and
- Entry and exit counts for car parks at M anchester Airport supplied by AECOM .
6.4 All counts were checked to exclude counts affected by known ‘unusual' events such as accidents, road works, adverse weather conditions, holidays etc.
6.5 Where manual counts were used, separate counts were obtained for car, LGV, OGV and PCU flows for each of the modelled hours. Where ATC counts were used, all vehicle flows were obtained. These were converted into separate car, LGV, OGV and bus flows using vehicle composition factors calculated from manual counts at the same locations.
6.6 The counts were allocated to links in the highway network using an automatic count matching procedure developed by HFAS, based on the count OSGRs and the coordinates of the link polylines. The count and link direction and the count and link road class and number were also used as additional match criteria, to minimise the possibility of transcription errors.
6.7 For matrix estimation and validation purposes, all of the counts that were used in the validation were factored to a 2015 October average weekday using locally derived factors.


## Count Checks

6.8 Matrix estimation procedures require accurate and consistent traffic counts if they are to work succesffully. As matrix estimation strategies were developed, inconsistent counts were identified and eliminated from this process. Reasons for counts being eliminated included:

- Day-to-day variations in traffic flows
- Enumerator errors; and
- Other errors, such as count transcription errors, where counts are allocated to the wrong links or the wrong direction on a link.
6.9 Inconsistent counts were also identified through an automatic checking procedure within the SATURN programme, where counts violated 'Kirchoff's rule'. (These violations occur, for example, when two counts that are physically separated by intervening links are not equal, but where the assignment pattern indicates that all flows that pass through the first count site must also pass through the second).
6.10 Where it was thought that the discrepancies may have been caused by a counting error, or where the count might have been affected by unusual events that had not been picked up in the filtering exercise described above, then the counts were discarded. In situations where the inconsistencies were small, (such as might be caused by day-to-day variations in traffic flows), the counts were automatically averaged using the AVERK option in SATURN's SATPIJA program.


## Cordons and Screenlines

6.11 To provide reassurance that the validation of the base year model was acceptable over a wider area counts on cordons and screenlines across Greater Manchester were included in the validation process. Overall, 908 counts were selected for matrix estimation and validation purposes across Greater Manchester. For the purposes of this report only cordons and screenlines within the A6 to M60 Area of Influence have been reported in detail but results for other cordons and screenlines within Greater Manchester are available on request from HFAS.
6.12 Overall, 1241 counts were selected for matrix estimation and validation purposes across Greater Manchester. For the purposes of this report only cordons and screenlines within the A6 to M60 Area of Influence have been reported in detail but results for other cordons and screenlines within Greater M anchester are available on request from HFAS.
6.13 In total, 516 of these counts were in the A6 to M60 AOI comprising of 373 counts input to the matrix estimation runs and 143 counts providing an independent check on the calibrated model.
6.14 Where possible, the matrix estimation counts were combined to form a series of cordons and screenlines within the study area, to intercept movements between local centres, and in those areas where the scheme benefits are most likely to occur.
6.15 In total, 20 (two-way) cordons and screenlines in the A6 to M60 AOI were formed for use in matrix estimation, as illustrated in Figure 6.1.
6.16 Two independent routes were formed running parallel to the A34and north of the M 60 that was not used in matrix estimation, but which was set aside to provide an independent check on the calibrated model.
6.17 The remaining counts that were not used to form cordons and screenlines were divided into three groups comprising:

- $\quad$ TRADS counts on motorways for use in matrix estimation (approximately 40)
- Independent TRADS counts on motorways, (that were not used in matrix estimation), which were set aside to provide an independent check on the calibrated model (8); and
- Other Independent (ad hoc) counts on local roads in the study area, that were also set aside to provide an independent check on the calibrated model (approximately 60).


## Point Zone Counts

6.18 In addition to the 'standard' zones representing areas with similar land use and travel patterns, the A6 to M60 SATURN model also includes a number of 'point zones', representing developments such as large superstores, hospitals and industrial estates.
6.19 Where point zone counts were available, the entry and exit flows at the point zone sites were used as zonal constraints in the matrix estimation runs.
6.20 Point zones within the Area of Influence include:

- $\quad$ Car Parks at M anchester Airport
- Retail Parks such as Cheadle Royal and Handforth Dean
- Individual superstores such as TESCO in Didsbury; and
- Business Parks/Trading Estates such as Stockport Trading Estate.


## Manchester Airport Car Park Counts

6.21 The Manchester Airport car park counts were also used as zonal constraints in the matrix estimation runs, to ensure that movements within the airport site were modelled as accurately as possible.


Figure 6.1 Cordon and Screenline Locations

## Matrix Estimation Results

6.22 This section summarises the changes brought about by matrix estimation. It is divided into five parts describing:

- $\quad$ Changes to matrix totals
- $\quad$ Changes to zonal trip ends
- $\quad$ Changes in GEH frequency distributions for the prior and estimated matrices
- Changes in trip length distributions.
6.23 Table 6.1 shows the total trips in the estimated matrices and the percentage change from the prior matrices by vehicle type and time period for trips in the model.

| Table 6.1 | Total Trips in Estimat Matrices | M atrice | and Pe | ntage | ange fro | Prior |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Type | Time Period |  |  |  |  |  |
|  | AM Peak |  | Inter-Peak |  | PM Peak |  |
|  | Trips | $\begin{array}{\|c\|} \hline \% \\ \text { Change } \end{array}$ | Trips | $\begin{gathered} \% \\ \text { Change } \end{gathered}$ | Trips | $\begin{gathered} \text { \% } \\ \text { Change } \end{gathered}$ |
| Car | 1096353 | -1.12\% | 837751 | -1.08\% | 1087589 | -0.89\% |
| LGV | 48175 | 3.41\% | 46374 | 0.63\% | 39968 | 1.94\% |
| OGV | 29333 | 5.53\% | 32607 | 2.93\% | 15706 | 4.70\% |
| Total (PCUS) | 1173862 | -1.06\% | 916733 | -1.06\% | 1246597 | -0.84\% |

6.24 For cars, the total numbers of trips have reduced in all three time periods, by approximately $1.1 \%$ in the AM peak hour, $1.0 \%$ in the inter-peak and $1.0 \%$ in the PM peak hour. For LGVs the total trips have increased in all three time periods, ranging from an approximate $3 \%$ increase in LGV trips in the AM peak hour to an approximate $1 \%$ in the interpeak and evening peak. For OGVs the total trips have decreased in the AM and PM peak hour ranging from an approximate $1.0 \%$ decrease in OGV trips in each time period.
6.25 Overall, the total change in PCU trips is relatively small, with a reduction of approximately $1 \%$ in each modelled hour
6.26 Appendix 2 gives a more detailed comparison of the prior and estimated matrices based on the aggregation of the 1097 A6 to M 60 zones to the 12 sectors shown in Figure 6.2. Any sector that changes by greater than $5 \%$ and 250 pcu's are highlighted in grey.
6.27 In the morning peak the majority of changes in sector to sector movements are within 5\% of 250 pcu's. However, the greatest changes in the prior to post sector to sector movements are as follows;

- Trafford (Outside M60) to Manchester West of A34 with a decrease of 572 pcu's - this would not use the proposed scheme;
- Trafford (Outside M60) to Wigan with a decrease of 720 pcu's - this would not use the proposed scheme;
- Wigan to Trafford (Outside M60) with a decrease of 809 pcu's - this would not use the proposed scheme;
- Rochdale to Manchester Within M 60 with a decrease of 739 pcu's - this would not use the proposed scheme;
- Rochdale to Manchester Within M 60 with a decrease of 739 pcu's - this would not use the proposed scheme.
6.28 In the interpeak the majority of changes in sector to sector movements are within $5 \%$ of 250 pcu's. However, the greatest changes in the prior to post sector to sector movements are as follows;
- East of A34 to West of A34 - with an increase of 924 pcu's these are local trips that are unlikely to use the proposed scheme
- Trafford (Outside M60) to Wigan with a decrease of 506 pcu's - this would not use the proposed scheme;
- Wigan to Trafford (Outside M60) with a decrease of 581 pcu's - this would not use the proposed scheme.
6.29 In the evening peak the majority of changes in sector to sector movements are within $5 \%$ of 250 pcu's. However, the greatest changes in the prior to post sector to sector movements are as follows;
- Trafford to Manchester (East of M46) with an increase of 630- pcu's - these would shorter distance trips that are unlikely to use the proposed scheme.

Trafford to M anchester Within the M 60 with an increase of 1500 pcu's - the majority of these movements would be to the North and West of the proposed scheme and as such would not be route via the scheme

- Trafford to Wigan with an decrease of 600 pcu's - the majority of these movements would be to the North and West of the proposed scheme and as such would not be route via the scheme
- Manchester Within the M60 to Cheshire East with an increase of 773 pcu's but as this zone encompasses the majority of the district district and given the location of the scheme to the South of the district only a marginal amount of this reduction in trips would have used the proposed scheme. Overall, this would slightly increase the forecast benefits of the proposed scheme;
- Wigan to Trafford with an decrease of 600 pcu's - the majority of these movements would be North to South movements and as such would not be route via the scheme



## Changes to Zonal Trip Ends

6.30 Table 6.2 shows regression statistics (slopes, intercepts and R-Squared values) for the best fit line obtained by regressing trip end totals from the estimated matrix against the prior matrix. Separate results are presented for the car, LGV, OGV and all vehicle PCU matrices, for each of the modelled hours. TAG suggests that the slope of the regression line should fall within the range 0.99 to 1.01 , that the intercept should be near to zero and that the R-squared value should be in excess of 0.98 , but notes that these figures may be difficult to achieve in large scale strategic models. The values of the regression statistics will, for example, be dependent on zone sizes, the numbers of trips generated in each zone and the number of movements that are updated by the matrix estimation procedure.

Table 6.2 Summary of M atrix Estimation Zonal Trip End Changes

| Time Period | Matrix | Slope | Intercept | R-Squared |
| :--- | :--- | :---: | :---: | :---: |
| Weekday AM Peak | Car | 1.00 | 19.98 | 1.00 |
|  | LGV | 1.00 | -2.75 | 0.94 |
|  | OGV (PCU) | 1.08 | -0.95 | 0.93 |
|  | All Vehicle (PCU) | 1.00 | 16.35 | 1.00 |
| Weekday Inter-Peak | Car | 1.00 | 14.57 | 1.00 |
|  | LGV | 1.00 | -0.58 | 0.94 |
|  | OGV (PCU) | 1.04 | -0.58 | 0.95 |
|  | All Vehicle (PCU) | 1.00 | 14.66 | 1.00 |
| Weekday PM Peak | Car | 1.01 | 1.07 | 1.00 |
|  | LGV | 0.99 | -0.60 | 0.93 |
|  | OGV (PCU) | 1.05 | -0.13 | 0.94 |
|  | All Vehicle (PCU) | 1.01 | -0.49 | 1.00 |

6.31 The R-Squared values for the weekday car matrices meet the TAG criteria in all time periods. The values of the slope statistics also meet the benchmark figures in all time periods. The values of the intercepts range from 1.07 for the evening peak matrix to 20 for the morning peak matrix. As noted above, however, the size of the intercept value will be dependent on the number of trips generated in each zone, and is likely to be greater for matrices with large cell values.
6.32 The regression statistics for the weekday LGV and OGV matrices fail to achieve the TAG criteria, with R-squared values ranging from 0.93 to 0.95 , and slopes ranging from 0.99 to 1.08 . This is probably related to the small number of trips in the commercial vehicle matrices, and difficulties obtaining robust regression statistics for small sample sizes. The results for the all-vehicle PCU matrices are very good, however, with the R-squared and slope values achieving the benchmark criteria in all time periods.
6.33 In the morning peak the absolute difference for origins ranges from - 223 pcu's to 147 pcu's but most of these are located in the external network remote to the proposed scheme and Trafford Park which was updated with new Origin Destination data from another study. For destinations changes in total number of trips ranges from - 451 pcu's to 540 pcu's but these are located in the
external network remote to the proposed scheme and Trafford Park which has been recently updated with new count data.
6.34 In the interpeak the absolute difference for origins ranges from-211 pcu's to 235 pcu's the majority of which are remote to the proposed scheme or external to the study area and Greater Manchester and again zones associated with Trafford Park. For destinations two zones have increases in total number of trips ranges from -667 pcu's to 434 pcu's but the majority are located in the external network remote to the proposed scheme and Trafford Park which has been recently updated with new count data. In the area of the scheme two zones show larger decreases of approximately 300 pcu's and these are located in Cheadle Heath Retail Park and Roundthorn Industrial Park which have updated count data.
6.35 In the evening peak the absolute difference for origins ranges from-930 pcu's to 2438 pcu's (external zones)the majority of which are remote to the proposed scheme or external to the study area and Greater Manchester and again zones associated with Trafford Park. For destinations two zones have increases in total number of trips ranges from -1142 pcu's to 534 pcu's but these are located in the external network remote to the proposed scheme and Trafford Park which has been recently updated with new count data.

## Changes to GEH Frequency Distributions

6.36 Tables 6.3 to 6.5 show GEH $^{1}$ frequency distributions from the assignment of the prior and estimated matrices for the AM peak, inter-peak and PM peak hours. The tables give an indication of the way in which the estimated matrices improve the assignment validation. Separate results are presented for the independent counts, the matrix estimation counts and for all counts combined.
6.37 Considering the results for the AM ${ }^{1}$ peak hour, approximately $89 \%$ of the counted links used in M atrix Estimation have a GEH value of less than 6 for the prior matrix, for all counts combined. This figure increases to almost $85 \%$ for the updated matrix, demonstrating how matrix estimation has improved the assignment validation.


[^0]Table 6.3 AM Peak Hour GEH Cumulative Frequency Distributions for the Prior and Estimated Matrices

| GEH <br> Range | Prior M atrix |  |  | Estimated M atrix |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Independent Counts | M atrix Estimation Counts | All Counts | Independent Counts | M atrix Estimation Counts | All Counts |
| 0-2 | 3.4\% | 13.0\% | 12.8\% | 21.8\% | 64.0\% | 58.7\% |
| 0-4 | 13.8\% | 28.3\% | 28.0\% | 38.2\% | 79.9\% | 74.6\% |
| 0-6 | 20.7\% | 41.1\% | 40.7\% | 52.7\% | 89.9\% | 85.2\% |
| 0-8 | 24.1\% | 53.0\% | 52.4\% | 65.5\% | 94.2\% | 90.5\% |
| 0-10 | 27.6\% | 62.1\% | 61.4\% | 67.3\% | 97.9\% | 94.0\% |

6.38 The results for the inter-peak and PM peak hours follow a similar pattern, with approximately $47 \%$ of the counted links for the inter-peak prior matrix having a GEH value of less the 6 , and an equivalent figure of $42 \%$ for the PM peak matrix. The link flow comparisons for the updated matrices indicate that approximately $91 \%$ and $88 \%$ of the counted links have a GEH value of less than 6 for the inter-peak hour and the PM peak hour respectively.

Table 6.4 Inter-Peak Hour GEH Cumulative Frequency Distributions for the Prior and Estimated Matrices

| GEH <br> Range | Independent <br> Counts | Matrix <br> Estimation <br> Counts | All <br> Counts | Independent <br> Counts | Matrix <br> Estimation <br> Counts | All <br> Counts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $13.8 \%$ | $16.4 \%$ | $16.3 \%$ | $38.2 \%$ | $72.8 \%$ | $68.4 \%$ |
| $0-4$ | $27.6 \%$ | $32.9 \%$ | $32.8 \%$ | $52.7 \%$ | $85.0 \%$ | $80.9 \%$ |
| $0-6$ | $58.6 \%$ | $47.4 \%$ | $47.7 \%$ | $69.1 \%$ | $91.5 \%$ | $88.2 \%$ |
| $0-8$ | $62.1 \%$ | $58.4 \%$ | $58.4 \%$ | $76.4 \%$ | $94.7 \%$ | $92.4 \%$ |
| $0-10$ | $69.0 \%$ | $68.2 \%$ | $68.2 \%$ | $85.5 \%$ | $98.9 \%$ | $97.2 \%$ |

Table 6.5 PM Peak Hour GEH Cumulative Frequency Distributions for the Prior and Estimated M atrices

| GEH <br> Range | Prior M atrix <br> Counts |  |  | Independent <br> Estimation <br> Counts | All <br> Counts | Independent <br> Counts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $3.4 \%$ | $20.7 \%$ | $15.0 \%$ | Matrix <br> Estimation <br> Counts | All <br> Counts |  |
| $0-4$ | $17.2 \%$ | $28.4 \%$ | $28.6 \%$ | $67.3 \%$ | $80.5 \%$ | $74.9 \%$ |
| $0-6$ | $27.6 \%$ | $53.0 \%$ | $42.7 \%$ | $76.4 \%$ | $87.6 \%$ | $82.3 \%$ |
| $0-8$ | $31.0 \%$ | $64.0 \%$ | $53.4 \%$ | $81.8 \%$ | $90.8 \%$ | $85.7 \%$ |
| $0-10$ | $31.0 \%$ | 68.1 | $64.7 \%$ | $83.6 \%$ | $95.0 \%$ | $89.4 \%$ |

## Changes to Trip Length Distributions

6.39 Table 6.6 compares mean trip lengths for movements with an origin or destination in GM and the extended A6 to M60 Area of Influence in the prior and estimated matrices by vehicle type and time period.
6.40 For cars, the mean trip lengths have reduced in the morning and evening time periods, with a reduction of approximately $4.6 \%$ in the AM peak hour and $5.3 \%$ in the PM Peak hour. The inter peak hour has an increase of $8.14 \%$.
6.41 Although the changes in peak period car trip lengths slightly exceed guidance, they are broadly in line with similar changes for other versions of the Saturn model (References 3 and 10). The changes that have been made to the matrices have also brought about a significant improvement in the link flow validation, as described above.
6.42 The LGV matrices exhibit decreases in mean trip lengths the morning and evening time periods, of approximately $8 \%$ and an increase in the inter peak hour of $4 \%$.
6.43 However, the numbers of LGV trips are relatively small, so that these changes are modest in terms of overall netw ork kilometres.

| Table 6.6 | Comparison of Mean Trip Lengths in the Prior and Estimated Matrices for Trips with an Origin or Destination in GM and Extended A6 to M60 Model |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Type | Time Period |  |  |  |  |  |
|  | AM Peak |  | Inter-Peak |  | PM Peak |  |
|  | Mean (km) |  | Mean (km) | \% Change | Mean (km) |  |
| Car | 22.80 | -4.62 | 21.60 | 8.14\% | 23.58 | -5.29 |
| LGV | 25.00 | -1.70 | 24.37 | 4.36\% | 24.78 | -1.66 |
| OGV | 37.49 | -12.82 | 38.01 | -8.94\% | 48.35 | -10.12\% |

6.44 The OGV matrices exhibit the greatest changes in mean trip lengths, with decreases in all three time periods, ranging from approximately $13 \%$ in the AM peak, $9 \%$ in the inter peak hour to $10 \%$ in the PM peak hour. As noted earlier, however, the numbers of OGV trips are relatively small, so these changes are modest in terms of overall netw ork kilometres.
6.45 In summary, the changes to car and LGV trip lengths in all periods are fairly small. Changes in OGV trip lengths are more significant, particularly in the inter-peak and PM peak hours when the numbers of longer distance trips increase. However, the numbers of OGV trips are relatively small. We therefore consider the changes to be acceptable.
6.46 The changes in the trip length distributions are illustrated graphically in Figures 6.3-6.11, for the weekday and Saturday models, for each of the modelled hours.

Comparison of Weekday AM Peak Hour Car Trip Length Distributions







## Comparison of Weekday PM Peak Hour LGV Trip Length

 DistributionsPrior vs Estimated Matrix


## Comparison of Weekday PM Peak Hour OGV Trip Length Distributions

Prior vs Estimated Matrix


## 7. Traffic Flow Validation

## Introduction

7.1 This section presents the link flow validation results for the updated matrices output from the matrix estimation procedure. It summarises the level of network convergence and compares assigned and observed link flows for each of the three modelled time periods using the criteria set out in the Webtag Unit M3.1. Separate results are presented for the matrix estimation counts, for the independent counts and for all counts combined.

## Network Convergence

7.2 Webtag guidance states that 'convergence is the key to robust economic appraisal' because, with a poorly converged base and/or test network, it is impossible to distinguish scheme effects from assignment 'noise'. Consequently, particular efforts were made to ensure that the networks were as highly converged as possible. This was achieved, but at the cost of protracted run times.
7.3 The W ebtag criteria for an acceptable level of network convergence are that:

- Delta should be less than $1 \%$ on the final assignment; and
- More than $90 \%$ of links should have a flow that changes by less than $5 \%$ on the final 4 iterations. Note, however, that HFAS normally adopt stricter criteria, that more than 99\% ( $98.5 \%$ prior to rounding) of links should have a flow change of less than $2 \%$ on the final four iterations.
7.4 Table 7.1 shows the above values for each of the modelled hours. The table indicates that the model meets DM RB convergence criteria, and that the model was well converged in all time periods, with Delta values well below $1 \%$ and the percentage of links with flows changing by less than $2 \%$ being over $98 \%$ in all cases.

Table 7.1 2015 A6 to M60 SATURN M odel Network Convergence Statistics

| Criterion | Target | AM Peak | Inter Peak | PM Peak |
| :---: | :---: | :---: | :---: | :---: |
| Delta | $<1 \%$ | 0.0111 | 0.0079 | 0.0210 |
| Percentage of links with $<2 \%$ flow change on final iteration | >99\% | 99.37 | 99.81 | 99.59 |
| Final iteration-1 |  | 99.42 | 99.80 | 99.52 |
| Final iteration-2 |  | 99.53 | 99.75 | 99.61 |
| Final iteration-3 |  | 98.31 | 99.81 | 99.55 |

## Assignment Validation Guidelines

7.5 The DMRB Volume 12 (reference 1) Table 4.2 sets out validation guidelines for comparing modelled and observed traffic flows based on the level of flow in vehicles per hour (vph). These are:

- For observed flows less than 700 vph, at least $85 \%$ of model flows should be within 100 vph of observations
- For observed flows of between $\mathbf{7 0 0}$ and $\mathbf{2 7 0 0} \mathbf{~ v p h}$, at least $85 \%$ of model flows should be within $15 \%$ of observations; and
- For observed flows greater than $\mathbf{2 7 0 0} \mathbf{~ v p h}$, at least $85 \%$ of model flows should be within 400 vph of observations

These criteria are referred to as the DM RB flow criteria in the text, and as 'All DM RB' in the tables.
7.6 Given that SATURN matrices are generally in units of PCUs per hour, the above criteria are assumed to apply to PCU flows.
7.7 In addition to the flow criteria described above, the DMRB also refers to the GEH statistic, where the guideline is that greater than $85 \%$ of counted links should have a GEH value of less than 5 .
7.8 DM RB also requires that for any cordons and screenlines, the GEH value calculated over the cordon or screenline as a whole should be less than 4 in nearly all cases.
7.9 Finally, the DM RB requires that, taking all counts together, the slope of the best fit regression line should lie in the range 0.9 to 1.1, and the corresponding R-squared value should be greater than 0.95 .

## GEH Statistic

The GEH error statistic is a form of the Chi squared statistic incorporating both relative and absolute errors. The DMRB Volume 12 (reference 1) refers to the GEH statistic, where;

$$
G E H=\sqrt{\frac{(M-C)^{2}}{(M+C) / 2}}
$$

and, $M \quad$ is the modelled flow
C is the observed flow (count).

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907

## Link Flow Comparisons for Matrix Estimation Counts

7.10 This section presents the validation results for sites in that were used during matrix estimation. Results are presented for the sites comprising the 10 cordons/ screenlines used as constraints during the matrix estimation, and for adhoc (TRADS) sites on the M 56/ M 60 M otorways.

## Matrix Estimation Cordons and Screenlines

7.11 In total, counts on 18 (two-way) cordons and screenlines were used during matrix estimation, as illustrated in Figure 6.1 and described below in Table 7.2.

7.12 The validation results for the matrix estimation cordons and screenlines are shown below in Tables 7.3 to 7.5. Results are presented for each of the three time periods for all vehicle types combined as PCUs. For each screenline and direction of travel, the tables show the number of count sites, the total observed flow, the total modelled flow, the difference between the modelled and observed flows and the percentage difference between the modelled and observed flows. The tables also show the screenline GEH value, which the DM RB recommends should be less than 4 in nearly all cases. The percentage of all individual count sites with a GEH value of less than 5 is shown at the bottom of the tables, together with the percentage of sites meeting either the DM RB1, DM RB2 or DM RB3 link flow criteria.
7.13 Table 7.3 compares modelled and observed flows in the AM peak hour. 28 out of 36 (two way) cordons/screenlines having a screenline GEH value of less than 4 and of these 3 marginally exceed 4.0. At the site level, approximately $89 \%$ of the sites have a GEH value of less than 5 , and meet the combined DM RB link flow criteria, which satisfies the DM RB requirements.

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907

Table 7.3 Comparison of AM Peak Hour Modelled and Observed Cordon and Screenline Crossing Flows for Counts used During Matrix Estimation (Actual Flows, All Vehicle Types)

| Cordon | Direction | Number Of Sites | Observed Flow | Modelled Flow | Difference | \% <br> Difference | Screenline GEH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Inbound | 10 | 7028 | 7007 | -21 | -0.3\% | 0.3 |
|  | Outbound | 10 | 6672 | 6432 | -240 | -3.6\% | 3.0 |
| 2 | Inbound | 20 | 14446 | 14251 | -195 | -1.3\% | 3.9 |
|  | Outbound | 20 | 14968 | 15063 | 95 | 0.6\% | 0.8 |
| 3 | Inbound | 22 | 11489 | 11207 | -282 | -2.5\% | 2.6 |
|  | Outbound | 22 | 11596 | 11334 | -262 | -2.3\% | 2.4 |
| 4 | Inbound | 5 | 2277 | 2244 | -33 | -1.5\% | 0.7 |
|  | Outbound | 5 | 1285 | 1190 | -95 | -7.4\% | 2.7 |
| 5 | Inbound | 14 | 10633 | 10003 | -630 | -5.9\% | 6.0 |
|  | Outbound | 14 | 8037 | 8116 | 79 | 1.0\% | 0.9 |
| 6 | Inbound | 8 | 5264 | 4900 | -364 | -6.9\% | 5.5 |
|  | Outbound | 8 | 5326 | 4950 | -376 | -7.1\% | 6.2 |
| 7 | Inbound | 9 | 9760 | 9755 | -5 | -0.1\% | 0.1 |
|  | Outbound | 9 | 10169 | 10009 | -160 | -1.6\% | 1.6 |
| 8 | Inbound | 6 | 877 | 973 | 96 | 11.0\% | 3.2 |
|  | Outbound | 6 | 999 | 1148 | 149 | 14.9\% | 4.5 |
| 9 | Inbound | 6 | 1456 | 1420 | -36 | -2.5\% | 0.9 |
|  | Outbound | 6 | 1582 | 1524 | -58 | -3.7\% | 1.5 |
| 10 | Inbound | 5 | 1229 | 1085 | -144 | -11.7\% | 4.2 |
|  | Outbound | 5 | 1216 | 1228 | 12 | 1.0\% | 0.3 |
| 11 | Northbound | 13 | 11107 | 10685 | -422 | -3.8\% | 4.0 |
|  | Southbound | 13 | 11301 | 10842 | -459 | -4.1\% | 4.4 |
| 12 | Eastbound | 7 | 3017 | 3031 | 14 | 0.5\% | 0.3 |
|  | Westbound | 7 | 4697 | 4770 | 73 | 1.6\% | 1.1 |
| 13 | Northbound | 10 | 9975 | 9688 | -287 | -2.9\% | 2.9 |
|  | Southbound | 9 | 9594 | 9482 | -112 | -1.2\% | 1.1 |
| 14 | Eastbound | 7 | 1317 | 1314 | -3 | -0.2\% | 0.1 |
|  | Westbound | 7 | 2145 | 1887 | -258 | -12.0\% | 4.0 |
| 15 | Eastbound | 5 | 1653 | 1653 | 0 | 0.0\% | 0.0 |
|  | Westbound | 5 | 2030 | 1946 | -84 | -4.1\% | 1.9 |
| 16 | Northbound | 11 | 3275 | 3421 | 146 | 4.5\% | 2.5 |
|  | Southbound | 11 | 3363 | 3342 | -21 | -0.6\% | 0.4 |
| 17 | Northbound | 10 | 4032 | 3800 | -232 | -5.8\% | 6.0 |
|  | Southbound | 10 | 4461 | 4123 | -338 | -7.6\% | 5.5 |
| 18 | Eastbound | 8 | 2058 | 1975 | -83 | -4.0\% | 1.8 |
|  | Westbound | 8 | 2587 | 2522 | -65 | -2.5\% | 1.3 |

## Notes:

Percentage of all sites with GEH < $5=89.3 \%$
Percentage of all sites meeting DM RB flow criteria $=89.1 \%$
7.14 Table 7.4 compares modelled and observed screenline crossing flows in the inter-peak hour in PCUs. Overall, the comparisons are good, with 28 out of 36 (two way) cordons/screenlines having a screenline GEH value of less than 4 and of these 4 marginally exceed 4.0 . At the site level, approximately $90 \%$ of sites have a GEH value of less than 5 and meet the combined DM RB link flow criteria, which is well within the DM RB guidelines.
7.15 The screenline with the greatest difference in modelled flow to counts is the Prestbury to Whaley Bridge screenline. This screenline is remote to the proposed scheme and there are difficulties identifying short distance trips particularly in more rural areas. Furthermore, the spatial accuracy which phone locations can be determined is dependent on antenna/cell tower coverage. Locations should be most accurate in areas with a high density of cell towers, typically comprising town centres and areas with high population, but will be less accurate elsewhere particularly in more rural areas.

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907

| Table 7.4 | Comparison of Inter Peak Hour M odelled and Observed Cordon and Screenline Crossing Flows for Counts used During Matrix Estimation (Actual Flows, All Vehicle Types) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cordon | Direction | Number Of Sites | Observed Flow | Modelled <br> Flow | Difference | \% <br> Difference | Screenline GEH |
| 1 | Inbound | 10 | 5744 | 5794 | 50 | 0.9\% | 0.7 |
|  | Outbound | 10 | 5772 | 5713 | -59 | -1.0\% | 0.8 |
| 2 | Inbound | 20 | 12023 | 11970 | -53 | -0.4\% | 0.5 |
|  | Outbound | 20 | 11971 | 11979 | 8 | 0.1\% | 0.1 |
| 3 | Inbound | 22 | 11716 | 11120 | -596 | -5.1\% | 3.9 |
|  | Outbound | 22 | 11990 | 11419 | -571 | -4.8\% | 4.1 |
| 4 | Inbound | 5 | 1550 | 1432 | -118 | -7.6\% | 3.1 |
|  | Outbound | 5 | 1393 | 1265 | -128 | -9.2\% | 3.5 |
| 5 | Inbound | 14 | 9511 | 9090 | -421 | -4.4\% | 6.0 |
|  | Outbound | 14 | 9585 | 9222 | -363 | -3.8\% | 4.4 |
| 6 | Inbound | 8 | 5357 | 5158 | -199 | -3.7\% | 2.7 |
|  | Outbound | 8 | 5512 | 5333 | -179 | -3.2\% | 4.1 |
| 7 | Inbound | 9 | 10238 | 10666 | 428 | 4.2\% | 4.2 |
|  | Outbound | 9 | 10182 | 10314 | 132 | 1.3\% | 1.3 |
| 8 | Inbound | 6 | 602 | 701 | 99 | 16.5\% | 3.9 |
|  | Outbound | 6 | 638 | 697 | 59 | 9.3\% | 2.3 |
| 9 | Inbound | 6 | 1798 | 1692 | -106 | -5.9\% | 2.5 |
|  | Outbound | 6 | 1823 | 1704 | -119 | -6.5\% | 2.8 |
| 10 | Inbound | 5 | 998 | 825 | -173 | -17.3\% | 4.7 |
|  | Outbound | 5 | 981 | 874 | -107 | -10.9\% | 3.5 |
| 11 | Northbound | 13 | 11033 | 10827 | -206 | -1.9\% | 2.0 |
|  | Southbound | 13 | 10947 | 11053 | 106 | 1.0\% | 1.0 |
| 12 | Eastbound | 7 | 4049 | 4113 | 64 | 1.6\% | 1.0 |
|  | Westbound | 7 | 4207 | 4153 | -54 | -1.3\% | 0.8 |
| 13 | Northbound | 10 | 9067 | 9123 | 56 | 0.6\% | 0.6 |
|  | Southbound | 9 | 8509 | 8466 | -43 | -0.5\% | 0.5 |
| 14 | Eastbound | 7 | 1485 | 1391 | -94 | -6.3\% | 2.5 |
|  | Westbound | 7 | 1476 | 1407 | -69 | -4.7\% | 1.8 |
| 15 | Eastbound | 5 | 1332 | 1154 | -178 | -13.4\% | 4.0 |
|  | Westbound | 5 | 1307 | 1181 | -126 | -9.6\% | 3.6 |
| 16 | Northbound | 11 | - 2678 | 2627 | -51 | -1.9\% | 1.0 |
|  | Southbound | 11 | 2630 | 2560 | -70 | -2.7\% | 1.4 |
|  | Northbound | 10 | 3296 | 2435 | -861 | -26.1\% | 16.1 |
|  | Southbound | 10 | 3192 | 2470 | -722 | -22.6\% | 13.6 |
| 18 | Eastbound | 8 | 2218 | 2277 | 59 | 2.7\% | 1.2 |
|  | Westbound | 8 | 2276 | 2256 | -20 | -0.9\% | 0.4 |

## Notes:

## Percentage of all sites with GEH < $5=89.9$

Percentage of all sites meeting DM RB flow criteria $=91.0$
7.16 Table 7.5 compares modelled and observed screenline crossing flows in the PM peak hour for all vehicles combined as PCUs. In total, 26 out of 36 of the (two way) cordons/ screenlines have a GEH value of less than 4 but of these 5 marginally exceed 4.0. At the site level, approximately $88 \%$ of the sites have a GEH value of less than 5 , with $91 \%$ of the sites meeting the combined DM RB link flow criteria.

Highways Forecasting and Analytical Services
DRAFT A6 to M60 Relief Road
A6M 60 LM VR
M ay 2017
2224-01 Report 1907

Table 7.5 Comparison of PM Peak Hour Modelled and Observed Cordon and Screenline Crossing Flows for Counts used During Matrix Estimation (Actual Fows, All Vehicle Types)

| Cordon | Direction | Number Of Sites | Observed Flow | Modelled Flow | Difference | Difference | Screenline GEH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Inbound | 10 | 7626 | 7463 | -163 | -2.1\% | 1.9 |
|  | Outbound | 10 | 8452 | 8043 | -409 | -4.8\% | 4.5 |
| 2 | Inbound | 20 | 17440 | 16990 | -450 | -2.6\% | 3.4 |
|  | Outbound | 20 | 16281 | 16634 | 353 | 2.2\% | 2.8 |
| 3 | Inbound | 22 | 14736 | 14176 | -560 | -3.8\% | 4.7 |
|  | Outbound | 22 | 15094 | 14579 | -515 | -3.4\% | 4.2 |
| 4 | Inbound | 5 | 1686 | 1625 | -61 | -3.6\% | 1.5 |
|  | Outbound | 5 | 2758 | 2525 | -233 | -8.4\% | 4.0 |
| 5 | Inbound | 14 | 10712 | 10365 | -347 | -3.2\% | 3.1 |
|  | Outbound | 14 | 12691 | 12002 | -689 | -5.4\% | 3.8 |
| 6 | Inbound | 8 | 6313 | 6001 | -312 | -4.9\% | 4.1 |
|  | Outbound | 8 | 6857 | 6665 | -192 | -2.8\% | 3.5 |
| 7 | Inbound | 9 | 13095 | 14173 | 1078 | 8.2\% | 3.0 |
|  | Outbound | 9 | 14337 | 13551 | -786 | -5.5\% | 4.1 |
| 8 | Inbound | 6 | 1164 | 1347 | 183 | 15.7\% | 5.2 |
|  | Outbound | 6 | 1011 | 1093 | 82 | 8.1\% | 2.5 |
| 9 | Inbound | 6 | 2339 | 2136 | -203 | -8.7\% | 3.7 |
|  | Outbound | 6 | 2198 | 2195 | -3 | -0.1\% | 0.1 |
| 10 | Inbound | 5 | 1477 | 1312 | -165 | -11.2\% | 3.8 |
|  | Outbound | 5 | 1453 | 1251 | -202 | -13.9\% | 3.7 |
| 11 | Northbound | 13 | 15391 | 14510 | -881 | -5.7\% | 4.1 |
|  | Southbound | 13 | 14573 | 14111 | -462 | -3.2\% | 3.8 |
| 12 | Eastbound | 7 | 5680 | 5714 | 34 | 0.6\% | 0.5 |
|  | Westbound | 7 | 4573 | 4544 | -29 | -0.6\% | 0.4 |
| 13 | Northbound | 10 | 11305 | 11466 | 161 | 1.4\% | 1.5 |
|  | Southbound | 9 | 11680 | 11375 | -305 | -2.6\% | 2.8 |
| 14 | Eastbound | 7 | 2403 | 2176 | -227 | -9.5\% | 4.7 |
|  | Westbound | 7 | 1653 | 1567 | -86 | -5.2\% | 2.1 |
| 15 | Eastbound | 5 | 1948 | 1828 | -120 | -6.2\% | 2.8 |
|  | Westbound | 5 | 1829 | 1708 | -121 | -6.6\% | 2.9 |
| 16 | Northbound | 11 | 4101 | 4191 | 90 | 2.2\% | 1.4 |
|  | Southbound | 11 | 3748 | 3889 | 141 | 3.8\% | 2.3 |
| 17 | Northbound | 10 | 5123 | 4777 | -346 | -6.8\% | 6.0 |
|  | Southbound | 10 | 4355 | 4085 | -270 | -6.2\% | 7.0 |
| 18 | Eastbound | 8 | 3390 | 3406 | 16 | 0.5\% | 0.3 |
|  | Westbound | 8 | 2830 | 2830 | 0 | 0.0\% | 0.0 |

## Notes:

Percentage of all sites with GEH <5 = 87.1
Percentage of all sites meeting DM RB flow criteria $=87.6$

## Matrix Estimation Motorway Sites

7.17 Table 7.6 compares modelled and observed flows for the matrix estimation sites on the M 56 and M60 motorways for all vehicles combined as PCUs, for each of the modelled time periods. The table shows the number of sites, the total observed flow, the total modelled flow, the difference
between the modelled and observed flows and the percentage difference between the modelled and observed flows. The table also shows the percentage of sites with a GEH value of less than 5. The figures in the column headed 'All DMRB' give the percentage of counted links that meet either the DM RB1, 2 or 3 link flow criteria.
7.18 In general, the comparisons are good, with greater than $89 \%$ of the sites having a GEH value of less than 5 in all time periods. The comparisons against the DM RB link flow criteria are also very good, with $93 \%$ of sites achieving the required standard in the AM peak hour, and $90 \%$ and $89 \% \%$ of the sites meeting the standard in the inter-peak and PM peak hours respectively.

Table 7.6 Link Flow Comparisons for M otorway Counts used During Matrix Estimation (Actual Flows, All Vehicles)

| Time Period <br> Period | Number <br> Of Sites | Observed <br> Flow | Modelled <br> Flow | Difference | Difference | $\%$ <br> GEH $<5$ | $\%$ <br> All DM RB |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | 227 | 472310 | 476761 | 4451 | 0.9 | 91 | 93 |
| Inter Peak | 227 | 594274 | 588793 | -5481 | -0.9 | 89 | 90 |
| PM Peak | 227 | 709903 | 709113 | -790 | -0.1 | 89 | 89 |

## Link Flow Comparisons for All Matrix Estimation Counts

7.19 Table 7.7 compares modelled and observed flows for all of the matrix estimation counts for each of the modelled time periods. These counts comprise the matrix estimation cordon and screenline counts plus the 36 TRADS counts on the M 56 and M 60 motorways in the A6 M 60 area. It should be noted that where a cordon or screenline uses the same count, that count is only included once in the overall number of sites.
7.20 As a whole, the comparisons are very good, with $89 \%$ of the sites having a GEH value of less than 5 in the AM peak hour, and 89\% of sites meeting the DM RB flow criteria. The results for the inter-peak hour are slightly better, with approximately $90 \%$ of sites having a GEH value of less than 5 and $91 \%$ meeting the DM RB flow criteria. The PM peak hour has approximately $87 \%$ of sites having a GEH value of less than 5 and approximately $88 \%$ meeting the DM RB flow criteria.
7.21 At an aggregate level, the modelled flows are within $1.3 \%$ of the counted flows in the AM peak and $1.9 \%$ inter-peak hours, and are within approximately $1.7 \%$ of the counted flows in PM peak hour.

Table 7.7 Link Flow Comparisons for All Matrix Estimation Counts (Actual Flows, All Vehicles)

| Time Period <br> Period | Number <br> Of Sites | Observed <br> Flow | M odelled <br> Flow | Difference | $\%$ <br> Difference | $\%$ <br> GEH < $<5$ | $\%$ <br> All DM RB |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | 1235 | 960895 | 948236 | -12569 | -1.3 | 89 | 89 |
| Inter-Peak | 1235 | 1055282 | -19470 | -19470 | -1.9 | 90 | 91 |
| PM Peak | 1235 | 1324582 | 1302865 | -21897 | -1.7 | 87 | 88 |

## Link Flow Comparisons for Independent Counts

7.22 This section presents the assignment validation results for the independent counts that were reserved to check the accuracy of the calibrated model. Separate results are presented for the A34 screenline, the adhoc counts in the Area of Influence of the scheme and for all counts combined.

## Independent Screenline North of M60

7.23 Table 7.8 compares modelled and observed flows for the A34 screenline, which south of the M 60 from Bredbury to Heald Green to intercept movements likely to use the proposed scheme. Results are presented for all vehicles combined for each of the modelled time periods.
7.24 The table shows a reasonable agreement between modelled and observed flows.
7.25 The percentage difference between the modelled and observed flows ranges from $+2.2 \%$ in the southbound direction in the inter peak hour to $-4.5 \%$ in the southbound direction in the eveningpeak hour.

| Table 7.8 | Link Flow Comparisons for the A34 Screenline (Actual Flows, All Vehicles) |  |  |  |  |
| :--- | :--- | ---: | ---: | ---: | ---: |
| Time | Direction | Observed | M odelled |  |  |
| Period |  | Flow | Flow | Difference | Difference | \(\left.\begin{array}{c}Screenline <br>

GEH\end{array}\right]\)
7.26 The overall validation across the independent screenline is reasonable in both directions with the screenline GEH under 5.0 in all time periods

## All Independent Counts

7.27 Table 7.9 compares modelled and observed flows for all of the independent sites combined. Separate figures are presented for each of the modelled hours, for all vehicle flows expressed in PCUs.

Table 7.9 Link Flow Comparisons for All Independent Counts (Actual Flows, All Vehicles)

$\left.$| Time Period <br> Period | Number <br> Of Sites | Observed <br> Flow | M odelled <br> Flow | Difference |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | | $\%$ |
| :---: |
| Difference |$\quad$| $\%$ |
| :---: |
| GEH <5 |$\quad$| $\%$ |
| :---: |
| All DM RB | \right\rvert\,

7.28 Overall, the comparisons are fair in the morning and interpeak, with the percentage of sites with a GEH value of less than 5 range from $72 \%$ in the interpeak period to approximately $65 \%$ in the remaining time periods. The percentage of links meeting the combined DM RB link flow criteria ranges from $66 \%$ in the AM peak hour, $72 \%$ in the PM peak hour to $75 \%$ in the inter-peak. The percentage differences between the range from an under-assignment of $2 \%$ in the AM peak hour, to an over-assignment of $1.5 \%$ in the inter peak.

## Regression Analysis

7.29 The regression parameters for the line $y=a x$ are shown in Table 7.11. As noted in earlier, the DMRB recommends that the slope of the line should lie in the range 0.9 to 1.1 , and the corresponding R -squared value should be greater than 0.95 .
7.30 The table shows that the slopes of the regression lines and the R-squared values are comfortably within the guideline ranges specified in the DM RB for all three time periods.

| Table 7.11 | Regression Line Statistics for All Counted Links (All Vehicles) |  |  |
| :---: | :---: | :---: | :---: |
| Time Period | Parameter | $\mathrm{Y}=\boldsymbol{R}$ | Within DM RB <br> Range |
| AM Peak Hour |  | Slope | 1.012 |
| Yes |  |  |  |
|  | R-squared | 0.988 | Yes |
| Inter-Peak Hour | Slope | 0.978 | Yes |
|  | R-squared | 0.996 | Yes |
| PM Peak Hour | Slope | 0.926 | Yes |
|  | R-squared | 1.002 | Yes |

7.31 Regression Plots of modelled versus observed flow for the matrix estimation and the independent count set are shown in Figures 7.1 to 7.6 .


Figure 7.1: AM Peak Regression Analysis of M odelled Versus Observed Flow - M atrix Estimation Count Set


Figure 7.2: AM Peak Regression Analysis of M odelled Versus Observed Flow - Independent Count Set


Figure 7.3: Inter-peak Peak Regression Analysis of M odelled Versus Observed Flow - Matrix Estimation Count Set


Figure 7.4: Inter-peak Peak Regression Analysis of Modelled Versus Observed Flow - Independent Count Set


Figure 7.5: PM Peak Regression Analysis of Modelled Versus Observed Flow - Matrix Estimation Count Set


Figure 7.6: PM Peak Regression Analysis of M odelled Versus Observed Flow - Independent Count Set

## 8. Journey Time Validation

## Introduction

8.1 Modelled and observed journey times have been compared on a selection of radial and orbital routes within the study area, as shown in Table 8.1 and illustrated in Figure 8.1. The routes are designed to replicate typical journeys within the Area of Influence of the scheme.
8.2 The observed journey times have been estimated using GPS data for 2015/16 from the Trafficmaster database. This information is collected on behalf of the Department for Transport by Trafficmaster PLC, and provides information about average vehicle speeds on roads across the UK for vehicles fitted with GPS devices. The information in the database has been processed by HFAS to exclude observations collected during school and national holidays, and to calculate average times for non-stopping vehicles (i.e. excluding buses and taxis) for standardized time periods. For the purpose of this analysis, the modelled times have been compared with observed times collected during for the morning peak hour 0800-0900, the evening peak hour 1700-1800 and the inter-peak period 0930-1430.
8.3 Taken together, the journey time routes cover approximately 590 km of the highway network in the A6 to M60 Area of Influence.

## Journey Time Validation Guidelines

8.4 The DM RB requirement for journey time validation is that modelled times should be within $15 \%$ (or 1 minute if this is higher) of the observed time on more than $85 \%$ of routes.
8.5 It should be noted, however, that paragraph 11.4.9 of the Traffic Appraisal Manual Volume 12) (reference 1) states:
"In congested conditions, where the journey times are flow dependent, the assignment package will provide estimates of link speeds and journey times for different times of day. These are not as accurate as the predictions of flows, as they are based on theoretical speed/flow relations that may not be the most appropriate for all parts of the network, and the standards for acceptance will generally be lower. Research has shown that, as long as the estimation of total travel time is unbiased, an empirically determined $95 \%$ confidence interval of $H-20 \%$ can be taken to signify that the journey times are adequately modelled."

This range is also used for comparison in the following paragraphs.
8.6 Finally, it should also be noted that the modelled times represent the sum of the link travel times comprising each route, and therefore include flow-weighted delays for each of turns at the downstream ends of the constituent links. As a consequence, the route times do not necessarily represent the time taken to travel from the start point of the route to the routes end point, (as would be calculated using the SATURN ‘Joy Ride’ facility, for example), as this would only include the turn delays for a specific set of movements. Any differences should, however, be small. (This approach has been adopted for compatibility with the Trafficmaster data, and its procedure for allocating turning delays to links.)

| Route No. | Description | Direction | Route Length M odelled KM |
| :---: | :---: | :---: | :---: |
| 1 | A6 Chapel to Heaton M oor | NW | 8.7 |
|  | A6 Heaton M oor to Chapel | SE | 8.7 |
| 2 | A537 Knutsford to M acclesfield | E | 16.4 |
|  | A537 M acclesfield to Knutsford | W | 16.4 |
| 3 | B5085 Knutsford to Alderley Edge | E | 10.2 |
|  | B5085 Alderley Edge to Knutsford | W | 10.2 |
| 4 | B5087 M acclesfield to Alderley Edge | NW | 6.6 |
|  | B5087 Alderley Edge to M acclesfield | SE | 6.6 |
| 5 | M 56 Manchester Airport to West Didsbury | N | 7.3 |
|  | M 56 West Didsbury to M anchester Airport | S | 6.8 |
| 6 | B5166 Wilmslow to Northenden | N | 10 |
|  | B5166 Northenden to Wilmslow | S | 10 |
| 7 | M 56 J8 to J5 | E | 8.4 |
|  | M 56 J5 to J8 | W | 8.4 |
| 8 | A5102 Wilmslow to Bramhall | NE | 7.6 |
|  | A5102 Bramhall to Wilmslow | SW | 7.6 |
| 9 | A34 Alderley Edge to East Didsbury | N | 14.4 |
|  | A34 East Didsbury to Alderley Edge | S | 14.3 |
| 10 | A523 Prestbury to Hazel Grove | N | 10.1 |
|  | A523 Hazel Grove to Prestbury | S | 10 |
| 11 | A555 M AELR Poynton to M anchester Airport | W | 14.4 |
|  | A555 M AELR M anchester Airport to Poynton | E | 14.4 |
| 12 | A538 Prestbury to Hale | NW | 22.1 |
|  | A538 Hale to Prestbury | SE | 22.1 |
| 13 | M60 J6 to J24 | AC | 17 |
|  | M 60 J24 to J 6 | CW | 17.2 |
| 14 | Heald Green to Cheadle Heath | NE | 5.2 |
|  | Cheadle Heath to Heald Green | SW | 5.2 |
| 15 | A5149/3 Cheadle Hulme to Hazel Grove | E | 5.8 |
|  | A5143/9 Hazel Grove to Cheadle Hulme | W | 5.8 |
| 16 | Buxton Old Road / Higher Lane | SB | 6 |
|  | Buxton Old Road / Higher Lane | NB | 6 |
| 17 | B5470 Chapel To M acclesfield | SB | 16.5 |
|  | B5470 M acclesfield To Chapel | NB | 16.5 |
| 18 | B5090 / Bakestonedale Rd | WB | 8.1 |
|  | B5090 / Bakestonedale Rd | EB | 8.1 |
| 19 | Bakestonedale Rd/ Brookledge Lane / M ill Lane | WB | 9.7 |
|  | Bakestonedale Rd/ Brookledge Lane / M ill Lane | EB | 9.7 |
|  | B5358 - | NB | 8.9 |
| 2021 | B5358 | SB | 8.9 |
|  | Roundy Lane / M iddlewood Rd/ Waterloo Rd | NB | 7.3 |
| 22 | Roundy Lane / M iddlewood Rd/ Waterloo Rd | SB | 7.3 |
|  | B5465 / A626 | NB | 2.1 |
|  | B5465 / A626 | SB | 2.1 |
| 23 | A626 | NB | 4.9 |
|  | A626 | SB | 4.9 |
| 24 | A560 | NB | 3.9 |
|  | A560 | SB | 3.9 |
| 25 | A6017 | NB | 3.9 |
|  | A6017 | SB | 3.9 |
| 26 | A560 / A627 | NB | 6.6 |
|  | A560 / A627 | SB | 6.6 |
| 27 | A626 | NB | 11.9 |
|  | A626 | SB | 11.9 |
| 28 | A560 | NB | 4.9 |
|  | A560 | SB | 4.9 |
| 29 | A627 | NB | 6.4 |
|  | A627 | SB | 6.4 |
| 30 | A560 | NB | 7.1 |
|  | A560 | SB | 7.1 |
| 31 | B6104 | NB | 5.8 |
|  | B6104 | SB | 5.8 |



## AM Peak Hour Journey Time Validation Results

8.7 Table 8.2 compares modelled and observed journey times in the AM peak hour along the 42 journey time routes. In total, journey times on 54 out of 62 (or approximately $87 \%$ ) of the routes meet DMRB journey time criteria that modelled times should be within $15 \%$ of observed times. The greatest differences between modelled and observed times are for routes on the M56 and M60, where the modelled times are too low on the M60 anticlockwise and too fast on the M 60 clockwise and on the M 56 Eastbound.
8.8 Considering all of the routes together, the total modelled time is approximately $8.0 \%$ lower than the total observed time, which is within the DMRB criteria, but suggests that the modelled speeds are slightly too low in general.

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
M ay 2017
2224-01 Report 1907

| Table 8.2 | Am Peak Journey Times |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Route | Route Description | Dir | Observed | Modelled | Modelled- | \% | Within |
| Number |  |  | Time | Time | Observed | Error | DMRB |
| 1A | A6 Chapel to Heaton M oor | NB | 54.4 | 48.9 | -5.5 | 10.0 | Y |
| 1B | A6 Heaton M oor To Chapel | SB | 43.9 | 48.5 | 4.6 | 10.6 | Y |
| 2A | A537 Knutsford To M acclesfield | E | 25.3 | 22.1 | -3.2 | 12.5 | Y |
| 2B | A537 M acclesfield To Knutsford | W | 23.6 | 20.7 | -2.9 | 12.3 | Y |
| 3A | B5085 Knutsford To Alderley Edge | E | 14.6 | 14.6 | 0.0 | 0.1 | Y |
| 3B | B5085 Alderley Edge To Knutsford | W | 15.0 | 13.4 | -1.6 | 10.6 | Y |
| 4A | B5087 M acclesfield To Alderley Edge | NW | 7.8 | 6.9 | -0.9 | 11.0 | Y |
| 4B | B5087 Alderley Edge To M acclesfield | SE | 7.2 | 6.8 | -0.4 | 6.0 | Y |
| 5A | M 56 M anchester Airport To West Didsbury | N | 13.1 | 6.6 | -6.5 | 49.5 | N |
| 5B | M 56 West Didsbury To M anchester Airport | S | 5.9 | 6.4 | 0.6 | 9.5 | Y |
| 6A | B5166 Wilmslow to Northenden | N | 17.4 | 17.1 | -0.2 | 1.4 | Y |
| 6B | B5166 Northenden to Wilmslow | S | 18.1 | 16.5 | -1.6 | 9.0 | Y |
| 7A | M 56 J 8 to J5 | E | 8.9 | 6.2 | -2.7 | 30.1 | N |
| 7B | M 56 J 5 to J8 | W | 5.2 | 5.8 | 0.6 | 11.7 | Y |
| 8A | A5102 Wilmslow to Bramhall | NE | 12.2 | 12.3 | 0.2 | 1.5 | Y |
| 8B | A5102 Bramhall to Bramhall | SW | 16.4 | 14.2 | -2.2 | 13.3 | Y |
| 9A | A34 Alderley Edge to East Didsbury | N | 27.0 | 28.2 | 1.2 | 4.6 | Y |
| 9B | A34 East Didsbury to Alderley Edge | S | 26.0 | 24.6 | -1.4 | 5.5 | Y |
| 10A | A523 Prestbury to Hazel Grove | N | 17.1 | 18.1 | 1.0 | 6.0 | Y |
| 10B | A523 Hazel Grove to Prestbury | 5 | 23.9 | 20.5 | -3.4 | 14.1 | Y |
| 11A | A555 M AELR Poynton to M anchester Airport | W | 25.5 | 24.7 | -0.7 | 2.9 | Y |
| 11B | A555 M anchester Airport to Poynton | E | 24.0 | 25.5 | 1.5 | 6.4 | Y |
| 12A | A538 Prestbury to Hazel Grove | NW | 38.4 | 33.0 | -5.4 | 14.0 | Y |
| 12B | A538 Hazel Grove to Prestbury | SE | 40.9 | 36.2 | -4.7 | 11.5 | Y |
| 13A | M 60 J 6 to J24 | AC | 12.5 | 15.7 | 3.3 | 26.1 | N |
| 13B | M 60 J24 to J6 | CW | 22.8 | 14.4 | -8.4 | 36.9 | N |
| 14A | Heald Green to Cheadle Heath | NE | 13.0 | 14.1 | 1.1 | 8.8 | Y |
| 14B | Cheadle Heath to Heald Green | SW | 14.9 | 14.2 | -0.7 | 4.8 | Y |
| 15A | A5149/3 Cheadle Hulme to Hazel Grove | E | 10.8 | 12.1 | 1.3 | 12.0 | Y |
| 15B | A5143/9 Hazel Grove to Cheadle Hulme | W | 18.9 | 11.1 | -7.8 | 41.3 | N |
| 16A | Buxton Old Rd/ Higher Lane | SB | 7.6 | 7.6 | -0.1 | 0.8 | Y |
| 16B | Buxton Old Rd / Higher Lane | NB | 7.9 | 7.5 | -0.4 | 5.0 | Y |
| 17A | B5470 Chapel to M acclesfield | SB | 22.2 | 20.7 | -1.6 | 7.0 | Y |
| 17B | B5470 M acclesfield to Chapel | NB | 22.0 | 20.4 | -1.6 | 7.2 | Y |
| 18A | B5090 / Bakestonedale Rd | WB | 12.3 | 11.8 | -0.4 | 3.4 | Y |
| 18B | B5090 / Bakestonedale Rd | EB | 12.2 | 11.7 | -0.5 | 4.3 | Y |
| 19A | Bakestonedale Rd/ Brookledge Lane / M ill Lane | WB | 15.4 | 13.5 | -1.9 | 12.1 | Y |
| 19B | Bakestonedale Rd/ Brookledge Lane / M ill Lane | EB | 12.4 | 13.1 | 0.6 | 5.0 | Y |
| 20A | B5358 | NB | 13.2 | 14.0 | 0.9 | 6.5 | Y |
| 20B | B5358 | SB | 15.1 | 16.2 | 1.1 | 7.3 | Y |


| 21A | Roundy Lane/ M iddlewood Rd / W aterloo Rd | NB | 13.1 | 13.3 | 0.2 | 1.2 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21B | Roundy Lane / M iddlewood Rd / W aterloo Rd | SB | 12.5 | 12.2 | -0.3 | 2.4 | Y |
| 22A | B5465 / A626 | NB | 5.5 | 5.9 | 0.4 | 7.7 | Y |
| 22B | B5465 / A626 | SB | 7.9 | 7.0 | -0.9 | 10.9 | Y |
| 23A | A626 | NB | 20.1 | 18.9 | -1.2 | 6.1 | Y |
| 23B | A626 | SB | 11.6 | 11.6 | 0.0 | 0.3 | Y |
| 24A | A560 | NB | 7.1 | 8.1 | 1.0 | 14.3 | Y |
| 24B | A560 | SB | 8.8 | 9.4 | 0.6 | 6.6 | Y |
| 25A | A6017 | NB | 7.8 | 7.0 | -0.8 | 10.1 | Y |
| 25B | A6017 | SB | 12.9 | 6.3 | -6.6 | 51.0 | N |
| 26A | A560 / A627 | NB | 14.8 | 14.3 | -0.6 | 3.8 | Y |
| 26B | A560 / A627 | SB | 23.9 | 15.4 | -8.5 | 35.5 | N |
| 27A | A626 | NB | 19.3 | 16.5 | -2.8 | 14.6 | Y |
| 27B | A626 | SB | 24.0 | 17.7 | -6.3 | 26.2 | N |
| 28A | A560 | NB | 7.0 | 8.1 | 1.0 | 14.9 | Y |
| 28B | A560 | SB | 6.6 | 6.6 | 0.0 | 0.0 | Y |
| 29A | A627 | NB | 13.6 | 12.5 | -1.1 | 8.3 | Y |
| 29B | A627 | SB | 20.0 | 17.5 | -2.5 | 12.3 | Y |
| 30A | A560 | NB | 23.0 | 20.1 | -2.9 | 12.7 | Y |
| 30B | A560 | SB | 28.4 | 25.3 | -3.1 | 10.9 | Y |
| 31A | B6104 | NB | 16.6 | 14.5 | -2.1 | 12.4 | Y |
| 31B | B6104 | SB | 11.8 | 11.2 | -0.7 | 5.5 | Y |
| Total |  |  | 1061.1 | 975.6 | -85.5 | -8.0\% |  |
| Number of routes satisfying DMRB Criteria = 54 out of 62 (87\%) |  |  |  |  |  |  |  |

## Inter-Peak Hour Journey Time Validation Results

8.9 Table 8.3 compares modelled and observed journey times in the inter-peak hour along the 42 journey time routes.
8.10 Overall, the comparisons are good, with 56 out of $62(90 \%)$ of the routes meeting the DM RB criteria of $+/-15 \%$. Considering all of the routes together, the total modelled time is $2.8 \%$ lower than the observed time, which is within the DM RB criteria, but suggests that the modelled speeds are slightly faster in general.
8.11 The greatest difference in the observed journey time compared to the modelled journey time is on the route between Cheadle Hulme and Whaley Bridge which

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907

| Table 8,3 | Inter Peak Journey Times |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Route | Route Description | Dir | Observed | Modelled | Modelled- | \% | Within |
| Number |  |  | Time | Time | Observed | Error | DMRB |
| 1A | A6 Chapel to Heaton M oor | NB | 41.3 | 44.6 | 3.3 | 8.1 | Y |
| 1B | A6 Heaton M oor To Chapel | SB | 39.5 | 42.5 | 2.9 | 7.4 | Y |
| 2A | A537 Knutsford To M acclesfield | E | 19.5 | 20.0 | 0.5 | 2.8 | Y |
| 2B | A537 M acclesfield To Knutsford | W | 18.9 | 20.0 | + 1.1 | 6.0 | Y |
| 3A | B5085 Knutsford To Alderley Edge | E | 13.4 | 12.5 | -0.9 | 6.7 | Y |
| 3B | B5085 Alderley Edge To Knutsford | W | 13.5 | 12.3 | -1.2 | 9.0 | Y |
| 4A | B5087 M acclesfield To Alderley Edge | NW | 7.5 | 6.5 | -1.0 | 13.2 | Y |
| 4B | B5087 Alderley Edge To M acclesfield | SE | 7.3 | 6.4 | -0.9 | 12.4 | Y |
| 5A | M 56 M anchester Airport To West Didsbury | N | 5.6 | 5.8 | 0.3 | 4.5 | Y |
| 5B | M 56 West Didsbury To M anchester Airport | S | 5.3 | 5.3 | 0.0 | 0.3 | Y |
| 6A | B5166 Wilmslow to Northenden | N | 15.5 | 15.2 | -0.3 | 2.2 | Y |
| 6B | B5166 Northenden to Wilmslow | S | 15.2 | 13.6 | -1.6 | 10.7 | Y |
| 7A | M 56 J 8 to J5 | E | 5.2 | 4.9 | -0.3 | 5.8 | Y |
| 7B | M 56 J 5 to J8 | W | 4.7 | 5.0 | 0.2 | 4.4 | Y |
| 8A | A5102 Wilmslow to Bramhall | NE | 11.6 | 10.4 | -1.2 | 10.3 | Y |
| 8B | A5102 Bramhall to Wilmslow | SW | 12.1 | 10.1 | -2.0 | 16.7 | N |
| 9A | A34 Alderley Edge to East Didsbury | N | 16.9 | 18.0 | 1.1 | 6.7 | Y |
| 9B | A34 East Didsbury to Alderley Edge | 5 | 17.4 | 15.7 | -1.8 | 10.1 | Y |
| 10A | A523 Prestbury to Hazel Grove | N | 15.1 | 14.5 | -0.6 | 4.1 | Y |
| 10B | A523 Hazel Grove to Prestbury | S | 14.3 | 13.9 | -0.4 | 2.9 | Y |
| 11A | A555 M AELR Poynton to M anchester Airport | W | 20.5 | 20.1 | -0.5 | 2.3 | Y |
| 11B | A555 M anchester Airport to Poynton | E | 21.4 | 21.4 | 0.0 | 0.2 | Y |
| 12A | A538 Prestbury to Hazel Grove | NW | 31.9 | 28.9 | -3.0 | 9.3 | Y |
| 12B | A538 Hazel Grove to Prestbury | SE | 33.0 | 30.8 | -2.1 | 6.5 | Y |
| 13A | M 60 J6toJ24 | AC | 10.4 | 12.2 | 1.8 | 17.4 | N |
| 13B | M 60J24 to J6 | CW | 10.8 | 11.9 | 1.1 | 10.3 | Y |
| 14A | Heald Green to Cheadle Heath | NE | 9.9 | 10.0 | 0.1 | 1.2 | Y |
| 14B | Cheadle Heath to Heald Green | SW | 9.7 | 11.2 | 1.5 | 15.1 | N |
| 15A | A5149/3 Cheadle Hulme to Hazel Grove | E | 10.2 | 9.2 | -1.0 | 9.7 | Y |
| 15B | A5143/9 Hazel Grove to Cheadle Hulme | W | 10.2 | 9.7 | -0.5 | 5.4 | Y |
| 16A | Buxton Old Rd / Higher Lane | SB | 7.7 | 7.6 | -0.1 | 1.9 | Y |
| 16B | Buxton Old Rd / Higher Lane | NB | 7.8 | 7.5 | -0.3 | 3.5 | Y |
| 17A | B5470 Chapel to M acclesfield | SB | 20.8 | 20.1 | -0.7 | 3.6 | Y |
| 17B | B5470 M acclesfield to Chapel | NB | 21.0 | 20.2 | -0.8 | 3.9 | Y |
| 18A | B5090 / Bakestonedale Rd | WB | 11.9 | 11.8 | -0.1 | 1.1 | Y |
| 18B | B5090 / Bakestonedale Rd | EB | 12.0 | 11.7 | -0.4 | 3.0 | Y |
| 19A | Bakestonedale Rd/ Brookledge Lane / M ill Lane | WB | 12.5 | 13.2 | 0.7 | 5.3 | Y |


| 19B | Bakestonedale Rd / Brookledge Lane / M ill Lane | EB | 12.4 | 13.0 | 0.6 | 4.6 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20A | B5358 | NB | 12.0 | 12.7 | 0.6 | 5.2 | Y |
| 20B | B5358 | SB | 12.3 | 13.4 | 1.2 | 9.6 | Y |
| 21A | Roundy Lane / M iddlewood Rd / W aterloo Rd | NB | 12.4 | 11.8 | -0.7 | 5.3 | Y |
| 21B | Roundy Lane/ M iddlewood Rd/ W aterloo Rd | SB | 11.6 | 11.7 | 0.1 | 0.4 | Y |
| 22A | B5465 / A626 | NB | 4.6 | 4.9 | 0.3 | 6.9 | Y |
| 22B | B5465 / A626 | SB | 5.2 | 5.4 | 0.2 | 3.7 | Y |
| 23A | A626 | NB | 12.2 | 11.5 | -0.6 | 5.2 | Y |
| 23B | A626 | SB | 11.6 | 10.5 | -1.1 | 9.5 | Y |
| 24A | A560 | NB | 7.4 | 7.8 | 0.5 | 6.5 | Y |
| 24B | A560 | SB | 7.1 | 8.6 | 1.5 | 20.8 | N |
| 25A | A6017 | NB | 7.2 | 6.5 | -0.7 | 9.8 | Y |
| 25B | A6017 | SB | 6.5 | 5.6 | -0.9 | 14.2 | Y |
| 26A | A560 / A627 | NB | 12.9 | 13.0 | 0.0 | 0.4 | Y |
| 26B | A560 / A627 | SB | 14.3 | 12.6 | -1.7 | 12.0 | Y |
| 27A | A626 | NB | 18.0 | 16.0 | -2.0 | 11.0 | Y |
| 27B | A626 | SB | 18.0 | 15.9 | -2.1 | 11.6 | Y |
| 28A | A560 | NB | 6.9 | 6.8 | 0.0 | 0.6 | Y |
| 28B | A560 | SB | 6.7 | 6.7 | 0.1 | 1.0 | Y |
| 29A | A627 | NB | 12.0 | 9.4 | -2.6 | 21.8 | N |
| 29B | A627 | SB | 12.4 | 9.0 | -3.4 | 27.4 | N |
| 30A | A560 | NB | 15.6 | 13.5 | -2.1 | 13.5 | Y |
| 30B | A560 | SB | 17.6 | 15.1 | -2.5 | 14.1 | Y |
| 31A | B6104 | NB | 10.3 | 9.7 | -0.6 | 5.6 | Y |
| 31B | B6104 | SB | 10.1 | 9.7 | -0.5 | 4.7 | Y |
| Total |  |  | 838.9 | 815.3 | -23.6 | -2.8 |  |
| Number of routes satisfying DMRB Criteria =56 out of 62 (90\%) |  |  |  |  |  |  |  |

## PM Peak Hour Journey Time Validation Results

8.12 Table 8.4 compares modelled and observed journey times in the PM peak hour for the 42 journey time routes.
8.13 For most routes the comparisons are very good, with 53 out of $62(85 \%)$ of the routes meeting the DMRB criteria of $H-15 \%$. Considering all of the routes together, the total modelled time is $8.4 \%$ lower than the observed time, which is within the DM RB criteria, but suggests that the modelled speeds are slightly faster in general.

| Table 8.4 | PM Peak Journey Times |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Route | Route Description | Dir | Observed | Modelled | Modelled- | \% | Within |
| Number |  |  | Time | Time | Observed | Error | DMRB |
| 1A | A6 Chapel to Heaton M oor | NB | 46.0 | 47.9 | 1.9 | 4.1 | Y |
| 1B | A6 Heaton M oor To Chapel | SB | 49.0 | 48.0 | -1.0 | 2.1 | Y |
| 2A | A537 Knutsford To M acclesfield | E | 22.2 | 20.6 | -1.6 | 7.2 | Y |
| 2B | A537 M acclesfield To Knutsford | W | 21.3 | 20.8 | -0.5 | 2.3 | Y |
| 3A | B5085 Knutsford To Alderley Edge | E | 13.9 | 13.7 | -0.2 | 1.6 | Y |
| 3B | B5085 Alderley Edge To Knutsford | W | 15.9 | 14.5 | -1.4 | 8.9 | Y |
| 4A | B5087 M acclesfield To Alderley Edge | NW | 7.5 | 6.8 | -0.6 | 8.3 | Y |
| 4B | B5087 Alderley Edge To M acclesfield | SE | 7.2 | 6.8 | -0.4 | 5.1 | Y |
| 5A | M 56 M anchester Airport To West Didsbury | N | 10.0 | 6.5 | -3.5 | 34.8 | N |
| 5B | M 56 West Didsbury To M anchester Airport | S | 6.2 | 6.2 | 0.0 | 0.5 | Y |
| 6A | B5166 Wilmslow to Northenden | N | 19.6 | 17.3 | -2.3 | 11.9 | Y |
| 6B | B5166 Northenden to Wilmslow | S | 18.4 | 16.2 | -2.2 | 12.0 | Y |
| 7A | M 56J8 to J5 | E | 10.3 | 8.4 | -1.9 | 18.6 | N |
| 7B | M 56 J 5 to J8 | W | 5.7 | 8.0 | 2.4 | 41.9 | N |
| 8A | A5102 Wilmslow to Bramhall | NE | 15.1 | 13.8 | -1.3 | 8.4 | Y |
| 8B | A5102 Bramhall to Bramhall | SW | 13.9 | 12.5 | -1.4 | 10.1 | Y |
| 9A | A34 Alderley Edge to East Didsbury | N | 28.7 | 26.0 | -2.7 | 9.4 | Y |
| 9B | A34 East Didsbury to Alderley Edge | S | 22.9 | 21.8 | -1.1 | 4.8 | Y |
| 10A | A523 Prestbury to Hazel Grove | N | 18.9 | 17.0 | -2.0 | 10.4 | Y |
| 10B | A523 Hazel Grove to Prestbury | S | 15.3 | 14.5 | -0.8 | 5.5 | Y |
| 11A | A555 M AELR Poynton to M anchester Airport | W | 22.2 | 22.6 | 0.4 | 2.0 | Y |
| 11B | A555 M anchester Airport to Poynton | E | 33.3 | 28.4 | -4.9 | 14.7 | Y |
| 12A | A538 Prestbury to Hazel Grove | NW | 34.9 | 34.3 | -0.6 | 1.7 | Y |
| 12B | A538 Hazel Grove to Prestbury | SE | 40.6 | 39.6 | -1.0 | 2.4 | Y |
| 13A | M 60 J6 to J24 | AC | 20.8 | 15.7 | -5.2 | 24.8 | N |
| 13B | M 60J24 to J6 | CW | 15.3 | 13.8 | -1.5 | 9.8 | Y |
| 14A | Heald Green to Cheadle Heath | NE | 13.8 | 12.1 | -1.7 | 12.5 | Y |
| 14B | Cheadle Heath to Heald Green | SW | 14.8 | 12.9 | -1.9 | 13.0 | Y |
| 15A | A5149/3 Cheadle Hulme to Hazel Grove | E | 13.6 | 10.7 | -2.9 | 21.5 | N |
| 15B | A5143/9 Hazel Grove to Cheadle Hulme | W | 12.4 | 11.3 | -1.1 | 9.0 | Y |
| 16A | Buxton Old Rd/ Higher Lane | SB | 7.7 | 7.6 | 0.0 | 0.4 | Y |
| 16B | Buxton Old Rd / Higher Lane | NB | 8.4 | 7.5 | -0.9 | 10.2 | Y |
| 17A | B5470 Chapel to M acclesfield | SB | 21.6 | 20.4 | -1.1 | 5.2 | Y |
| 17B | B5470 M acclesfield to Chapel | NB | 21.5 | 20.0 | -1.5 | 6.9 | Y |
| 18A | B5090 / Bakestonedale Rd | WB | 11.9 | 11.8 | -0.1 | 0.9 | Y |
| 18B | B5090 / Bakestonedale Rd | EB | 12.1 | 11.8 | -0.3 | 2.3 | Y |
| 19A | Bakestonedale Rd/ Brookledge Lane / M ill Lane | WB | 13.1 | 13.4 | 0.3 | 2.2 | Y |
| 19B | Bakestonedale Rd/ Brookledge Lane / M ill Lane | EB | 12.6 | 13.3 | 0.7 | 5.3 | Y |
| 20A | B5358 | NB | 12.6 | 14.3 | 1.7 | 13.8 | Y |
| 20B | B5358 | SB | 15.8 | 15.5 | -0.3 | 1.8 | Y |


| 21A | Roundy Lane / M iddlewood Rd/ W aterloo Rd | NB | 13.1 | 11.2 | -1.9 | 14.3 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21B | Roundy Lane/ M iddlewood Rd/ W aterloo Rd | SB | 12.2 | 10.4 | -1.8 | 14.7 | Y |
| 22A | B5465 / A626 | NB | 6.3 | 6.0 | -0.3 | 5.4 | Y |
| 22B | B5465 / A626 | SB | 7.8 | 6.8 | -1.0 | 12.7 | Y |
| 23A | A626 | NB | 14.4 | 12.8 | -1.6 | 11.2 | Y |
| 23B | A626 | SB | 19.5 | 12.1 | -7.5 | 38.2 | N |
| 24A | A560 | NB | 9.0 | 10.7 | 1.7 | 19.3 | N |
| 24B | A560 | SB | 8.1 | 8.1 | 0.0 | 0.5 | Y |
| 25A | A6017 | NB | 8.6 | 8.3 | -0.3 | 3.4 | Y |
| 25B | A6017 | SB | 9.6 | 8.4 | -1.2 | 12.6 | Y |
| 26A | A560 / A627 | NB | 18.1 | 15.9 | -2.2 | 12.4 | Y |
| 26B | A560 / A627 | SB | 14.7 | 14.8 | 0.1 | 0.6 | Y |
| 27A | A626 | NB | 18.6 | 16.6 | -2.0 | 10.7 | Y |
| 27B | A626 | SB | 18.3 | 17.5 | -0.8 | 4.4 | Y |
| 28A | A560 | NB | 7.1 | 7.5 | 0.4 | 6.0 | Y |
| 28B | A560 | SB | 7.1 | 7.5 | 0.5 | 6.7 | Y |
| 29A | A627 | NB | 17.7 | 16.1 | -1.6 | 9.0 | Y |
| 29B | A627 | SB | 14.7 | 13.3 | -1.4 | 9.8 | Y |
| 30A | A560 | NB | 26.3 | 15.4 | -10.8 | 41.2 | N |
| 30B | A560 | SB | 26.8 | 18.3 | -8.4 | 31.5 | N |
| 31A | B6104 | NB | 10.1 | 11.0 | 0.9 | 9.1 | Y |
| 31B | B6104 | SB | 13.6 | 12.0 | -1.6 | 11.7 | Y |
| Total |  |  | 1028.8 | 942.8 | -85.9 | -8.4 |  |
| Number of routes satisfying DMRB Criteria = 54 out of 62 (87\%) |  |  |  |  |  |  |  |

## Commentary on Journey Time Outliers

8.14 In all three time periods the major outliers are the motorway-based routes along the M 56/A5103 from Junction 5 to West Didsbury and the M 60 from Junction 6 to Junction 24. These journey time routes display significant degrees of variability in times. For example:
8.15 The variability in times reflects:

- The wider range of possible speeds on the motorway network (given the speed limit of 70 mph );
- the closely spaced junctions along these sections of motorways and the resulting weaving, merging and shock wave effects; and
- the variations in flow on the motorway network that can result from 'strategic' diversion of traffic.
8.16 The frequency of junctions and associated weaving, merging, lane-drops/gains etc impact on driver behaviour and on lane chose e.g. lanes 1 and 2 may move much slower than lanes 3 and 4 causing drivers to switch lanes.
8.17 Flows (and therefore times/ speeds) can vary significantly as a result of incidents elsewhere on the SRN which can cause traffic to divert. For example, an incident on the M 62 west of M anchester can result in traffic diverting to the M56. Many of these incidents can be some distance from the section of motorway being observed and may not be identified when 'filtering' data for use in analysis.
8.18 Note that SATURN as a modelling package cannot model lane use, lane switching or driver behaviour to the same extent as microsimulation or mesoscopic models. Working with the Highways Agency and Leeds ITS, HFAS has undertaken extensive testing to improve the representation of motorways within the GMSM and SATURN models in general. Further changes are being made to SATURN software (for example, the introduction of link specific parameters which will reflect the willingness of vehicles to move out of the nearside lane to permit merging vehicles to join) which may improve the representation of urban motorw ays in the future.


## Conclusions of Journey Time Validation

8.19 The results presented above indicate that the journey time validation fully meets DM RB requirements in all three time period.
8.20 The percentages of routes within $15 \%$ of the observed time ranges are $87 \%, 90 \%$ and $87 \%$ in the AM peak hour, inter-peak hour and PM peak hour respectively.
8.21 Graphs of observed versus modelled journey times are included in Appendix 3.

## 9. Condusions

9.1 The A6 to M60 SATURN model has been built to inform the development of the business case for the proposed A6 to M 60 Relief Road. The models have been developed from the GM -SATURN model.
9.2 The A6 to M60 modelling network is in full SATURN simulation detail throughout the A6 to M 60 Area of Influence (Stockport, South M anchester and the northern part of Cheshire East) and the remainder of Greater Manchester, and SATURN buffer network outside of these areas.
9.3 The model was well converged in all time periods, with Delta values well below $1 \%$ and the percentage of links with flows changing by less than $2 \%$ over approximately $99 \%$ in all periods.
9.4 The SATURN model has been built to evaluate the A6 to M 60 Relief Road. The model has therefore been validated by comparing modelled link flows and journey times with observed data across the SEM M M S Area of Influence, for the 2015 base year.
9.5 In the AM peak, inter-peak and PM peak hours the percentages of all motorway and local road sites used in matrix estimation which met webtag validation criteria were $89 \%, 91 \%$ and $88 \%$ respectively.
9.6 Eighteen cordons and screenlines were formed for the link flow validation within the AOI.
9.7 Considering the 18 ME cordon and screenlines together, the percentage with screenline GEH values less than 4 is $78 \%$ in the AM peak, $78 \%$ in the inter-peak and $72 \%$ in the PM peak. Of these several routes marginally exceed 4 with values less than 4.5 of $86 \%$ in the AM peak, $89 \%$ in the inter-peak and $86 \%$ in the PM peak.
9.8 Modelled and observed journey times were compared on 31 (two-way) routes covering key radials and orbitals crossing or parallel to the proposed scheme.
9.9 The Webtag guideline for journey time validation is that modelled times should be within $15 \%$ (or 1 minute if this is higher) of the observed time on more than $85 \%$ of route. The percentages of routes within $15 \%$ of the observed time ranges were $87 \%, 90 \%$ and $85 \%$ in the AM peak hour, inter-peak hour and PM peak hour respectively. All time periods therefore comfortably meet Webtag criteria.
9.10 The model is well converged in all three modelled time periods and the modelled traffic volumes are therefore very stable.
9.11 The results presented above indicate that the model meets Webtag requirements in almost all regards. Where it falls short of these requirements it does so only marginally.
9.12 Overall we consider that the model provides a sound basis for forecasting the effects of the proposed A6 to M 60 M odel.
10. References

1. Traffic Appraisal of Road Schemes - Traffic Appraisal Advice, Design Manual for Roads and Bridges, Volume 12, Highways Agency, M ay 1996
2. M anchester Airport M aster Plan to 2030, M anchester Airport, 2007
3. Manchester Airport Ground Transport Plan, Manchester Airport, 2007
4. The Need for Land - Manchester Airport Company's Response to Manchester City Council's LDF Option Development, M anchester Airport
5. A6 to Manchester Airport Relief Road Area of Influence, Greater Manchester Transportation Unit, A6 to M60 Briefing Note 24
6. A6 to M60 A6 to Manchester Airport Relief Road Technical Node 13, Highway Demand Matrices, MVA, July 2010

## Appendix 1 Example Calculation of Generalised Cost

A6M 60 uses a set of user class specific generalised costs. These are calculated using an excel workbook prepared initially by M VA Consultancy The basic approach has been applied in a number of studies from the Greater M anchester TIF bid onwards, with regular reviews and updates to reflect the impact of changes to WebTAG parameters. The approach is summarised below

## Basic Parameters

The basic parameter inputs to the calculation process consist of:

- Perceived Values of Time per person expressed as pence per hour at average 2002 prices and values, sourced from Tables 1 and 2 of WebTag Unit 3.5.6
- Vehicle Occupancies per trip by vehicle type and work/non-work, sourced from WebTag Unit 3.5.6, Table 4
- Vehicle Operating Costs (fuel) sourced from W ebTag Unit 3.5.6 Table 10 (parameter values), Table 11 (Fuel cost factors) and Table 12 (fleet composition)
- Vehicle Operating Costs (non-fuel) sourced from WebTag Unit 3.5.6 Table 15
- Goods vehicle splits from GMTU monitoring (class by proportion of vehicles and proportion of veh/km) and GMATS RSI data (work, non-work).

All WebTag inputs are drawn from the April 2011 edition of Unit 3.5.6.

## Growth Rates

Information on growth in parameter values is based on WebTag Unit 3.5.6, April 2011. Tables used are:

- Value of Time per person 2003-2052, Table 3
- Car passenger occupancy by period, 2000-2036, Table 6
- Fleet composition 2002-2031, Table 12
- Fuel Efficiency improvements 2002-2035, Table 13
- Fuel price - increase in resource cost/hr, Table 14; and
- Fuel Price - fuel costs, duties and VAT, Table 11.

Process - Worked Example - 2009 Car Work-Time AM Peak Hour

## Value of Time (PPM)

Value of Time for car work-time driver $2002=2186$ pence per hour

Growth in VOT for car work-time from 2002 to $2009=1.05$
VOT for car work-time driver, $2009=2186 * 1.05=2296$ pence per hour per person
Value of Time for car work-time passenger $2002=1566$ pence per hour
Growth in VOT for car work-time from 2002 to $2009=1.05$

VOT for car work-time passenger, $2009=1566 * 1.05=1645$ pence per hour per person
Occupants per car work-time, $2000=1.20$
Growth in Passengers from 2000 to 2009 (AM Peak) $=0.9576$
Occupants per car work-time, $2009=(1.20-1) * 0.9576=0.19$
Value of time, pence per hour at $2009=2296+\left(1645^{*} 0.19\right)=2611$ pence
Value of time, pence per minute at $2009=2611 / 60=43.52$ pence

## Value of Distance (PPK)

## Fuel Consumption (Petrol)

From WebTag, Consumption Formula is $\mathrm{L}=\left(\mathrm{a}+\mathrm{bV}+\mathrm{cV}^{2}+\mathrm{dV}^{3}\right) / \mathrm{V}$

## For Petrol:

$A=1.04285$
$B=0.04484$
$C=0.00005$
$\mathrm{D}=0.0000021781$
V=37.8 kph (AM Peak Network speed)

Substituting in above formula
$L=\left(1.054285+0.04484 * 37.8+0.00005 * 37.8^{2}+0.0000021781 * 37.8^{3}\right) / 37.8$
$\mathrm{L}=0.07368$

Growth adjustment for Petrol based on WebTag Unit 3.5.6, Table 13
$=0.07368 * 0.94=0.0695$

## For Diesel

$A=0.48099$
$B=0.06450$
$C=0.00058$
$D=0.0000045416$
$\mathrm{V}=37.8 \mathrm{kph}$

Substituting in above formula
$L=\left(0.48099+0.06450 * 37.8+0.00058 * 37.8^{2}+0.0000045416 * 37.8^{3}\right) / 37.8$
L=0.06188

Growth adjustment for Diesel based on WebTag Unit 3.5.6, Table 13
$=0.06188 * 0.92=0.570$

## Fuel Price Per Litre

Price $=$ Resource Cost + Duty +VAT

## Petrol

Resource Cost $=$ Fuel Cost Factor*(2009 Resource Cost Growth Factor/2005 Resource Cost Growth Factor) $=25 *(1.617 / 1.497)=27.00$

Fuel Duty = Duty*(2009 Duty Growth Factor/2005 Duty Growth Factor) =43.7 * $(1.002 / 0.954)=45.51$

VAT $=2009$ VAT Rate * Fuel Cost Factor $=0 * 1=0$

Petrol price $=(27+45.51) * 0=72.51 \mathrm{p} / \mathrm{ltr}$
Diesel
Resource Cost $=$ Fuel Cost Factor*(2009 Resource Cost Growth Factor/2005 Resource Cost Growth Factor) $=28 *(1.636 / 1.522)=30.10$

Fuel Duty = Duty*(2009 Duty Growth Factor/2005 Duty Growth Factor) = 43.7 * (1.002/0.954) $=45.51$

VAT $=2009$ VAT Rate $*$ Fuel Cost Factor $=0 * 1=0$

Diesel price $=(30.1+45.51) * 0=75.61 \mathrm{p} / \mathrm{ltr}$

## Cost Per Km

Proportion of fleet using petrol \& diesel

2009 Petrol $=0.621$
2009 Diesel $=0.379$

Petrol $=0.0695 * 72.51 * 0.621=3.129$
Diesel $=0.0570 * 75.61 * 0.379=1.633$
Cost per KM $=4.76$

Vehicle Operating Costs - Non-Fuel
Based on formula $C=a 1+b 1 / v$

For car work-time:
A1=4.069
$B 1=111.391$

VOC $($ Non-Fuel $)=4.069+111.391 / 37.8=7.016$

Final Values:

PPM $=43.52$
PPK $=(4.76+7.016)=11.78$

Appendix 2 Prior and Estimated Matrix Comparisons by Sector

Highways Forecasting and Analytical Services
Greater Manchester
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907

| AM - Peak - ALL PCU's |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sectors | SATME2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | Orig Totals |
| 1 | Prior | 1425.3 | 904.0 | 354.5 | 1000.0 | 1476.4 | 261.7 | 139.7 | 152.9 | 69.2 | 24.9 | 140.1 | 598.8 | 6547.4 |
|  | After | 1285.1 | 1069.3 | 234.3 | 1393.7 | 1126.8 | 321.9 | 158.9 | 188.5 | 76.0 | 23.6 | 184.9 | 731.2 | 6794.3 |
|  | Perc Diff | -9.8\% | 18.3\% | -33.9\% | 39.4\% | -23.7\% | 23.0\% | 13.8\% | 23.3\% | 9.9\% | -5.0\% | 32.0\% | 22.1\% | 3.8\% |
| 2 | Prior | 1025.0 | 4020.7 | 2296.3 | 661.2 | 2664.8 | 449.7 | 744.5 | 184.7 | 164.5 | 44.3 | 324.8 | 891.7 | 13472.4 |
|  | After | 938.5 | 5356.1 | 2555.1 | 689.9 | 2287.8 | 546.3 | 935.4 | 165.3 | 154.3 | 69.4 | 384.4 | 933.6 | 15016.0 |
|  | Perc Diff | -8.4\% | 33.2\% | 11.3\% | 4.3\% | -14.1\% | 21.5\% | 25.6\% | -10.5\% | -6.2\% | 56.7\% | 18.3\% | 4.7\% | 11.5\% |
| 3 | Prior | 598.4 | 3193.4 | 12938.7 | 851.3 | 6070.6 | 335.0 | 944.0 | 354.3 | 229.4 | 155.5 | 3331.2 | 1609.7 | 30611.5 |
|  | After | 433.3 | 2380.7 | 14329.3 | 717.0 | 4916.0 | 469.5 | 1080.7 | 218.3 | 103.0 | 108.9 | 2553.3 | 1232.8 | 28542.8 |
|  | Perc Diff | -27.6\% | -25.4\% | 10.7\% | -15.8\% | -19.0\% | 40.1\% | 14.5\% | -38.4\% | -55.1\% | -30.0\% | -23.4\% | -23.4\% | -6.8\% |
| 4 | Prior | 1553.2 | 898.8 | 845.0 | 14580.7 | 8811.6 | 1231.6 | 232.7 | 1480.5 | 485.3 | 170.1 | 438.7 | 2346.3 | 33074.5 |
|  | After | 2125.6 | 791.3 | 850.8 | 15897.1 | 10602.9 | 1406.1 | 189.9 | 759.8 | 323.4 | 107.2 | 590.4 | 1666.7 | 35311.0 |
|  | Perc Diff | 36.8\% | -12.0\% | 0.7\% | 9.0\% | 20.3\% | 14.2\% | -18.4\% | -48.7\% | -33.4\% | -37.0\% | 34.6\% | -29.0\% | 6.8\% |
| 5 | Prior | 1644.6 | 2441.1 | 4616.8 | 4879.6 | 63658.3 | 1095.6 | 709.9 | 3370.5 | 3691.7 | 1208.4 | 6807.4 | 6005.5 | 100129.4 |
|  | After | 1633.9 | 2294.5 | 3718.7 | 5650.6 | 70489.5 | 1142.0 | 447.0 | 3164.1 | 2837.3 | 913.6 | 5317.2 | 4958.3 | 102566.6 |
|  | Perc Diff | -0.7\% | -6.0\% | -19.5\% | 15.8\% | 10.7\% | 4.2\% | -37.0\% | -6.1\% | -23.1\% | -24.4\% | -21.9\% | -17.4\% | 2.4\% |
| 6 | Prior | 235.8 | 239.6 | 106.0 | 709.2 | 547.9 | 6382.2 | 525.5 | 373.1 | 74.9 | 25.5 | 82.1 | 3715.4 | 13017.2 |
|  | After | 363.3 | 270.8 | 228.4 | 816.6 | 601.5 | 6382.2 | 538.5 | 351.1 | 72.0 | 19.0 | 209.3 | 3696.1 | 13548.9 |
|  | Perc Diff | 54.1\% | 13.0\% | 115.4\% | 15.1\% | 9.8\% | 0.0\% | 2.5\% | -5.9\% | -3.8\% | -25.3\% | 155.0\% | -0.5\% | 4.1\% |
| 7 | Prior | 154.6 | 656.6 | 763.0 | 151.1 | 520.6 | 603.9 | 6217.7 | 123.2 | 51.9 | 13.6 | 124.8 | 1777.7 | 11158.7 |
|  | After | 96.9 | 756.5 | 1138.5 | 159.8 | 343.1 | 699.8 | 6608.6 | 72.4 | 20.2 | 6.5 | 70.9 | 1713.0 | 11686.1 |
|  | Perc Diff | -37.3\% | 15.2\% | 49.2\% | 5.8\% | -34.1\% | 15.9\% | 6.3\% | -41.2\% | -61.1\% | -52.4\% | -43.2\% | -3.6\% | 4.7\% |
| 8 | Prior | 242.7 | 223.6 | 328.4 | 1856.5 | 6049.2 | 852.5 | 192.0 | 39461.6 | 6297.4 | 231.0 | 401.2 | 13748.0 | 69884.1 |
|  | After | 287.3 | 125.1 | 190.5 | 1047.3 | 5250.3 | 828.1 | 133.5 | 36313.7 | 5497.2 | 129.5 | 211.2 | 12422.9 | 62436.6 |
|  | Perc Diff | 18.4\% | -44.1\% | -42.0\% | -43.6\% | -13.2\% | -2.9\% | -30.5\% | -8.0\% | -12.7\% | -43.9\% | -47.4\% | -9.6\% | -10.7\% |
| 9 | Prior | 181.2 | 150.3 | 266.2 | 509.0 | 6012.9 | 238.2 | 72.0 | 4304.0 | 38797.0 | 2064.9 | 1233.0 | 5589.3 | 59418.0 |
|  | After | 141.3 | 76.3 | 186.0 | 146.6 | 4677.3 | 38.8 | 18.1 | 4014.4 | 37682.4 | 1843.1 | 1064.6 | 4988.3 | 54877.1 |
|  | Perc Diff | -22.0\% | -49.2\% | -30.1\% | -71.2\% | -22.2\% | -83.7\% | -74.9\% | -6.7\% | -2.9\% | -10.7\% | -13.7\% | -10.8\% | -7.6\% |
| 10 | Prior | 54.3 | 55.1 | 128.7 | 128.2 | 2001.3 | 88.2 | 31.7 | 194.1 | 2368.2 | 13931.7 | 3825.3 | 2258.8 | 25065.5 |
|  | After | 27.9 | 40.4 | 106.5 | 38.6 | 1262.0 | 3.5 | 4.7 | 134.8 | 1995.7 | 13749.7 | 3279.2 | 2510.0 | 23153.0 |
|  | Perc Diff | -48.7\% | -26.6\% | -17.2\% | -69.8\% | -36.9\% | -96.0\% | -85.2\% | -30.6\% | -15.7\% | -1.3\% | -14.3\% | 11.1\% | -7.6\% |
| 11 | Prior | 312.7 | 375.4 | 2942.1 | 407.5 | 9714.2 | 212.6 | 156.5 | 350.3 | 1296.0 | 3307.1 | 30668.6 | 2572.1 | 52315.0 |
|  | After | 245.6 | 144.7 | 2322.3 | 327.1 | 10616.9 | 277.6 | 59.8 | 412.9 | 1020.2 | 3300.0 | 30286.8 | 2129.7 | 51143.5 |
|  | Perc Diff | -21.5\% | -61.5\% | -21.1\% | -19.7\% | 9.3\% | 30.6\% | -61.8\% | 17.9\% | -21.3\% | -0.2\% | -1.2\% | -17.2\% | -2.2\% |
| 12 | Prior | 1376.8 | 888.8 | 1559.8 | 2085.2 | 8607.1 | 6413.8 | 2362.6 | 11495.2 | 4961.4 | 1818.9 | 2880.8 | 720480.1 | 764930.5 |
|  | After | 1548.0 | 806.7 | 1603.2 | 1597.0 | 6414.1 | 5711.7 | 2307.0 | 11657.8 | 5367.8 | 2173.6 | 2408.5 | 719171.8 | 760767.2 |
|  | Perc Diff | 12.4\% | -9.2\% | 2.8\% | -23.4\% | -25.5\% | -10.9\% | -2.4\% | 1.4\% | 8.2\% | 19.5\% | -16.4\% | -0.2\% | -0.5\% |
| Dest Totals | Prior | 8804.5 | 14047.4 | 27145.6 | 27819.7 | 116134.9 | 18164.9 | 12328.8 | 61844.3 | 58486.9 | 22995.8 | 50258.1 | 761593.3 | 1179624.1 |
|  | After | 9126.7 | 14112.4 | 27463.5 | 28481.4 | 118588.2 | 17827.5 | 12482.0 | 57452.9 | 55149.5 | 22444.2 | 46560.6 | 756154.2 | 1165843.0 |
|  | Perc Diff | 3.7\% | 0.5\% | 1.2\% | 2.4\% | 2.1\% | -1.9\% | 1.2\% | -7.1\% | -5.7\% | -2.4\% | -7.4\% | -0.7\% | -1.2\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Inter - Peak - ALL PCU's |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Sectors | SATME2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | Orig Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Prior | 1453.5 | 801.5 | 394.6 | 896.3 | 1165.8 | 181.2 | 99.2 | 119.7 | 81.4 | 30.4 | 143.9 | 490.3 | 5857.9 |
| 1 | After | 1293.5 | 862.9 | 343.4 | 1247.7 | 1296.8 | 207.2 | 83.5 | 127.9 | 97.6 | 37.3 | 193.2 | 557.3 | 6348.1 |
|  | Perc Diff | -11.0\% | 7.7\% | -13.0\% | 39.2\% | 11.2\% | 14.3\% | -15.9\% | 6.8\% | 19.9\% | 22.5\% | 34.3\% | 13.7\% | 8.4\% |
|  | Prior | 850.9 | 3382.8 | 2352.2 | 453.3 | 1633.1 | 287.8 | 522.9 | 104.1 | 74.5 | 37.6 | 208.3 | 483.3 | 10390.7 |
| 2 | After | 795.4 | 4306.5 | 2212.0 | 549.1 | 1460.0 | 296.0 | 488.7 | 89.2 | 75.7 | 65.4 | 152.5 | 505.6 | 10995.9 |
|  | Perc Diff | -6.5\% | 27.3\% | -6.0\% | 21.1\% | -10.6\% | 2.9\% | -6.6\% | -14.3\% | 1.6\% | 73.6\% | -26.8\% | 4.6\% | 5.8\% |
|  | Prior | 404.7 | 2180.4 | 14100.1 | 318.3 | 4265.5 | 160.3 | 786.2 | 132.2 | 138.5 | 75.7 | 2777.5 | 968.0 | 26307.2 |
| 3 | After | 336.1 | 2250.2 | 14535.0 | 371.3 | 3762.2 | 234.6 | 779.2 | 144.8 | 122.3 | 74.0 | 2273.4 | 1000.0 | 25883.3 |
|  | Perc Diff | -17.0\% | 3.2\% | 3.1\% | 16.7\% | -11.8\% | 46.4\% | -0.9\% | 9.5\% | -11.7\% | -2.3\% | -18.1\% | 3.3\% | -1.6\% |
|  | Prior | 1074.4 | 438.6 | 340.0 | 11999.6 | 4553.9 | 785.2 | 102.6 | 1136.5 | 280.4 | 80.3 | 218.6 | 1364.5 | 22374.7 |
| 4 | After | 1337.1 | 534.6 | 380.2 | 12969.5 | 5212.8 | 862.5 | 98.5 | 630.1 | 233.7 | 81.2 | 305.2 | 1203.9 | 23849.2 |
|  | Perc Diff | 24.5\% | 21.9\% | 11.8\% | 8.1\% | 14.5\% | 9.8\% | -4.0\% | -44.6\% | -16.7\% | 1.1\% | 39.6\% | -11.8\% | 6.6\% |
|  | Prior | 1224.2 | 1528.3 | 4245.0 | 4286.7 | 54313.0 | 726.2 | 434.9 | 3252.5 | 3577.2 | 1042.9 | 6516.8 | 5104.8 | 86252.7 |
| 5 | After | 1174.0 | 1454.2 | 4133.8 | 4083.5 | 56655.1 | 845.3 | 188.0 | 2908.5 | 2916.8 | 791.1 | 5560.4 | 4970.6 | 85681.4 |
|  | Perc Diff | -4.1\% | -4.8\% | -2.6\% | -4.7\% | 4.3\% | 16.4\% | -56.8\% | -10.6\% | -18.5\% | -24.2\% | -14.7\% | -2.6\% | -0.7\% |
|  | Prior | 144.2 | 216.7 | 144.0 | 697.8 | 528.8 | 4676.1 | 341.9 | 416.5 | 119.9 | 71.2 | 156.0 | 2896.0 | 10408.9 |
| 6 | After | 136.3 | 236.2 | 175.1 | 748.3 | 665.2 | 4676.0 | 336.4 | 378.1 | 85.7 | 46.7 | 278.7 | 2897.3 | 10660.0 |
|  | Perc Diff | -5.5\% | 9.0\% | 21.6\% | 7.2\% | 25.8\% | 0.0\% | -1.6\% | -9.2\% | -28.5\% | -34.4\% | 78.7\% | 0.0\% | 2.4\% |
|  | Prior | 105.1 | 516.4 | 708.5 | 108.7 | 274.5 | 386.8 | 4991.8 | 53.4 | 27.8 | 14.0 | 108.0 | 1183.6 | 8478.6 |
| 7 | After | 95.3 | 436.9 | 799.1 | 80.4 | 137.1 | 378.0 | 5323.5 | 33.6 | 8.7 | 5.7 | 47.7 | 1200.1 | 8546.0 |
|  | Perc Diff | -9.3\% | -15.4\% | 12.8\% | -26.0\% | -50.1\% | -2.3\% | 6.6\% | -37.0\% | -68.6\% | -59.4\% | -55.9\% | 1.4\% | 0.8\% |
|  | Prior | 114.8 | 75.1 | 114.8 | 1115.1 | 2696.3 | 384.7 | 34.4 | 35385.5 | 3918.3 | 157.4 | 236.2 | 8380.5 | 52613.2 |
| 8 | After | 116.4 | 55.0 | 98.3 | 534.2 | 3074.4 | 349.7 | 30.8 | 31670.8 | 3673.4 | 103.9 | 190.4 | 7803.1 | 47700.3 |
|  | Perc Diff | 1.3\% | -26.8\% | -14.4\% | -52.1\% | 14.0\% | -9.1\% | -10.4\% | -10.5\% | -6.2\% | -34.0\% | -19.4\% | -6.9\% | -9.3\% |
|  | Prior | 86.5 | 54.8 | 130.6 | 269.3 | 3282.8 | 116.9 | 28.2 | 4103.9 | 32775.8 | 2039.4 | 814.0 | 3438.4 | 47140.6 |
| 9 | After | 130.5 | 67.6 | 221.2 | 209.2 | 2998.1 | 31.3 | 17.4 | 3851.3 | 31204.8 | 1601.0 | 682.3 | 3674.8 | 44689.5 |
|  | Perc Diff | 50.9\% | 23.3\% | 69.3\% | -22.3\% | -8.7\% | -73.2\% | -38.1\% | -6.2\% | -4.8\% | -21.5\% | -16.2\% | 6.9\% | -5.2\% |
|  | Prior | 36.7 | 28.4 | 77.8 | 77.0 | 1000.2 | 67.2 | 14.2 | 165.9 | 2056.8 | 13682.2 | 2739.5 | 1580.0 | 21525.9 |
| 10 | After | 26.7 | 26.0 | 89.4 | 49.8 | 702.9 | 9.4 | 4.6 | 151.0 | 1598.7 | 12876.5 | 2470.7 | 1842.4 | 19848.1 |
|  | Perc Diff | -27.3\% | -8.6\% | 15.0\% | -35.3\% | -29.7\% | -86.0\% | -67.8\% | -9.0\% | -22.3\% | -5.9\% | -9.8\% | 16.6\% | -7.8\% |
|  | Prior | 142.0 | 178.7 | 2673.3 | 203.6 | 6391.4 | 175.8 | 103.7 | 277.6 | 866.7 | 2685.0 | 28879.0 | 1916.2 | 44492.9 |
| 11 | After | 168.9 | 173.2 | 2633.3 | 252.4 | 5842.6 | 269.4 | 71.1 | 308.2 | 918.0 | 2557.6 | 27874.6 | 2127.8 | 43196.9 |
|  | Perc Diff | 19.0\% | -3.1\% | -1.5\% | 24.0\% | -8.6\% | 53.2\% | -31.5\% | 11.0\% | 5.9\% | -4.7\% | -3.5\% | 11.0\% | -2.9\% |
|  | Prior | 793.3 | 502.9 | 1263.0 | 1492.5 | 5151.6 | 3498.2 | 1171.8 | 9346.3 | 3868.7 | 1757.8 | 2316.1 | 553768.0 | 584930.1 |
| 12 | After | 861.2 | 476.4 | 1346.3 | 1160.4 | 4648.9 | 3150.6 | 1205.3 | 8470.8 | 3569.2 | 1897.7 | 1826.9 | 554096.3 | 582710.1 |
|  | Perc Diff | 8.6\% | -5.3\% | 6.6\% | -22.3\% | -9.8\% | -9.9\% | 2.9\% | -9.4\% | -7.7\% | 8.0\% | -21.1\% | 0.1\% | -0.4\% |
|  | Prior | 6430.3 | 9904.7 | 26544.0 | 21918.1 | 85256.9 | 11446.2 | 8631.8 | 54494.2 | 47785.8 | 21673.8 | 45113.9 | 581573.7 | 920773.4 |
|  | After | 6471.3 | 10879.8 | 26967.1 | 22255.7 | 86456.2 | 11309.9 | 8626.9 | 48764.2 | 44504.6 | 20138.0 | 41856.0 | 581879.1 | 910108.8 |
|  | Perc Diff | 0.6\% | 9.8\% | 1.6\% | 1.5\% | 1.4\% | -1.2\% | -0.1\% | -10.5\% | -6.9\% | -7.1\% | -7.2\% | 0.1\% | -1.2\% |
| PM- Peak-ALL PCU's  <br> Sectors SATME2 |  | 4 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | $\begin{array}{ll} \hline 5 & 6 \\ \hline \end{array}$ |  |  | $8 \quad 9$ |  | $\begin{array}{ll} \hline 9 & 10 \\ \hline \end{array}$ |  |  |  |
|  |  | 7 | 11 | 12 |  |  | Orig Totals |


| 1 | Prior | 1190.2 | 872.4 | 639.3 | 1188.2 | 2014.5 | 288.6 | 228.1 | 344.5 | 267.0 | 107.4 | 359.1 | 2279.0 | 9778.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | After | 1194.0 | 1237.3 | 514.9 | 1624.1 | 1501.6 | 471.4 | 203.7 | 250.0 | 79.6 | 28.7 | 273.7 | 1600.6 | 8979.8 |
|  | Perc Diff | 0.3\% | 41.8\% | -19.4\% | 36.7\% | -25.5\% | 63.3\% | -10.7\% | -27.4\% | -70.2\% | -73.2\% | -23.8\% | -29.8\% | -8.2\% |
| 2 | Prior | 847.8 | 3238.1 | 2778.3 | 701.0 | 2399.3 | 324.4 | 739.1 | 155.7 | 138.9 | 72.2 | 395.2 | 792.2 | 12582.1 |
|  | After | 792.1 | 4041.9 | 2587.8 | 816.5 | 1883.0 | 354.3 | 790.2 | 88.3 | 97.2 | 49.4 | 375.3 | 653.1 | 12529.0 |
|  | Perc Diff | -6.6\% | 24.8\% | -6.9\% | 16.5\% | -21.5\% | 9.2\% | 6.9\% | -43.3\% | -30.0\% | -31.6\% | -5.0\% | -17.6\% | -0.4\% |
| 3 | Prior | 448.2 | 2133.7 | 12726.8 | 466.6 | 4701.1 | 197.9 | 887.8 | 157.1 | 211.0 | 117.2 | 3265.9 | 1199.3 | 26512.7 |
|  | After | 343.0 | 2355.2 | 13879.3 | 580.6 | 4791.0 | 356.2 | 1194.0 | 99.4 | 215.8 | 91.4 | 2660.5 | 1154.1 | 27720.5 |
|  | Perc Diff | -23.5\% | 10.4\% | 9.1\% | 24.4\% | 1.9\% | 79.9\% | 34.5\% | -36.8\% | 2.3\% | -22.1\% | -18.5\% | -3.8\% | 4.6\% |
| 4 | Prior | 1068.8 | 610.9 | 560.0 | 11884.2 | 5492.1 | 949.1 | 166.0 | 1624.4 | 466.5 | 123.1 | 362.3 | 2106.9 | 25414.3 |
|  | After | 1698.0 | 926.7 | 699.2 | 13039.5 | 7003.3 | 1146.5 | 241.4 | 1021.4 | 331.3 | 69.2 | 437.0 | 1617.2 | 28230.7 |
|  | Perc Diff | 58.9\% | 51.7\% | 24.8\% | 9.7\% | 27.5\% | 20.8\% | 45.4\% | -37.1\% | -29.0\% | -43.8\% | 20.6\% | -23.2\% | 11.1\% |
| 5 | Prior | 1484.9 | 2235.6 | 5435.9 | 6709.2 | 59017.5 | 958.7 | 749.6 | 5183.7 | 5763.0 | 1886.3 | 9002.5 | 7455.5 | 105882.5 |
|  | After | 1477.6 | 2341.7 | 5531.5 | 6169.4 | 63193.6 | 1731.5 | 312.0 | 5479.2 | 4915.1 | 1614.8 | 8444.5 | 7511.2 | 108722.1 |
|  | Perc Diff | -0.5\% | 4.7\% | 1.8\% | -8.0\% | 7.1\% | 80.6\% | -58.4\% | 5.7\% | -14.7\% | -14.4\% | -6.2\% | 0.7\% | 2.7\% |
| 6 | Prior | 221.7 | 374.5 | 358.9 | 1270.3 | 1145.4 | 5901.0 | 648.1 | 850.0 | 234.6 | 93.5 | 343.1 | 6689.4 | 18130.7 |
|  | After | 315.3 | 414.7 | 379.1 | 1252.5 | 983.4 | 5901.0 | 686.0 | 769.8 | 120.2 | 36.0 | 297.1 | 6348.9 | 17504.0 |
|  | Perc Diff | 42.2\% | 10.7\% | 5.6\% | -1.4\% | -14.1\% | 0.0\% | 5.8\% | -9.4\% | -48.8\% | -61.5\% | -13.4\% | -5.1\% | -3.5\% |
| 7 | Prior | 158.4 | 757.8 | 1065.7 | 247.5 | 723.3 | 531.6 | 6465.7 | 86.5 | 81.3 | 30.2 | 184.6 | 2212.6 | 12545.3 |
|  | After | 64.6 | 720.7 | 1023.5 | 176.8 | 361.2 | 495.5 | 6753.0 | 49.8 | 25.7 | 6.1 | 41.5 | 2100.3 | 11818.7 |
|  | Perc Diff | -59.2\% | -4.9\% | -4.0\% | -28.6\% | -50.1\% | -6.8\% | 4.4\% | -42.5\% | -68.4\% | -79.7\% | -77.5\% | -5.1\% | -5.8\% |
| 8 | Prior | 122.3 | 107.7 | 173.0 | 1524.3 | 3280.4 | 482.9 | 52.9 | 36231.6 | 4669.4 | 180.1 | 324.8 | 10463.6 | 57613.2 |
|  | After | 149.8 | 113.8 | 135.9 | 965.6 | 3187.9 | 426.7 | 50.2 | 34792.7 | 4328.3 | 108.7 | 212.1 | 10266.1 | 54737.7 |
|  | Perc Diff | 22.4\% | 5.6\% | -21.5\% | -36.7\% | -2.8\% | -11.6\% | -5.3\% | -4.0\% | -7.3\% | -39.6\% | -34.7\% | -1.9\% | -5.0\% |
| 9 | Prior | 94.6 | 91.2 | 198.6 | 442.6 | 4225.2 | 107.3 | 33.3 | 5294.4 | 33701.9 | 2340.6 | 1168.9 | 4439.0 | 52137.5 |
|  | After | 112.4 | 95.2 | 216.7 | 195.5 | 3544.9 | 27.2 | 11.6 | 5377.7 | 34315.9 | 2194.5 | 907.3 | 5080.6 | 52079.6 |
|  | Perc Diff | 18.9\% | 4.4\% | 9.1\% | -55.8\% | -16.1\% | -74.7\% | -65.2\% | 1.6\% | 1.8\% | -6.2\% | -22.4\% | 14.5\% | -0.1\% |
| 10 | Prior | 35.5 | 32.1 | 105.6 | 111.8 | 1342.2 | 43.7 | 15.3 | 219.0 | 2168.2 | 12797.9 | 2964.4 | 1802.5 | 21638.4 |
|  | After | 69.2 | 52.1 | 178.1 | 78.8 | 1084.0 | 9.9 | 5.1 | 216.9 | 1800.1 | 12033.4 | 2905.2 | 2376.9 | 20809.8 |
|  | Perc Diff | 94.8\% | 62.4\% | 68.6\% | -29.5\% | -19.2\% | -77.3\% | -66.6\% | -1.0\% | -17.0\% | -6.0\% | -2.0\% | 31.9\% | -3.8\% |
| 11 | Prior | 194.2 | 240.6 | 2915.9 | 326.0 | 7100.6 | 137.0 | 136.3 | 345.6 | 1239.4 | 3207.3 | 27529.4 | 2222.6 | 45594.9 |
|  | After | 270.0 | 222.4 | 2874.8 | 498.3 | 7040.0 | 355.4 | 71.6 | 477.3 | 1304.5 | 2968.7 | 27838.3 | 2830.1 | 46751.3 |
|  | Perc Diff | 39.0\% | -7.6\% | -1.4\% | 52.9\% | -0.9\% | 159.4\% | -47.5\% | 38.1\% | 5.2\% | -7.4\% | 1.1\% | 27.3\% | 2.5\% |
| 12 | Prior | 972.4 | 857.4 | 1884.6 | 2712.1 | 8675.6 | 5031.9 | 1995.4 | 13141.9 | 5713.3 | 2347.3 | 3293.2 | 711997.6 | 758622.7 |
|  | After | 1099.1 | 805.8 | 1564.1 | 2097.9 | 5036.3 | 4634.9 | 1876.5 | 12992.4 | 4901.3 | 2141.3 | 2185.7 | 706690.6 | 746026.0 |
|  | Perc Diff | 13.0\% | -6.0\% | -17.0\% | -22.6\% | -41.9\% | -7.9\% | -6.0\% | -1.1\% | -14.2\% | -8.8\% | -33.6\% | -0.7\% | -1.7\% |
| Dest <br> Totals | Prior | 6839.0 | 11552.0 | 28842.7 | 27583.9 | 100117.4 | 14954.1 | 12117.6 | 63634.4 | 54654.6 | 23303.1 | 49193.4 | 753660.2 | 1146452.5 |
|  | After | 7585.0 | 13327.5 | 29584.9 | 27495.6 | 99610.1 | 15910.4 | 12195.2 | 61615.0 | 52435.2 | 21342.1 | 46578.2 | 748229.8 | 1135909.1 |
|  | Perc Diff | 10.9\% | 15.4\% | 2.6\% | -0.3\% | -0.5\% | 6.4\% | 0.6\% | -3.2\% | -4.1\% | -8.4\% | -5.3\% | -0.7\% | -0.9\% |

## Appendix 3 - Journey time Graphs





J ourney Time Versus Distance Plot - Route 2: A6 Heaton
Moor To Chapel





J ourney Time Versus Distance Plot - Route 3: A537 Knutsford To Macclesfield



J ourney Time Versus Distance Plot - Route 4: A537 Macclesfield To Knutsford




Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
M ay 2017
2224-01 Report 1907







J ourney Time Versus Distance Plot - Route 7: B5087 Macclesfield To Alderley Edge



J ourney Time Versus Distance Plot - Route 8: B5087 Alderley Edge To Macclesfield



Journey Time Versus Distance Plot - Route 8: B5087
Alderley Edge To Macclesfield



Journey Time Versus Distance Plot - Route 9: M56 Manchester Airport To West Didsbury



J ourney Time Versus Distance Plot - Route 10: M56 West Didsbury To Manchester Airport



J ourney Time Versus Distance Plot - Route 10: M56 West Didsbury To Manchester Airport




J ourney Time Versus Distance Plot - Route 12: B5 166 Northenden to Wilmslow





Transport for





Transport for Greater Manchester

Highways Forecasting and Analytical Services




J ourney Time Versus Distance Plot - Route 16: A5102
Bramhall to Wilmslow





J ourney Time Versus Distance Plot - Route 17: A34 Alderley Edge to East Didsbury



J ourney Time Versus Distance Plot - Route 18: A34 East Didsbury to Alderley Edge



J ourney Time Versus Distance Plot - Route 18: A34 East Didsbury to Alderley Edge





J ourney Time Versus Distance Plot - Route 20: A523 Hazel Grove to Prestbury



J ourney Time Versus Distance Plot - Route 20: A523 Hazel Grove to Prestbury


Transport for Greater Manchester

DRAFT
Highways Forecasting and Analytical Services



J ourney Time Versus Distance Plot - Route 22: A555
Manchester Airport to Poynton




Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907


J ourney Time Versus Distance Plot - Route 23: A538 Prestbury to Hazel Grove



J ourney Time Versus Distance Plot - Route 24: A538 Hazel Grove to Prestbury



J ourney Time Versus Distance Plot - Route 24: A538 Hazel Grove to Prestbury











J ourney Time Versus Distance Plot - Route 28: Cheadle Heath to Heald Green



J ourney Time Versus Distance Plot - Route 28: Cheadle Heath to Heald Green





J ourney Time Versus Distance Plot - Route 30: A5143/9 Hazel Grove to Cheadle Hulme







J ourney Time Versus Distance Plot - Route 32: Buxton Old Rd / Higher Lane




J ourney Time Versus Distance Plot - Route 33: B5470 Chapel to Macclesfield





J ourney Time Versus Distance Plot - Route 35: B5090 / Bakestonedale Rd



J ourney Time Versus Distance Plot - Route 36: B5090 / Bakestonedale Rd



J ourney Time Versus Distance Plot - Route 36: B5090 / Bakestonedale Rd








Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907


Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907






J ourney Time Versus Distance Plot - Route 41: Roundy Lane / Middlewood Rd / Waterloo Rd






Transport for Greater Manchester

Highways Forecasting and Analytical Services








Transport for
Highways Forecasting and Analytical Services











Transport for


J ourney Time Versus Distance Plot - Route 50: A6017


Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907







Transport for Greater Manchester





Transport for



Transport for Greater Manchester

Highways Forecasting and Analytical Services
DRAFT
A6 to M 60 Relief Road
A6M 60 LM VR
May 2017
2224-01 Report 1907








J ourney Time Versus Distance Plot - Route 57: A627




Transport for
Highways Forecasting and Analytical Services



Transport for Greater Manchester


J ourney Time Versus Distance Plot - Route 59: A560




Transport for
Highways Forecasting and Analytical Services



Transport for Greater Manchester





Transport for
Highways Forecasting and Analytical Services




## Report HFAS Report 1915

## Client A6 to M60 Relief Road Project Board

Project A6 to M60 Relief Road

## Subject Forecasting Report

This Report describes the derivation of the scheme traffic forecasts used for the appraisal of the A6 to M 60 Relief Road. The forecasts produced are for an assumed opening year of 2024 and for a design year of 2039, assuming three potential growth and highway infrastructure scenarios.

| This Report | HFAS_1915_A6M60_ForecastingReport_V1.0.docx |  |  |
| ---: | :--- | ---: | :--- |
| Originator | Michael Reese | Date | Check/ Approve |
| Version | Comments |  | 010617 |
| V1.0 | Draft For Comment | MR |  |
| V2.0 | Incorporate SM BC Comments | 101117 | MR |

## CONTENTS

Page

1. Introduction ..... 1
2. The A6 to M60 Relief Road ..... 2
Scheme Description of the proposed preferred scheme ..... 2
Overview ..... 2
Mitigation Measures ..... 2
3. Development of Forecast Year Highway Networks ..... 4
4. Demand Forecasting ..... 11
5. Forecast Year Scenarios ..... 12
Development Assumptions ..... 12
Generalised Cost Parameters ..... 15
6. A6 to M60 Relief Road Traffic Impacts ..... 18
Junction Operation ..... 18
Overall Network Performance ..... 18
Scheme Re-Assignment Impacts ..... 21
Flow Differences. ..... 30
Journey Time Impacts ..... 33
7. Conclusions. ..... 40

## 1. Introduction

1.1 In 2016, Transport for Greater Manchester Highways Forecasting and Analytical Services (TfGM HFAS) was commissioned by the A6 TO M 60 Relief Road Project Board to develop traffic models for the appraisal of the proposed A6 to M 60 Relief Road.
1.2 The development of the base demand and traffic assignment models was carried out in partnership with WSPPB Consultancy, with WSPPB Transportation managing the modelling work on behalf of the client.
1.3 This report summarises the work undertaken to produce the traffic forecasts for scheme appraisal. It has seven main sections:

- Introduction;
- Description of the A6 to M60 Relief Road Scheme;
- Development of the forecast year highway networks;
- Demand forecasting;
- Forecast year scenarios;
- Traffic impacts.


## 2. The $\mathbf{A} 6$ to $\mathbf{M} 60$ Relief Road

Scheme Description of the proposed preferred scheme

## Overview

2.1 The A6 M60 Relief Road scheme includes a new 2-lane dual carriageway connecting the A6 to the M60 at Bredbury with a spur to Stepping Hill Hospital The scheme bypasses Stockport Town Centre, Hazel Grove, Offerton and Bredbury.
2.2 The scheme improves access to / from M anchester Airport and its employment areas as well as Hazel Grove, New by Road, Bramhall M oor Lane, Poynton and Stanley Green employment areas. Access to a number of regeneration areas is also improved by the scheme, including Stockport Town Centre M60 Gateway, and Wythenshawe.
2.3 The proposed scheme consists of approximately 7.5 km of new dual 2-lane and will include two new junctions and amendments to junctions at the A6 and at the M6A560 roundabout at Bredbury as well as a new junction with the A6 at Stepping Hill.
2.4 The location and extent of the scheme is shown in Figure 2.1.
2.5 The scheme has been designed to Department for Transport standards and adheres to the Design M anual for Roads and Bridges (DM RB). Any departures from approved standards will be authorised by the Director of the Overseeing Organisation.

## Mitigation Measures

2.6 It is recognised that building the A6 to M60 Relief Road will have an impact on the adjacent existing road network and that on some routes or locations mitigation measures will be required. The mitigation measures assumed in this tranche of modelling include Improvements to the junction of the A6 with Windlehurst Lane to provide additional capacity for traffic to/from Windlehurst Lane.


Figure 2.1 Proposed Alignment of scheme

## 3. Development of Forecast Year Highway Networks

3.1 The Do-Minimum networks for 2024 and 2039 were derived from the 2015 base year network. The starting network therefore contained a representation of the network structure in the base year together with traffic signal data provided by the GM traffic signals unit, Greater M anchester Urban Traffic Control (GM UTC). Further information on the content and construction of the base year networks can be found in the A6 to M60 Relief Road LMVR.
3.2 WSPPB made contact with the relevant local authorities, the Highways Agency and Manchester Airport in order to ascertain which highway schemes should be included in the Do-Minimum networks at 2024 and 2039. A package of schemes deemed to be "committed" was added to the base year network to create the new network for 2024 and 2039. To be included in this package, a scheme had to meet one or more of the following criteria:

- Scheme completed since 2015;
- Scheme construction in progress;
- Scheme funding allocated;
- Scheme is part of the Highways Agency programme; and
- Scheme likely to be completed by the forecast year(s).
3.3 HFAS subsequently coded these schemes into the validated base year SATURN assignment networks and provided them to MVA for inclusion in the Variable Demand M odel (VDM).
3.4 Table 3.1 lists highway schemes identified that are either within the Core Area of Influence or outside the Area of Influence but could affect or be affected by the A6 to M60 Relief Road Scheme in each of the forecast years and development scenario.
3.5 Besides adding these schemes, the traffic signal timings in the networks were "optimised" after convergence of the initial traffic assignment, and then subjected to a further traffic assignment convergence; automatic SATURN procedures were used to adjust the green times and offset times to minimise delays. This was done to reflect the adjustment of signals that inevitably occurs as traffic flows change over time, as well as the continuing rollout of demand-responsive control mechanisms such as SCOOT and M OVA.
3.6 Bus service and frequency data were left unaltered from 2009 because there was no information available on future changes. While a number of Quality Bus Corridor (QBC) routes are being implemented or planned in GM, in many cases the QBC measures are still in development and are insufficiently well specified to incorporate them in the model.

A6to M 60 Relief Road Forecasting Report
June 2017

| Highway Scheme | Status | Core |  |
| :---: | :---: | :---: | :---: |
|  |  | 2024 | 2039 |
| M6 Junctions 21A-26 | Committed | Y | Y |
| M56 Junctions 6-8 | Committed Advanced in Budget 2016 | Y | Y |
| M60 Junction 8 to M62 Junction 20 Smart Motorway | Under Construction; completion Summer 2017 | Y | Y |
| M60 Junctions 24-27 \& J1-4 | Committed | Y | Y |
| M60 Junction 18 | Development in RIS 1 for build in RIS2 - Advanced in Budget 2016 | Y | Y |
| M62 Junctions 10-12 | Committed Advanced in budget 2016 | Y | Y |
| M62 Junctions 20-25 | Committed Advanced in Budget 2016 | Y | Y |
| Mottram Moor Link Road | Committed | Y | Y |
| Poynton Relief Road | Likely to be completed by opening | Y | Y |
| A57(T) to A57 Link Road | Committed | Y | Y |
| A556 Knutsford to Bowdon (Cheshire East) | Under construction; completion by end-March 2017 | Y | Y |
| A6-Manchester Airport Relief Road | Under construction; | Y | Y |
| A49 Link Road | Likely to be completed by opening | Y | Y |
| M58 Link Road | Likely to be completed by opening | Y | Y |
| South Heywood Link Road | Likely to be completed by opening | Y | Y |

## Manchester Airport Future Growth Assumptions

3.7 The following section airport assumptions to feed into the highway modelling for outline assessment of the A6 to M60 road scheme. This builds on the Manchester Airport assumptions used in the development of the A6MARR model that has been used in a number of recent transport assessments, including A6 MARR, Airport City and the Manchester Airport Transformation Programme (MTP). This material has been drawn from the Manchester Airport Sustainable Development Plan (Land Use Plan and Economy and Surface Access Plan) 1 and includes:

- Future Passenger Numbers
- Future Employee Numbers
- Future Developments
- Future Surface Access Proposals


## Passenger Growth

3.8 Manchester is the third busiest airport in the UK and is the major international gateway for the north of England. In 2015 the Airport handled 23,136,000 passengers and 104,000 tonnes of cargo. The population within the 1 hour drive-tie catchment is some 8.9 million people and this increases to 22 million within the 2hour drive-time catchment. The forecasts for future growth at M anchester Airport are consistent with those prepared by the Department for Transport (DFT)2 and those used by the UK Airports Commission3. This suggests that by 2040, Manchester Airport could be handling some 45 million passengers a year. This is the forecast assumption used in the M anchester Airport Land Use Plan.
3.9 For the modelling of airport activity, the Airport's passenger and aircraft throughput is better expressed in hourly rather than annual terms. Aircraft and passenger traffic at the Airport shows significant peaks across the day with the runway demand peak between 06:00 and 08:00. This reflects aircraft that are based at the Airport and park overnight and the high proportion of passengers that are UK originating. Whilst some spreading of the peak is expected as traffic grows, the Airport's general daily traffic profile will remain similar to that of today. The 2014 and 2018 design day passenger profiles are included in the Land Use Plan, part of the Sustainable Development Plan.

[^1]Manchester Airport Terminating Passengers in 2015

| Region | Passengers <br> (millions) | $\%$ |
| :--- | :---: | :---: |
| North West | 13.62 | $60 \%$ |
| North East | 0.5 | $2 \%$ |
| Yorkshire and the Humber | 4.3 | $19 \%$ |
| The Midlands | 2.15 | $9 \%$ |
| Wales | 0.98 | $4 \%$ |
| Other Regions | 0.47 | $2 \%$ |
| Total | 22 | $97 \%$ |
| Connecting Passengers | 0.68 | $3 \%$ |
| Grand Total | 23 | $100 \%$ |
|  | CAA Passenger Survey |  |

## Staff Growth

3.10 The on-site working population at the Airport in 2015 is estimated to be 20,600. The majority of Airport staff live in Greater Manchester and in areas close to the Airport. Because of the large number and the wide variety of businesses operating on the site, detailed staff travel profiles are difficult to obtain, however the majority of the on-site workforce work shift patterns that are significantly different to a usual $9-5$ operation.
3.11 The data on staff place of residence shows that around $87 \%$ of the Airport's employees live in the North West region, with around $73 \%$ of these living in Greater Manchester and $17 \%$ in Cheshire. The distribution of Manchester Airport's employees within the Greater Manchester region is shown in the table below.

## Distribution of Airport Employees living within Greater Manchester

| District | Percentage |
| :---: | :---: |
| Bolton | $4.3 \%$ |
| Bury | $2.7 \%$ |
| Manchester | $37.3 \%$ |
| Oldham | $3.9 \%$ |
| Rochdale | $2.4 \%$ |
| Salford | $5.3 \%$ |
| Stockport | $19.5 \%$ |
| Tameside | $7.1 \%$ |
| Trafford | $11.7 \%$ |
| Wigan | $5.9 \%$ |
| Total | $100 \%$ |

3.12 The number of on-site employees will grow as the Airport's passenger and cargo activity grows. On-site employment is expected to be some 41,838 by 20404 when the Airport is handling some 45 million passengers a year. A high proportion of staff work shifts, with early shifts in the passenger operation requiring access to the Airport from 04:00.

## Developments

3.13 The Airport's Operational Area is defined in the Land Use Plan5, and for the land in Manchester, and the land use is set out in the Manchester City Council Core Strategy6. The Core Strategy defines the Airport Strategic Site and the Operational Area includes the core airport operational facilities and infrastructure along with other developments that are required for the amenity of the Airport.
3.14 In M arch 2016, the Airport secured planning consent for the M anchester Airport Transformation Programme. This is centred on a significant expansion to Terminal 2 and the demolition of Terminal 1. Expanding Terminal 2 and demolishing Terminal provides the most efficient airfield operation and provides more flexible terminal capacity. Access to Terminal 2 will be from the existing M 56 Spur and the existing T2 Elevated Roundabout.

[^2]3.15 The Airport plays an important role within the Greater Manchester economy and it sits at the heart of the Greater M anchester Enterprise Zone. This includes two sites known as Airport City.
3.16 Immediately to the north of the Airport's Operational Area, is Airport City M anchester. This is a commercial mixed use development that will include a range of uses such as offices, hotels, advanced manufacturing and support activity. To the west of the Airport is the World Logistics Hub that is being developed for freight and logistics uses.

Airport City M anchester:

- 26.3 hectares
- 113,433 sq m B1
- $49,046 \mathrm{sq} \mathrm{m} \mathrm{B1c} \mathrm{(Advanced} \mathrm{Manufacturing)}$
- 1,293 hotel beds
- 5,761 sq m of support retail and ancillary
- 4,182 car parking spaces
- Direct links to The Station (public transport)

W orld Logistics Hub:

- 36.9 hectares
- 140,000 sq m of B1 logistics
- Car parking to MCC parking standards
3.17 The assumptions on the scale and the activity of the Airport City development sites were included within the A6M ARR highway model.


## Surface Access

3.18 The approach to public transport `and future passenger and staff mode-share is set out in the Economy and Surface Access Plan. It also identifies a range of future transport measures at the Airport and in the local area. These include:

- A6 M ARR to open in 2017
- A556 Knutsford to Bowdon in 2017
- M 56-Jct 6-8 Smart M otorway - planned 2020
- $M$ anchester Airport Western Access improvements - improving the link between Terminal 2 and M 56 Jct 6 . To be complete by the time the Airport is handling some 30 million passengers a year.
- Completion of the Northern Rail Hub
- HS2 and a M anchester Airport Parkway station by 2033
- M etrolink extension to T2
- M etrolink Western Extension
- Improvements to local bus and national coach services

A6to M 60 Relief Road Forecasting Report
3.19 The Surface Access Plan includes targets for public transport use. Achieving these targets depends on the future public transport schemes. The Airport passenger mode-share targets are:

| M ode | Current | 30 mppa | 45 mppa |
| :--- | :---: | :---: | :---: |
| Kiss \& Fly/ Taxi | $52 \%$ | $40 \%$ | $30 \%$ |
| Park on Site | $21 \%$ | $18 \%$ | $15 \%$ |
| Rail | $14 \%$ | $18 \%$ | $25 \%$ |
| Park \& Ride | $8 \%$ | $14 \%$ | $17 \%$ |
| Coach \& Bus | $3 \%$ | $4 \%$ | $5 \%$ |
| Car Hire | $2 \%$ | $3 \%$ | $3 \%$ |
| M etrolink | $0 \%$ | $3 \%$ | $5 \%$ |

Currently around $80 \%$ of Airport employees use a car, either as a driver or passenger. The future staff mode-share is:

| M ode | Current | 45 mppa |
| :--- | :---: | :---: |
| Bus | $12 \%$ | $10 \%$ |
| Rail | $4 \%$ | $10 \%$ |
| Car | $79 \%$ | $57 \%$ |
| Cycle / Walk / Other | $5 \%$ | $8 \%$ |
| M etrolink | See footnote* | $15 \%$ |

[^3]
## 4. Demand Forecasting

4.1 Demand forecasts were derived using TEM PRO v7 and the development uncertainty logs provided by local authorities and other relevant organisations.
4.2 Assumptions on population and employment growth used to derive the Core forecasts came from a variety of sources, namely :

- The relevant planning departments in High Peak, Cheshire East, Manchester, Stockport, Trafford for specific developments included in their Local Development Frameworks;
- Manchester Airport Group (MAG) for passenger and employee growth and development at and around M anchester Airport;
- Local Development Framework datasets for developments elsewhere in Greater Manchester;
- The National Trip End Model (NTEM) dataset 6.2 forecasts; and
- The National Transport M odel forecasts (for freight traffic).
4.3 The methodology used to derive the Core forecasts involved:
- Application of NTEM adjusted TEM PRO growth by district to 2024 and 2039
- Addition of development growth in appropriate zone based on information provided by districts and utilising trip generation rates utilised for the A6M ARR scheme
- constraining the population and employment growth forecasts to the overall growth level implied by TEM PRO at the district level within Greater M anchester the pre-2009 district level for Cheshire East and at the county level elsewhere; and
4.4 Freight growth was applied uniformly across the whole A6 to M60 Relief Road area using data from the National Transport Model 2015 forecasts. This resulted in no difference in freight growth between the three scenarios.


## 5. Forecast Year Scenarios

5.1 This section of the report summarises the production of the forecast year scenarios for the preferred scheme and the lower cost alternative. It describes:

- assumptions about the progress of proposed developments in the vicinity of the scheme
- generalised costs used in the assignment process
- the strategy used for assigning forecast year networks (Do-M inimum and Do-Something); and
- the levels of convergence achieved for all assignments.


## Development Assumptions

5.2 The data collection process involved engaging with the various stakeholders to introduce the uncertainty log concept and the nature of the data which we required to enable the uncertainty logs to be compiled. The stakeholder parties included;

- Cheshire East Council
- High Peak Borough Council
- $\quad$ Transport for Greater M anchester (TfGM)
- Highw ays England(HE)
- M anchester Airport Group
- M anchester City Council
- Stockport M etropolitan Council
- Tameside Council; and
- Trafford Council.
5.3 Information was collected for developments which were likely to be implemented by the opening and design years of 2024 and 2039 respectively. The information received was reviewed and where necessary, alterations were undertaken and, or additional information requested, to ensure the most up to date data was collated in a format appropriate for the purposes of the uncertainty $\log$ and alternative scenario creation.
5.4 As the number of development sites is extensive and covering six districts they have not been detailed in this report but are reported in detail in WSPPB uncertainty log which is available on request.
5.5 Table 5.1 and Table 5.2 summarise total pcu tripends in the 2024 and 2039 forecast year DoM inimum and Do-Something matrices for each of the scenarios.

Transport for
Greater Manchester

Highways Forecasting and Analytical Services
A6 to M60 Relief Road
A6to M60 Relief Road Forecasting Report
2224-01 Report 1915

Table 5.1: A6M ARR Forecasts - M atrix Totals - 2024

| Time Period | User Class | Do-M inimum Core \& Do-Something Core |
| :---: | :---: | :---: |
|  |  | Grand Totals |
| AM Peak Hour | Car Commute | 87,890 |
|  | Car Employers Business | 13,052 |
|  | Car other | 83,314 |
|  | LGVs | 20,133 |
|  | OGVs | 9,330 |
|  | Total | 213,720 |
| Average Inter Peak Hour | Car Commute | 20,178 |
|  | Car Employers Business | 13,242 |
|  | Car other | 104,316 |
|  | LGVs | 19,248 |
|  | OGVs | 10,595 |
|  | Total | 167,579 |
| PM Peak Hour | Car Commute | 76,464 |
|  | Car Employers Business | 12,039 |
|  | Car other | 105,077 |
|  | LGVs | 17,037 |
|  | OGVs | 4,876 |
|  | Total | 215,493 |


| Time Period | User Class | Do-M inimum Core \& Do-Something Core |
| :---: | :---: | :---: |
|  |  | Grand Totals |
| AM Peak Hour | Car Commute | 81,064 |
|  | Car Employers Business | 12,993 |
|  | Car other | 75,682 |
|  | LGVs | 23,456 |
|  | OGVs | 8,873 |
|  | Total | 202,069 |
| Average Inter Peak Hour | Car Commute | 19,177 |
|  | Car Employers Business | 12,838 |
|  | Car other | 98,338 |
|  | LGVs | 22,163 |
|  | OGVs | 10,088 |
|  | Total | 162,605 |
| PM Peak Hour | Car Commute | 70,454 |
|  | Car Employers Business | 11,055 |
|  | Car other | 96,844 |
|  | LGVs | 19,378 |
|  | OGVs | 4,621 |
|  | Total | 202,353 |

## Generalised Cost Parameters

5.6 The generalised cost parameters used in the assignment process are derived using an Excel spreadsheet prepared by M VA for the A6M ARR study. They are consistent with data taken from TAG Unit 3.5.6 (Autumn 2015).
5.7 User inputs to the spreadsheet consist of:

- Average network speed, used in the calculation of vehicle operating costs; and
- Proportions of distance travelled by each of three car-based user classes (i.e. commute, employers business and other) as output from a five user class assignment; these are used in the calculation of the cost parameters for the all-car user class (i.e. as a weight).
5.8 All other inputs (e.g. values of time, fuel consumption parameters and fuel costs, fuel price grow th rates etc) were taken directly from the appropriate section of WebTAG.
5.9 The 2024 and 2039 values of time (pence per minute - PPM) and distance (pence per kilometre PPK) as output from the spreadsheet and used in the assignments are shown in Table 5.3 below.

Table 5.3 Generalised Cost Parameters Used in the Forecast Assignments

| Period | User Class | 2024 |  | 2039 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PPM | PPK | PPM | PPK |
| AM Peak Hour | Commuting Car | 22.98 | 6.15 | 31.02 | 5.74 |
|  | Employer's Business Car | 34.32 | 13.92 | 46.33 | 13.47 |
|  | Other Car | 15.87 | 6.15 | 21.42 | 5.74 |
|  | LGV | 24.15 | 13.84 | 32.6 | 13.81 |
|  | OGV | 24.65 | 60.72 | 33.28 | 63.76 |
| Inter-Peak Hour | Commuting Car | 23.39 | 5.66 | 31.57 | 5.29 |
|  | Employer's Business Car | 35.23 | 12.65 | 47.56 | 12.24 |
|  | Other Car | 16.89 | 5.66 | 22.8 | 5.29 |
|  | LGV | 24.15 | 13.17 | 32.6 | 13.15 |
|  | OGV | 24.65 | 54.01 | 33.28 | 56.71 |
| PM Peak Hour | Commuting Car | 23.18 | 6.04 | 31.3 | 5.64 |
|  | Employer's Business Car | 34.93 | 13.63 | 47.15 | 13.19 |
|  | Other Car | 16.61 | 6.04 | 22.42 | 5.64 |
|  | LGV | 24.15 | 13.66 | 31.6 | 13.64 |
|  | OGV | 24.65 | 59.23 | 33.28 | 62.19 |

## Forecast Year Assignments

5.10 Forecast year assignments of the A6 to M60 Relief Road model were run differently for DoMinimum and Do-Something networks. Do-M inimum tests were assigned in the following way:

- assign Do-M inimum network with corresponding Do-M inimum matrix
- optimise traffic signal green splits and offsets across the full modelled area; and
- re-assign incorporating the optimised traffic signal settings.
5.11 Do-Something tests by contrast, were assigned in the following way:
- incorporate optimised traffic signal settings from the Do-Minimum network at common junctions across the full modelled area
- assign updated network with corresponding Do-Something matrix
- optimise traffic signal green splits and offsets on and in the A6 To M 60 Relief Road area of influence; and
- re-assign incorporating the optimised traffic signal settings.
5.12 The full model assignments were then cordoned before economic appraisal of the schemes was undertaken. This was done:
- to speed up model run times while fine-tuning scheme performance (for example testing different traffic signal green splits and staging arrangements)
- to improve run times for the economic appraisal programs TUBA and COBA; and
- to reduce the possibility of including user benefits accruing in areas remote from the scheme as a result of assignment 'noise'.


## Forecast Year Assignment Convergence

5.13 W ebtag states that 'convergence is the key to robust economic appraisal' because, with a poorly converged base and/or test network, it is impossible to distinguish scheme effects from assignment 'noise'. Consequently, particular efforts were made to ensure that the networks were as highly converged as possible.
5.14 The DM RB criteria for an acceptable level of network convergence are that:

- the Delta statistic should be less than $1 \%$ on the final assignment; and
- at least $90 \%$ of links should have a flow that changes by less than $5 \%$ on the final 4 iterations.
5.15 For this work, we adopted a tighter convergence criteria than required by DM RB, requiring the perecentage Gap to be less than 0.02 . Table 5.4 summarises the convergence statistics for all scenarios and shows that all model assignments are extremely well converged.

Table 5.4: A6 to M60 Relief Road Convergence Statistics

| Scenario | Year | Test | AM Peak Hour |  |  |  |  | Average Inter-Peak Hour |  |  |  |  | PM Peak Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delta | \% Gap for Iteration |  | \% Flows for Iteration |  | Delta | \% Gap for Iteration |  | \% Flows for Iteration |  | Delta | \% Gap for Iteration |  | \% Flows for Iteration |  |
|  |  |  |  | N | N-4 | N | N-4 |  | N | N-4 | N | N-4 |  | N | $\mathrm{N}-4$ | N | N-4 |
| $\stackrel{0}{0}$ | 2024 | $\begin{aligned} & \text { Do- } \\ & \text { M in } \end{aligned}$ | 0.01 | 99.73 | 99.66 | 99.74 | 99.66 | 0.0053 | 99.51 | 99.38 | 99.4 | 99.32 | 0.017 | 99.69 | 99.59 | 99.67 | 99.63 |
|  |  | $\begin{aligned} & \hline \text { Do- } \\ & \text { Som } \end{aligned}$ | 0.012 | 99.75 | 99.76 | 99.73 | 99.59 | 0.0049 | 99.76 | 99.65 | 99.34 | 99.01 | 0.014 | 99.77 | 99.79 | 99.68 | 99.69 |
|  | 2039 | $\begin{aligned} & \text { Do- } \\ & \text { M in } \end{aligned}$ | 0.01 | 99.77 | 99.61 | 99.79 | 99.7 | 0.0048 | 99.69 | 99.64 | 99.72 | 99.28 | 0.015 | 99.68 | 99.8 | 99.56 | 99.32 |
|  |  | $\begin{aligned} & \text { Do- } \\ & \text { Som } \end{aligned}$ | 0.14 | 99.8 | 99.77 | 99.81 | 99.76 | 0.006 | 99.89 | 99.85 | 99.7 | 99.59 | 0.022 | 99.91 | 99.88 | 99.89 | 99.88 |

## 6. A6 to M60 Relief Road Traffic Impacts

6.1 This section of the report summarises the main traffic impacts of the Core A6 to M 60 Relief Road scheme, in terms of:

- impact on overall network performance
- broad re-assignment impacts
- changes in journey times.


## Junction Operation

6.2 All junctions along the proposed scheme have been assessed at various stage of the design process both within the SATURN model and in junction models such as LINSIG. This work has indicated that the junctions will operate within capacity in the opening year of 2024. Detailed assessments will be repeated following completion of the public consultation process and reflecting any consequent change in scheme design.

## Overall Network Performance

6.3 Table 6.1 summarises the network performance statistics for the Do-M inimum (DM) and DoSomething (DS) scenarios. Briefly, these statistics are aggregated over the whole modelled area (for the modelled peak-hour and the period after the peak-hour to allow the completion of any trips delayed by queues or congestion) and represent the following:

- Over-Capacity Queues - this is the time spent in queues resulting from turning movements in excess of capacity, resulting in the build-up of a permanent queue that is unable to clear in a single signal cycle;
- Total Travel Time - this is the sum of the time spent in transient and over-capacity queues plus the link cruise time;
- Travel Distance - this is the total distance travelled by all vehicles during the modelled hour; and
- Average Speed - this is simply the total distance divided by the total travel time.
6.4 The statistics shown in Table 6.1 demonstrate a decrease in the amount of time spent in over capacity queues and travel in each time period in the DS scenario compared to the DM scenario in both 2024 and 2039. This is reflected in the overall network average speed, which increases and the total number of vehicles queued at the end of the modelled hour, which decreases slightly between the DM and the DS.

These statistics demonstrate that there is an overall improvement in network performance in both test scenarios when compared against the Do-M inimum. In particular, the decrease in time spent in over-capacity queues.

Transport for
Greater Manchester

Highways Forecasting and Analytical Services
A6 to M60 Relief Road
A6to M60 Relief Road Forecasting Report 2224-01 Report 1915

| Year | Network Data | AM |  |  | IP |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | DM | DS | Diff | DM | DS | Diff | DM | DS | Diff |
|  |  |  |  | $\begin{aligned} & \text { (DS- } \\ & \text { DM) } \end{aligned}$ |  |  | $\begin{aligned} & \text { (DS } \\ & \text { DM) } \end{aligned}$ |  |  | $\begin{aligned} & \text { (DS- } \\ & \text { DM) } \\ & \hline \end{aligned}$ |
| Core |  |  |  |  |  |  |  |  |  |  |
| 2024 | Over capacity queuing (pcu hours) | 1,705 | 1,616 | -89 | 208.7 | 171 | -37.7 | 1,403 | 1,110 | -292 |
|  | Total travel time (pcu hours/ hour) | 43,639 | 42,920 | -719 | 27,438 | 27,113 | -324.9 | 45,398 | 44,388 | -1,010 |
|  | Total travel distance (km / hr) | 1,821,458 | 1,822,931 | 1,473 | 1,336,741 | 1,338,129 | 1388.2 | 1,894,566 | 1,896,101 | 1,535 |
|  | Average network speed (km/hr) | 41.7 | 42.5 | 1 | 48.7 | 49.4 | 0.7 | 41.7 | 42.7 | 1 |
| 2039 | Permanent queuing (pcus) | 4,188 | 3,424 | -764 | 469.5 | 318.3 | -151.2 | 3,535 | 3,052 | -483 |
|  | Total travel time (pcu hours per hour) | 54,728 | 52,985 | -1,743 | 32,976 | 32,313 | -663.4 | 56,231 | 54,577 | -1,654 |
|  | Total distance travelled (km per hr) | 2,060,133 | 2,059,223 | -910 | 1,530,341 | 1,528,216 | -2125.4 | 2,141,039 | 2,140,979 | -60 |
|  | Average network speed (km/hr) | 37.6 | 38.9 | 1 | 46.4 | 47.3 | 0.9 | 38.1 | 39.2 | 1 |

6.5 Tables 6.2 to 6.3 below summarise the performance of major junctions in the A6 to M 60 Relief Road area of influence at 2024 and 2039 for the morning and evening peak hours. Again, the performance figures are based on the worst turn at each junction, i.e. If a junction has a single turn in excess of $100 \%$ it is placed in the VCR $>100 \%$ category. It should be noted that the figures quoted for the Do-Something scenario include junctions along the scheme.

Table 6.2 - Junction Performance in the A6 to M60 Relief Road Area of Influence in 2024

| Junction Control | Morning Peak Hour |  |  |  | Evening Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Do-Minimum |  | Do-Something |  | Do-Minimum |  | Do-Something |  |
|  | $\begin{gathered} \text { At } \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \text { Over } \\ \text { Capacity } \end{gathered}$ | At Capacity | Over Capacity | $\begin{gathered} \text { At } \\ \text { Capacity } \end{gathered}$ | $\begin{gathered} \text { Over } \\ \text { Capacity } \end{gathered}$ | At Capacity | Over Capacity |
|  | $\begin{gathered} \text { V/C }=85 \\ -100 \% \end{gathered}$ | $\begin{aligned} & \text { V/C > } \\ & 100 \% \end{aligned}$ | $\begin{aligned} & \mathrm{V} / \mathrm{C}=85 \end{aligned}$ | $\begin{aligned} & \text { V/C }> \\ & 100 \% \end{aligned}$ | $\begin{aligned} & \text { V/C }=85 \\ & 10 n \% \end{aligned}$ | $\begin{aligned} & \text { V/C> } \\ & 100 \% \end{aligned}$ | $\mathrm{V} / \mathrm{C}=85$ | $\begin{aligned} & \text { V/C } \\ & 100 \% \end{aligned}$ |
| Signals | 71 | 38 | 64 | 31 | 69 | 28 | 58 | 22 |
| Roundabouts | 6 | 4 | 7 | 3 | 7 | 7 | 7 | 7 |
| Total | 119 |  | 105 |  | 111 |  | 94 |  |

6.6 Table 6.2 shows that in 2024 the introduction of the A6 to M 60 Relief Road scheme is forecast to result in a reduction in the number of junctions (both signalised and roundabouts) with a turn that is operating at overcapacity (VC $>100 \%$ ) from 42 to 33 and for junctions operating at capacity (VC 85-100\%) from 77 to 71 in the morning peak hour. In the evening peak hour, the number of junctions with a turn that is operating at overcapacity (VC $>100 \%$ ) is forecast to fall from 35 to 29 and for junctions operating at capacity (VC 85-100\%) from 76 to 65.

Table 6.3 - Junction Performance in the A6 to M60 Relief Road Area of Influence in 2039

| Junction Control | Morning Peak Hour |  |  |  | Evening Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Do-Minimum |  | Do-Something |  | Do-Minimum |  | Do-Something |  |
|  | At Capacity | Over Capacity | At Capacity | Over Capacity | At Capacity | Over Capacity | At Capacity | Over Capacity |
|  | V/C = 85 | V/C > | V/C = 85 | V/C > | V/C $=85$ | V/C > | V/C = 85 | V/C > |
|  | -100\% | 100\% | -100\% | 100\% | -100\% | 100\% | -100\% | 100\% |
| Signals | 93 | 63 | 77 | 55 | 91 | 46 | 79 | 41 |
| Roundabouts | 8 | 6 | 9 | 5 | 7 | 8 | 4 | 10 |
| Total | 170 |  | 146 |  | 152 |  | 134 |  |

6.7 Table 6.3 shows that in 2039 the introduction of the A6 to M 60 Relief Road scheme is forecast to result in a reduction in the number of junctions (both signalised and roundabouts) with a turn that is operating at overcapacity (VC $>100 \%$ ) from 69 to 54 and for junctions operating at capacity (VC 85-100\%) from 101 to 86 in the morning peak hour. In the evening peak hour, the number of junctions with a turn that is operating at overcapacity ( $\mathrm{VC}>100 \%$ ) is forecast to fall from 54 to 51 and for junctions operating at capacity (VC 85-100\%) from 98 to 83.

## Scheme Re-Assignment Impacts

6.8 The analysis of the traffic impacts of the A6 to M60 Relief Road scheme is based on an analysis of traffic flows crossing five screenlines across the study area. The screenlines are illustrated in Figure 6.1.

Screenline 1 Tameside to Stockport to Manchester North of Scheme Screenline to intercept North-South traffic movements through in the Northern area of influence.

Screenline $\mathbf{2}$ Bredbury to High Lane East-West traffic movements through the area of influence. It extends from Disley in the East to Wilmslow in the West.

Screenline 3 Bredbury to Heald Green North-South traffic movements through the Southern area of influence.
6.9 Tables 6.4 to 6.6 summarise 2024 and 2039 actual flows (in pcus) on all links crossing Screenlines 1 to 5 respectively in the Do-M inimum and Do-Something scenarios.
6.10 Table 6.4 shows that in the Northbound direction flows are forecast to increase on the M60 North of Brinnington in all time periods at 2024 and 2039. The remaining links are forecast to remain broadly neutral or to reduce particularly on the A5145 Didsbury Road in the morning peak in both forecast years.
6.11 In the Southbound direction, flows are forecast to significantly increase on the M60 North of Brinnington Bypass in all time periods at 2024 and 2039in some cases by over 100 pcu's. Overall, the forecast change in flow across the screenline in either direction ranges from $-3 \%$ to $-+10 \%$ in any one time period and forecast year.
6.12 Table 6.5 shows that in both directions flows are forecast to decrease particularly on the A6 Buxton Road and Otterspool Road for all time periods in 2024 and 2039. Overall, the forecast change in flow across the screenline in either direction ranges from $0 \%$ to $+7 \%$ in any one time period and forecast year.
6.13 Table 6.6 shows that in the both directions flows are forecast to decrease on the A6 Wellington Road South and Longshut Lane West with the maximum decrease of up to $30 \%$ in either direction. Overall, the forecast change in flow across the screenline in either direction ranges from $+1 \%$ to $-12 \%$ in any one time period and forecast year.


| Crossing Links | Time Period | Northbound |  |  |  |  |  |  |  | Southbound |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. Werneth Low Road | AM | 242 | 216 | -26 | -11\% | 309 | 259 | -50 | -16\% | 181 | 216 | 35 | 19\% | 251 | 259 | 8 | 3\% |
| 2. A560 Stockport Road |  | 135 | 117 | -18 | -13\% | 182 | 128 | -54 | -30\% | 265 | 117 | -148 | -56\% | 290 | 128 | -162 | -56\% |
| 3. A627 Dowson Road |  | 540 | 488 | -52 | -10\% | 680 | 596 | -84 | -12\% | 491 | 488 | -3 | -1\% | 555 | 596 | 41 | 7\% |
| 4. Ashton Road |  | 539 | 536 | -3 | -1\% | 655 | 647 | -8 | -1\% | 1097 | 536 | -561 | -51\% | 1336 | 647 | -689 | -52\% |
| 5. M60 North of Brinnington |  | 6036 | 6176 | 140 | 2\% | 6657 | 7005 | 348 | 5\% | 4861 | 6176 | 1315 | 27\% | 5966 | 7005 | 1039 | 17\% |
| 6. B6167 Sandy Lane |  | 995 | 986 | -9 | -1\% | 1060 | 1008 | -52 | -5\% | 917 | 986 | 69 | 8\% | 963 | 1008 | 45 | 5\% |
| 7. A626 M anchester Road |  | 524 | 598 | 74 | 14\% | 641 | 611 | -30 | -5\% | 851 | 598 | -253 | -30\% | 858 | 611 | -247 | -29\% |
| 8. Belmont Way |  | 195 | 230 | 35 | 18\% | 132 | 270 | 138 | 105\% | 243 | 230 | -13 | -5\% | 277 | 270 | -7 | -3\% |
| 9. A6 Wellington Road North |  | 1053 | 1011 | -42 | -4\% | 1083 | 1146 | 63 | 6\% | 1298 | 1011 | -287 | -22\% | 1460 | 1146 | -314 | -22\% |
| 10. A5145 Didsbury Road |  | 1113 | 1197 | 84 | 8\% | 1231 | 1294 | 63 | 5\% | 1197 | 1197 | 0 | 0\% | 1314 | 1294 | -20 | -2\% |
| 11. B5095 Wilmslow Road |  | 985 | 743 | -242 | -25\% | 1276 | 1102 | -174 | -14\% | 722 | 743 | 21 | 3\% | 814 | 1102 | 288 | 35\% |
| 12. A34 Kingsway |  | 1503 | 1665 | 162 | 11\% | 1291 | 1508 | 217 | 17\% | 1729 | 1665 | -64 | -4\% | 1896 | 1508 | -388 | -20\% |
| 13. B5167 Palatine Road |  | 872 | 819 | -53 | -6\% | 1005 | 973 | -32 | -3\% | 727 | 819 | 92 | 13\% | 1003 | 973 | -30 | -3\% |
| Total |  | 14732 | 14782 | 50 | 0\% | 16202 | 16547 | 345 | 2\% | 14579 | 14782 | 203 | 1\% | 16983 | 16547 | -436 | -3\% |
| 1. Werneth Low Road | IP | 92 | 75 | -17 | -18\% | 108 | 95 | -13 | -12\% | 122 | 75 | -47 | -39\% | 180 | 95 | -85 | -47\% |
| 2. A560 Stockport Road |  | 153 | 154 | 1 | 1\% | 198 | 198 | 0 | 0\% | 174 | 154 | -20 | -11\% | 199 | 198 | -1 | -1\% |
| 3. A627 Dowson Road |  | 463 | 456 | -7 | -2\% | 491 | 515 | 24 | 5\% | 406 | 456 | 50 | 12\% | 473 | 515 | 42 | 9\% |
| 4. Ashton Road |  | 510 | 503 | -7 | -1\% | 586 | 585 | -1 | 0\% | 457 | 503 | 46 | 10\% | 564 | 585 | 21 | 4\% |
| 5. M60 North of Brinnington |  | 4697 | 4772 | 75 | 2\% | 5600 | 5676 | 76 | 1\% | 4598 | 4772 | 174 | 4\% | 5318 | 5676 | 358 | 7\% |
| 6. B6167 Sandy Lane |  | 957 | 936 | -21 | -2\% | 1035 | 1069 | 34 | 3\% | 1011 | 936 | -75 | -7\% | 1001 | 1069 | 68 | 7\% |
| 7. A626 M anchester Road |  | 807 | 848 | 41 | 5\% | 806 | 838 | 32 | 4\% | 711 | 848 | 137 | 19\% | 788 | 838 | 50 | 6\% |
| 8. Belmont Way |  | 290 | 383 | 93 | 32\% | 317 | 390 | 73 | 23\% | 331 | 383 | 52 | 16\% | 377 | 390 | 13 | 3\% |
| 9. A6 Wellington Road North |  | 929 | 872 | -57 | -6\% | 1029 | 997 | -32 | -3\% | 930 | 872 | -58 | -6\% | 1094 | 997 | -97 | -9\% |
| 10. A5145 Didsbury Road |  | 901 | 930 | 29 | 3\% | 1045 | 1065 | 20 | 2\% | 1194 | 930 | -264 | -22\% | 1101 | 1065 | -36 | -3\% |
| 11. B5095 Wilmslow Road |  | 437 | 440 | 3 | 1\% | 548 | 508 | -40 | -7\% | 516 | 440 | -76 | -15\% | 687 | 508 | -179 | -26\% |
| 12. A34 Kingsway |  | 1385 | 1378 | -7 | -1\% | 1606 | 1604 | -2 | 0\% | 1101 | 1378 | 277 | 25\% | 1302 | 1604 | 302 | 23\% |
| 13. B5167 Palatine Road |  | 496 | 498 | 2 | 0\% | 634 | 608 | -26 | -4\% | 538 | 498 | -40 | -7\% | 699 | 608 | -91 | -13\% |
| Total |  | 12117 | 12245 | 128 | 1\% | 14003 | 14148 | 145 | 1\% | 12089 | 12245 | 156 | 1\% | 13783 | 14148 | 365 | 3\% |


| Crossing Links | Time Period | Northbound |  |  |  |  |  |  |  | Southbound |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. Werneth Low Road | PM | 179 | 109 | -70 | -39\% | 279 | 187 | -92 | -33\% | 234 | 109 | -125 | -53\% | 267 | 187 | -80 | -30\% |
| 2. A560 Stockport Road |  | 370 | 357 | -13 | -4\% | 349 | 356 | 7 | 2\% | 229 | 357 | 128 | 56\% | 268 | 356 | 88 | 33\% |
| 3. A627 Dowson Road |  | 467 | 462 | -5 | -1\% | 563 | 714 | 151 | 27\% | 634 | 462 | -172 | -27\% | 729 | 714 | -15 | -2\% |
| 4. Ashton Road |  | 945 | 1045 | 100 | 11\% | 982 | 1120 | 138 | 14\% | 602 | 1045 | 443 | 74\% | 624 | 1120 | 496 | 79\% |
| 5. M60 North of Brinnington |  | 6204 | 6413 | 209 | 3\% | 7241 | 6990 | -251 | -3\% | 5303 | 6413 | 1110 | 21\% | 6322 | 6990 | 668 | 11\% |
| 6. B6167 Sandy Lane |  | 1065 | 1025 | -40 | -4\% | 1079 | 1047 | -32 | -3\% | 920 | 1025 | 105 | 11\% | 1005 | 1047 | 42 | 4\% |
| 7. A626 M anchester Road |  | 756 | 780 | 24 | 3\% | 813 | 779 | -34 | -4\% | 798 | 780 | -18 | -2\% | 742 | 779 | 37 | 5\% |
| 8. Belmont Way |  | 187 | 261 | 74 | 40\% | 367 | 408 | 41 | 11\% | 278 | 261 | -17 | -6\% | 303 | 408 | 105 | 35\% |
| 9. A6 Wellington Road North |  | 1055 | 982 | -73 | -7\% | 1167 | 1161 | -6 | -1\% | 961 | 982 | 21 | 2\% | 1110 | 1161 | 51 | 5\% |
| 10. A5145 Didsbury Road |  | 1313 | 1328 | 15 | 1\% | 1355 | 1378 | 23 | 2\% | 1091 | 1328 | 237 | 22\% | 1304 | 1378 | 74 | 6\% |
| 11. B5095 Wilmslow Road |  | 670 | 544 | -126 | -19\% | 808 | 690 | -118 | -15\% | 1096 | 544 | -552 | -50\% | 1154 | 690 | -464 | -40\% |
| 12. A34 Kingsway |  | 1546 | 1689 | 143 | 9\% | 1691 | 1902 | 211 | 12\% | 1734 | 1689 | -45 | -3\% | 1812 | 1902 | 90 | 5\% |
| 13. B5167 Palatine Road |  | 1054 | 1098 | 44 | 4\% | 1046 | 1121 | 75 | 7\% | 714 | 1098 | 384 | 54\% | 947 | 1121 | 174 | 18\% |
| Total |  | 15811 | 16093 | 282 | 2\% | 17740 | 17853 | 113 | 1\% | 14594 | 16093 | 1499 | 10\% | 16587 | 17853 | 1266 | 8\% |

# Highways Forecasting and Analytical Services 

A6 to M60 Relief Road
A6to M60 Relief Road Forecasting Report

| Crossing Links | Time Period | Northbound |  |  |  |  |  |  |  | Southbound |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. A6 Buxton Road | AM | 881 | 962 | 81 | 9\% | 978 | 1136 | 158 | 16\% | 962 | 1098 | 136 | 14\% | 832 | 929 | 97 | 12\% |
| 2. Windlehurst Road |  | 232 | 148 | -84 | -36\% | 278 | 168 | -110 | -40\% | 347 | 221 | -126 | -36\% | 242 | 118 | -124 | -51\% |
| 3. A626 Buxton Road |  | 976 | 788 | -188 | -19\% | 1144 | 931 | -213 | -19\% | 1443 | 1415 | -28 | -2\% | 1271 | 1198 | -73 | -6\% |
| 4. A627 Otterspool Road |  | 661 | 462 | -199 | -30\% | 828 | 600 | -228 | -28\% | 704 | 347 | -357 | -51\% | 955 | 732 | -223 | -23\% |
| 5. B6104 Stockport Road |  | 542 | 545 | 3 | 1\% | 603 | 613 | 10 | 2\% | 840 | 835 | -5 | -1\% | 744 | 659 | -85 | -11\% |
| 6. Stockport Road East |  | 529 | 498 | -31 | -6\% | 626 | 588 | -38 | -6\% | 1084 | 1115 | 31 | 3\% | 896 | 874 | -22 | -2\% |
| 7. Ashton Road |  | 539 | 536 | -3 | -1\% | 655 | 647 | -8 | -1\% | 1097 | 1062 | -35 | -3\% | 624 | 681 | 57 | 9\% |
| Total |  | 4360 | 3939 | -421 | -10\% | 5112 | 4683 | -429 | -8\% | 6477 | 6093 | -384 | -6\% | 5564 | 5191 | -373 | -7\% |
| 1. A6 Buxton Road | IP | 859 | 930 | 71 | 8\% | 1112 | 1210 | 98 | 9\% | 776 | 937 | 161 | 21\% | 832 | 929 | 97 | 12\% |
| 2. Windlehurst Road |  | 270 | 192 | -78 | -29\% | 333 | 228 | -105 | -32\% | 174 | 123 | -51 | -29\% | 242 | 118 | -124 | -51\% |
| 3. A626 Buxton Road |  | 1006 | 837 | -169 | -17\% | 1280 | 1014 | -266 | -21\% | 1134 | 1067 | -67 | -6\% | 1271 | 1198 | -73 | -6\% |
| 4. A627 Otterspool Road |  | 600 | 499 | -101 | -17\% | 626 | 518 | -108 | -17\% | 748 | 419 | -329 | -44\% | 955 | 732 | -223 | -23\% |
| 5. B6104 Stockport Road |  | 636 | 658 | 22 | 3\% | 678 | 729 | 51 | 8\% | 575 | 616 | 41 | 7\% | 744 | 659 | -85 | -11\% |
| 6. Stockport Road East |  | 706 | 703 | -3 | 0\% | 766 | 826 | 60 | 8\% | 750 | 746 | -4 | -1\% | 896 | 874 | -22 | -2\% |
| 7. Ashton Road |  | 510 | 503 | -7 | -1\% | 586 | 585 | -1 | 0\% | 457 | 447 | -10 | -2\% | 624 | 681 | 57 | 9\% |
| Total |  | 4587 | 4322 | -265 | -6\% | 5381 | 5110 | -271 | -5\% | 4614 | 4355 | -259 | -6\% | 5564 | 5191 | -373 | .7\% |

# Highways Forecasting and Analytical Services 

A6 to M60 Relief Road
A6to M60 Relief Road Forecasting Report

| Crossing Links | Time Period | Eastbound |  |  |  |  |  |  |  | Westbound |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. A6 Buxton Road | PM | 1063 | 1191 | 128 | 12\% | 1112 | 1368 | 256 | 23\% | 856 | 950 | 94 | 11\% | 832 | 929 | 97 | 12\% |
| 2. Windlehurst Road |  | 474 | 323 | -151 | -32\% | 603 | 460 | -143 | -24\% | 191 | 103 | -88 | -46\% | 242 | 118 | -124 | -51\% |
| 3. A626 Buxton Road |  | 1483 | 1274 | -209 | -14\% | 1495 | 1419 | -76 | -5\% | 1005 | 936 | -69 | -7\% | 1271 | 1198 | -73 | -6\% |
| 4. A627 Otterspool Road |  | 663 | 419 | -244 | -37\% | 829 | 474 | -355 | -43\% | 937 | 610 | -327 | -35\% | 955 | 732 | -223 | -23\% |
| 5. B6104 Stockport Road |  | 834 | 879 | 45 | 5\% | 962 | 1051 | 89 | 9\% | 655 | 639 | -16 | -2\% | 744 | 659 | -85 | -11\% |
| 6. Stockport Road East |  | 879 | 850 | -29 | -3\% | 901 | 1044 | 143 | 16\% | 806 | 786 | -20 | -2\% | 896 | 874 | -22 | -2\% |
| 7. Ashton Road |  | 945 | 1045 | 100 | 11\% | 982 | 1120 | 138 | 14\% | 602 | 594 | -8 | -1\% | 624 | 681 | 57 | 9\% |
| Total |  | 6341 | 5981 | -360 | -6\% | 6884 | 6936 | 52 | 1\% | 5052 | 4618 | -434 | -9\% | 5564 | 5191 | -373 | -7\% |


| $\bigcap \Omega \begin{aligned} & \text { Transport for } \\ & \text { Greater Manchester } \end{aligned}$ | Highways Forecasting and Analytical Services |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A6 to M 60 Relief Road A6to M60 Relief Road Forecasting Report |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | June 2017 |  |  |  |  | 2224-01 Report 1915 |  |  |  |  |  |  |  |  |  |  |  |
| Table 6.6: A6 to M60 Relief R | oad Scre | ine 3 | redbur | o | Gree | cree | - | ng | s in |  |  |  |  |  |  |  |  |
|  | Time Period | Eastbound |  |  |  |  |  |  |  | Westbound |  |  |  |  |  |  |  |
| Crossing Links |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. Ashton Road | AM | 539 | 536 | -3 | -1\% | 655 | 647 | -8 | -1\% | 1097 | 1062 | -35 | -3\% | 1336 | 1244 | -92 | -7\% |
| 2. Stockport Road West |  | 1604 | 1396 | -208 | -13\% | 1704 | 1592 | -112 | -7\% | 1047 | 892 | -155 | -15\% | 1109 | 1008 | -101 | -9\% |
| 3. Osborne Street |  | 534 | 535 | 1 | 0\% | 488 | 498 | 10 | 2\% | 183 | 237 | 54 | 30\% | 261 | 269 | 8 | 3\% |
| 4. A626 Offerton Lane |  | 543 | 720 | 177 | 33\% | 550 | 772 | 222 | 40\% | 226 | 649 | 423 | 187\% | 318 | 699 | 381 | 120\% |
| 5. Dialstone Lane |  | 565 | 472 | -93 | -16\% | 622 | 451 | -171 | -27\% | 455 | 285 | -170 | -37\% | 438 | 305 | -133 | -30\% |
| 6. Nangreave Road |  | 193 | 170 | -23 | -12\% | 253 | 195 | -58 | -23\% | 195 | 173 | -22 | -11\% | 274 | 186 | -88 | -32\% |
| 7. Hillgate |  | 621 | 451 | -170 | -27\% | 719 | 507 | -212 | -29\% | 521 | 428 | -93 | -18\% | 514 | 496 | -18 | -4\% |
| 8. Longshut Lane |  | 336 | 323 | -13 | -4\% | 503 | 444 | -59 | -12\% | 226 | 249 | 23 | 10\% | 250 | 297 | 47 | 19\% |
| 9. A6 Wellington Road South |  | 498 | 362 | -136 | -27\% | 589 | 424 | -165 | -28\% | 515 | 364 | -151 | -29\% | 558 | 453 | -105 | -19\% |
| 10. B5465 Longshut Lane West |  | 1322 | 1108 | -214 | -16\% | 1401 | 1228 | -173 | -12\% | 808 | 863 | 55 | 7\% | 900 | 930 | 30 | 3\% |
| 11. Dale Street |  | 559 | 524 | -35 | -6\% | 676 | 536 | -140 | -21\% | 402 | 383 | -19 | -5\% | 384 | 349 | -35 | -9\% |
| 12. Councillor Lane |  | 578 | 530 | -48 | -8\% | 635 | 660 | 25 | 4\% | 389 | 417 | 28 | 7\% | 461 | 450 | -11 | -2\% |
| 13.Cheadle Road |  | 673 | 651 | -22 | -3\% | 872 | 756 | -116 | -13\% | 393 | 371 | -22 | -6\% | 414 | 471 | 57 | 14\% |
| 14. A34 Bypass |  | 2870 | 2598 | -272 | -9\% | 2546 | 2437 | -109 | -4\% | 2726 | 2423 | -303 | -11\% | 2777 | 2452 | -325 | -12\% |
| Total |  | 8565 | 7778 | -787 | -9\% | 9667 | 8710 | -1066 | -11\% | 6457 | 6373 | -84 | -1\% | 7217 | 7157 | -60 | -1\% |
| 1. Ashton Road | IP | 510 | 503 | -7 | -1\% | 586 | 585 | -1 | 0\% | 457 | 447 | -10 | -2\% | 564 | 540 | -24 | -4\% |
| 2. Stockport Road West |  | 1334 | 1164 | -170 | -13\% | 1517 | 1306 | -211 | -14\% | 1673 | 1502 | -171 | -10\% | 1744 | 1722 | -22 | -1\% |
| 3. Osborne Street |  | 347 | 272 | -75 | -22\% | 396 | 337 | -59 | -15\% | 339 | 475 | 136 | 40\% | 288 | 463 | 175 | 61\% |
| 4. A626 Offerton Lane |  | 293 | 348 | 55 | 19\% | 372 | 398 | 26 | 7\% | 295 | 591 | 296 | 100\% | 439 | 732 | 293 | 67\% |
| 5. Dialstone Lane |  | 545 | 471 | -74 | -14\% | 610 | 525 | -85 | -14\% | 419 | 303 | -116 | -28\% | 392 | 327 | -65 | -17\% |
| 6. Nangreave Road |  | 121 | 112 | -9 | -7\% | 121 | 129 | 8 | 7\% | 210 | 186 | -24 | -11\% | 266 | 262 | -4 | -2\% |
| 7. Hillgate |  | 616 | 594 | -22 | -4\% | 687 | 698 | 11 | 2\% | 647 | 581 | -66 | -10\% | 705 | 673 | -32 | -5\% |
| 8. Longshut Lane |  | 280 | 236 | -44 | -16\% | 360 | 285 | -75 | -21\% | 213 | 289 | 76 | 36\% | 232 | 334 | 102 | 44\% |
| 9. A6 Wellington Road South |  | 374 | 237 | -137 | -37\% | 547 | 298 | -249 | -46\% | 343 | 229 | -114 | -33\% | 459 | 274 | -185 | -40\% |
| 10. B5465 Longshut Lane West |  | 1216 | 1172 | -44 | -4\% | 1231 | 1196 | -35 | -3\% | 1172 | 1212 | 40 | 3\% | 1231 | 1301 | 70 | 6\% |

Transport for
Greater Manchester

Highways Forecasting and Analytical Services
A6 to M60 Relief Road
A6to M 60 Relief Road Forecasting Report 2224-01 Report 1915

| 11. Dale Street | 328 | 313 | -15 | -5\% | 435 | 370 | -65 | -15\% | 355 | 342 | -13 | -4\% | 418 | 336 | -82 | -20\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12. Councillor Lane | 332 | 353 | 21 | 6\% | 391 | 376 | -15 | -4\% | 435 | 400 | -35 | -8\% | 484 | 461 | -23 | -5\% |
| 13.Cheadle Road | 382 | 393 | 11 | 3\% | 568 | 471 | -97 | -17\% | 390 | 401 | 11 | 3\% | 579 | 481 | -98 | -17\% |
| 14. A34 Bypass | 1942 | 1760 | -182 | -9\% | 2257 | 2159 | -98 | -4\% | 1817 | 1634 | -183 | -10\% | 2118 | 1878 | -240 | -11\% |
| Total | 6678 | 6168 | -510 | -8\% | 7821 | 6974 | -945 | -12\% | 6948 | 6958 | 10 | 0\% | 7801 | 7906 | 105 | 1\% |


| Crossing Links | Time Period | Eastbound |  |  |  |  |  |  |  | Westbound |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2024 |  |  |  | 2039 |  |  |  | 2024 |  |  |  | 2039 |  |  |  |
|  |  | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff | DM | DS | Diff | \% Diff |
| 1. Ashton Road | PM | 945 | 1045 | 100 | 11\% | 982 | 1120 | 138 | 14\% | 602 | 594 | -8 | -1\% | 624 | 681 | 57 | 9\% |
| 2. Stockport Road W est |  | 1214 | 962 | -252 | -21\% | 1254 | 994 | -260 | -21\% | 1507 | 1549 | 42 | 3\% | 1712 | 1607 | -105 | -6\% |
| 3. Osborne Street |  | 312 | 319 | 7 | 2\% | 340 | 329 | -11 | -3\% | 487 | 339 | -148 | -30\% | 487 | 556 | 69 | 14\% |
| 4. A626 Offerton Lane |  | 329 | 317 | -12 | -4\% | 490 | 377 | -113 | -23\% | 586 | 884 | 298 | 51\% | 786 | 966 | 180 | 23\% |
| 5. Dialstone Lane |  | 508 | 263 | -245 | -48\% | 492 | 264 | -228 | -46\% | 523 | 288 | -235 | -45\% | 591 | 298 | -293 | -50\% |
| 6. Nangreave Road |  | 84 | 56 | -28 | -33\% | 129 | 79 | -50 | -39\% | 201 | 280 | 79 | 39\% | 381 | 396 | 15 | 4\% |
| 7. Hillgate |  | 779 | 800 | 21 | 3\% | 672 | 775 | 103 | 15\% | 825 | 777 | -48 | -6\% | 765 | 810 | 45 | 6\% |
| 8. Longshut Lane |  | 348 | 263 | -85 | -24\% | 400 | 361 | -39 | -10\% | 414 | 429 | 15 | 4\% | 486 | 465 | -21 | -4\% |
| 9. A6 Wellington Road South |  | 397 | 305 | -92 | -23\% | 535 | 353 | -182 | -34\% | 965 | 645 | -320 | -33\% | 1028 | 781 | -247 | -24\% |
| 10. B5465 Longshut Lane West |  | 1232 | 1095 | -137 | -11\% | 1177 | 1133 | -44 | -4\% | 885 | 938 | 53 | 6\% | 1006 | 919 | -87 | -9\% |
| 11. Dale Street |  | 463 | 419 | -44 | -10\% | 525 | 470 | -55 | -10\% | 275 | 278 | 3 | 1\% | 299 | 288 | -11 | -4\% |
| 12. Councillor Lane |  | 325 | 351 | 26 | 8\% | 304 | 377 | 73 | 24\% | 769 | 733 | -36 | -5\% | 861 | 837 | -24 | -3\% |
| 13.Cheadle Road |  | 621 | 548 | -73 | -12\% | 736 | 614 | -122 | -17\% | 543 | 491 | -52 | -10\% | 569 | 525 | -44 | -8\% |
| 14. A34 Bypass |  | 2488 | 2426 | -62 | -2\% | 2532 | 2605 | 73 | 3\% | 2412 | 2238 | -174 | -7\% | 2555 | 2503 | -52 | -2\% |
| Total |  | 7557 | 6743 | -814 | -11\% | 8036 | 7246 | -717 | -9\% | 8582 | 8225 | -357 | -4\% | 9595 | 9129 | -466 | -5\% |

## Flow Differences

6.14 Figures 6.2 and 6.3 show forecast changes in AADT flow between the Do-M inimum and the DoSomething and scenario for the 2024 and 2039 in the A6 to M 60 Relief Road area of influence. The plots show flow differences represented by variable width bands, where the width of the band is proportional to the magnitude of the change. Increases in actual flows are shown in green and decreases in blue.
6.15 As expected, the most significant forecast increases in flow in the A6 to M 60 Relief Road area of influence as a result of the scheme are on:

- A6 Buxton Road (South of its junction with A6to M60 Relief Road)
- A6M ARR East of Poynton Relief Road
- M60 North of Brinnington
- A523 M acclesfield Road South of Hazel Grove
6.16 The most significant forecast decreases in flow occur on the local road network in the Heald Green and Wythenshawe area and Bramhall to the North of the scheme. Other routes with significant decreases in flow as a result of the scheme include:
- A6 through Stockport and Hazel Grove
- A627 Otterspool Road
- M60 Junction 25 to 3
- M56
- A34 South of the M60A538 Wilmslow Road


Figure 6.2 2024 AADT Flow Differences (Do-Min to Do-Som)


Figure 6.3 2039 AADT Flow Differences (Do-Min to Do-Som)

## Journey Time Impacts

6.17 Table 6.7 lists the journey time routes in the area of influence of the A6 to M60 Relief Road scheme and illustrated in Figure 6.4. The journey time data from the AM, IP and PM peak-hour 2024 and 2039 Core Do-M inimum and Do-Something for thirty-one routes in each direction are summarised in Table 6.8 and Table 6.9 for 2024 and 2039 respectively. Differences in travel time (Do-M inimum to Do-Something) greater than plus 60 seconds are highlighted in red and greater than minus 60 seconds in green
6.18 The tables indicate that with A 6 to M 60 Relief Road in place journey times are forecast to decrease in the northbound directions on the A6 Buxton Road (High Lane to Heaton Moor) in all time periods up to approximately three-to four minutes. In the southbound direction the journey times are forecast to rise in the morning and interpeak by approximately one to two minutes and decrease in the evening peak by two to three minutes
6.19 Journey times are forecast to increase in the morning peak in 2024 on the A523 Macclesfield Road (Prestbury to Hazel Grove) Northbound by approximately one. The route from Chapel-en-le-Frith to M acclesfield is forecast to increase by two minutes in the 2039 evening peak/
6.20 The journey times on the M60 are forecast to remain broadly neutral in 2024 but will decrease more significantly in 2029 particularly in the clockwise direction in the morning peak.

| Route No. | Description | Direction | Route Length M odelled KM |
| :---: | :---: | :---: | :---: |
| 1 | A6 Chapel to Heaton Moor | NW | 8.7 |
|  | A6 Heaton M oor to Chapel | SE | 8.7 |
| 2 | A537 Knutsford to M acclesfield | E | 16.4 |
|  | A537 M acclesfield to Knutsford | W | 16.4 |
| 3 | B5085 Knutsford to Alderley Edge | E | 10.2 |
|  | B5085 Alderley Edge to Knutsford | W | 10.2 |
| 4 | B5087 M acclesfield to Alderley Edge | NW | 6.6 |
|  | B5087 Alderley Edge to M acclesfield | SE | 6.6 |
| 5 | M 56 M anchester Airport to West Didsbury | N | 7.3 |
|  | M 56 West Didsbury to M anchester Airport | S | 6.8 |
| 6 | B5166 Wilmslow to Northenden | N | 10 |
|  | B5166 Northenden to Wilmslow | S | 10 |
| 7 | M 56 J8 to J5 | E | 8.4 |
|  | M 56 J 5 to J8 | W | 8.4 |
| 8 | A5102 Wilmslow to Bramhall | NE | 7.6 |
|  | A5102 Bramhall to Wilmslow | SW | 7.6 |
| 9 | A34 Alderley Edge to East Didsbury | N | 14.4 |
|  | A34 East Didsbury to Alderley Edge | S | 14.3 |
| 10 | A523 Prestbury to Hazel Grove | N | 10.1 |
|  | A523 Hazel Grove to Prestbury | S | 10 |
| 11 | A555 M AELR Poynton to M anchester Airport | W | 14.4 |
|  | A555 M AELR M anchester Airport to Poynton | E | 14.4 |
| 12 | A538 Prestbury to Hale | NW | 22.1 |
|  | A538 Hale to Prestbury | SE | 22.1 |
| 13 | M60 J6 to J24 | AC | 17 |
|  | M 60 J24 to J6 | CW | 17.2 |
| 14 | Heald Green to Cheadle Heath | NE | 5.2 |
|  | Cheadle Heath to Heald Green | SW | 5.2 |
| 15 | A5149/3 Cheadle Hulme to Hazel Grove | E | 5.8 |
|  | A5143/9 Hazel Grove to Cheadle Hulme | W | 5.8 |
| 16 | Buxton Old Road / Higher Lane | SB | 6 |
|  | Buxton Old Road / Higher Lane | NB | 6 |
| 17 | B5470 Chapel To M acclesfield | SB | 16.5 |
|  | B5470 M acclesfield To Chapel | NB | 16.5 |
| 18 | B5090 / Bakestonedale Rd | WB | 8.1 |
|  | B5090 / Bakestonedale Rd | EB | 8.1 |
| 19 | Bakestonedale Rd/ Brookledge Lane / M ill Lane | WB | 9.7 |
|  | Bakestonedale Rd/ Brookledge Lane / M ill Lane | EB | 9.7 |
| 20 | B5358 | NB | 8.9 |
|  | B5358 | SB | 8.9 |
| 21 | Roundy Lane / M idd lewood Rd/ Waterloo Rd | NB | 7.3 |
|  | Roundy Lane / M iddlewood Rd/ Waterloo Rd | SB | 7.3 |
| 22 | B5465 / A626 | NB | 2.1 |
|  | B5465 / A626 | SB | 2.1 |
| 23 | A626 | NB | 4.9 |
|  | A626 | SB | 4.9 |
| 24 | A560 | NB | 3.9 |
|  | A560 | SB | 3.9 |
| 25 | A6017 | NB | 3.9 |
|  | A6017 | SB | 3.9 |
| 26 | A560 / A627 | NB | 6.6 |
|  | A560 / A627 | SB | 6.6 |
| 27 | A626 | NB | 11.9 |
|  | A626 | SB | 11.9 |
| 28 | A560 | NB | 4.9 |
|  | A560 | SB | 4.9 |
| 29 | A627 | NB | 6.4 |
|  | A627 | SB | 6.4 |
| 30 | A560 | NB | 7.1 |
|  | A560 | SB | 7.1 |
| 31 | B6104 | NB | 5.8 |
|  | B6104 | SB | 5.8 |



Figure 6.4 Journey Time Routes

Highways Forecasting and Analytical Services

A6 to M60 Relief Road

A6M ARR Forecasting Report
June 2017

| Rout e | Distanc e | AM Peak |  |  | Inter Peak |  |  | PM Peak |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Do-Minimum Time (minutes) | DoSomething Time (minutes) | Difference (minutes) | Do-Minimum Time (minutes) | DoSomething Time (minutes) | Difference (minutes) | Do-Minimum Time (minutes) | DoSomething Time (minutes) | Difference (minutes) |
| 1 | 25.325 | 56.8 | 53.3 | -3.5 | 48.9 | 45.2 | -3.7 | 53.4 | 50.0 | -3.4 |
|  | 25.306 | 50.8 | 52.1 | 1.3 | 44.4 | 46.3 | 1.9 | 50.4 | 48.3 | -2.1 |
| 2 | 16.353 | 20.6 | 20.6 | 0.0 | 19.8 | 19.8 | 0.0 | 20.3 | 20.2 | 0.0 |
|  | 16.353 | 20.2 | 20.2 | 0.0 | 19.8 | 19.8 | 0.0 | 20.2 | 20.2 | 0.0 |
| 3 | 10.196 | 14.1 | 14.1 | 0.0 | 12.6 | 12.6 | 0.0 | 14.1 | 14.0 | -0.1 |
|  | 10.196 | 13.4 | 13.4 | 0.0 | 12.5 | 12.5 | 0.0 | 14.0 | 14.0 | -0.1 |
| 4 | 6.575 | 6.9 | 6.9 | 0.0 | 6.5 | 6.5 | 0.0 | 6.8 | 6.8 | 0.0 |
|  | 6.575 | 6.8 | 6.8 | 0.0 | 6.4 | 6.4 | 0.0 | 6.8 | 6.8 | 0.0 |
| 5 | 7.653 | 7.7 | 7.4 | -0.3 | 6.4 | 6.4 | 0.0 | 8.2 | 7.8 | -0.4 |
|  | 6.632 | 7.2 | 7.2 | 0.0 | 5.7 | 5.7 | 0.1 | 7.0 | 7.1 | 0.1 |
| 6 | 9.92 | 15.5 | 15.5 | 0.0 | 13.9 | 14.0 | 0.0 | 15.8 | 15.8 | 0.0 |
|  | 8.155 | 13.3 | 13.1 | -0.2 | 11.5 | 11.5 | 0.0 | 13.7 | 13.7 | 0.0 |
| 7 | 7.872 | 7.4 | 7.3 | 0.0 | 5.5 | 5.5 | 0.0 | 7.3 | 7.3 | 0.0 |
|  | 5.312 | 4.7 | 4.7 | 0.0 | 3.7 | 3.7 | 0.0 | 7.0 | 7.1 | 0.1 |
| 8 | 6.457 | 9.9 | 9.9 | 0.0 | 8.2 | 8.2 | 0.0 | 10.2 | 9.8 | -0.4 |
|  | 6.457 | 10.3 | 10.3 | 0.0 | 8.4 | 8.4 | 0.0 | 9.9 | 9.9 | 0.0 |
| 9 | 14.281 | 21.5 | 20.0 | -1.6 | 16.0 | 15.9 | -0.1 | 22.0 | 20.5 | -1.5 |
|  | 13.541 | 21.1 | 20.0 | -1.2 | 15.0 | 15.1 | 0.1 | 20.4 | 18.6 | -1.7 |
| 10 | 10.126 | 18.8 | 19.8 | 1.1 | 16.4 | 16.2 | -0.2 | 19.3 | 18.7 | -0.6 |
|  | 10.098 | 17.9 | 18.2 | 0.4 | 15.6 | 15.6 | 0.0 | 17.0 | 17.6 | 0.5 |
| 11 | 10.578 | 18.3 | 18.2 | 0.0 | 16.1 | 16.0 | 0.0 | 18.4 | 18.2 | -0.1 |
|  | 12.589 | 21.0 | 20.6 | -0.4 | 18.4 | 18.4 | 0.0 | 21.7 | 21.5 | -0.2 |
| 12 | 22.394 | 32.9 | 32.9 | 0.0 | 29.5 | 29.5 | 0.1 | 32.7 | 32.6 | -0.1 |
|  | 22.299 | 32.7 | 32.7 | 0.0 | 29.6 | 29.5 | -0.1 | 38.9 | 38.3 | -0.6 |
| 13 | 17.043 | 16.6 | 16.3 | -0.3 | 13.9 | 13.8 | -0.2 | 16.7 | 16.7 | -0.1 |
|  | 17.817 | 16.4 | 16.5 | 0.1 | 13.8 | 13.8 | 0.0 | 15.3 | 15.6 | 0.3 |
| 14 | 5.173 | 13.8 | 12.8 | -1.0 | 10.1 | 10.0 | -0.1 | 12.1 | 12.1 | -0.1 |
|  | 5.173 | 11.8 | 11.5 | -0.3 | 10.6 | 10.5 | -0.2 | 12.3 | 12.1 | -0.1 |

ค Transport for
Greater Manchester

| 15 | 5.765 | 10.6 | 10.5 | -0.1 | 9.0 | 9.0 | 0.0 | 10.5 | 10.3 | -0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.765 | 11.0 | 10.8 | -0.2 | 9.4 | 9.4 | 0.0 | 11.1 | 11.0 | -0.2 |
| 16 | 5.968 | 7.6 | 7.6 | 0.0 | 7.6 | 7.6 | 0.0 | 7.7 | 7.6 | 0.0 |
|  | 5.968 | 7.5 | 7.6 | 0.0 | 7.5 | 7.5 | 0.0 | 7.5 | 7.5 | 0.0 |
| 17 | 16.538 | 20.7 | 20.7 | 0.0 | 20.3 | 20.3 | 0.1 | 20.8 | 20.7 | -0.1 |
|  | 16.538 | 20.8 | 21.1 | 0.4 | 20.0 | 20.0 | 0.0 | 20.3 | 20.1 | -0.1 |
| 18 | 4.579 | 7.6 | 7.7 | 0.0 | 7.5 | 7.5 | 0.0 | 7.5 | 7.6 | 0.0 |
|  | 4.579 | 7.4 | 7.4 | 0.0 | 7.3 | 7.3 | 0.0 | 7.4 | 7.4 | 0.0 |
| 19 | 9.671 | 13.1 | 13.5 | 0.4 | 13.1 | 13.2 | 0.1 | 13.2 | 13.5 | 0.3 |
|  | 9.671 | 12.9 | 13.2 | 0.3 | 12.9 | 13.1 | 0.2 | 13.0 | 13.3 | 0.3 |
| 20 | 8.934 | 13.9 | 13.9 | 0.1 | 12.6 | 12.6 | 0.0 | 14.1 | 14.2 | 0.1 |
|  | 8.927 | 14.5 | 14.9 | 0.4 | 13.2 | 13.7 | 0.5 | 15.3 | 16.0 | 0.7 |
| 21 | 7.345 | 12.8 | 13.0 | 0.2 | 12.0 | 12.4 | 0.4 | 12.2 | 12.7 | 0.5 |
|  | 7.345 | 12.2 | 12.2 | 0.0 | 11.7 | 11.7 | 0.0 | 11.7 | 11.8 | 0.0 |
| 22 | 2.007 | 6.5 | 5.5 | -1.0 | 5.0 | 4.7 | -0.3 | 5.2 | 5.1 | -0.1 |
|  | 2.035 | 5.8 | 5.6 | -0.2 | 4.9 | 4.8 | -0.1 | 5.8 | 5.4 | -0.4 |
| 23 | 5.071 | 13.8 | 12.9 | -0.9 | 12.2 | 12.0 | -0.1 | 14.6 | 14.0 | -0.6 |
|  | 5.071 | 12.8 | 13.4 | 0.5 | 10.9 | 11.1 | 0.2 | 13.1 | 12.4 | -0.8 |
| 24 | 4.012 | 9.9 | 10.1 | 0.3 | 8.5 | 8.9 | 0.4 | 11.3 | 9.3 | -2.0 |
|  | 3.968 | 10.6 | 9.8 | -0.7 | 7.5 | 7.4 | -0.1 | 9.2 | 8.7 | -0.5 |
| 25 | 3.898 | 7.2 | 7.3 | 0.1 | 6.6 | 6.4 | -0.1 | 7.9 | 7.5 | -0.4 |
|  | 3.922 | 6.6 | 6.7 | 0.2 | 5.7 | 5.7 | 0.0 | 6.3 | 6.6 | 0.3 |
| 26 | 6.485 | 13.9 | 13.6 | -0.3 | 12.5 | 12.0 | -0.5 | 13.9 | 13.3 | -0.6 |
|  | 6.485 | 14.9 | 13.4 | -1.5 | 12.0 | 11.5 | -0.5 | 13.5 | 12.9 | -0.6 |
| 27 | 8.729 | 13.2 | 13.3 | 0.1 | 11.8 | 11.8 | 0.0 | 13.3 | 13.3 | 0.0 |
|  | 8.729 | 14.3 | 14.0 | -0.3 | 12.4 | 12.5 | 0.1 | 14.2 | 13.8 | -0.4 |
| 28 | 4.886 | 9.5 | 9.8 | 0.3 | 7.0 | 7.0 | 0.0 | 7.7 | 7.7 | 0.0 |
|  | 4.886 | 7.8 | 7.8 | 0.0 | 6.9 | 6.9 | 0.0 | 7.8 | 7.7 | 0.0 |
| 29 | 6.267 | 10.3 | 10.5 | 0.2 | 9.5 | 9.9 | 0.4 | 11.1 | 11.0 | -0.1 |
|  | 6.267 | 9.7 | 9.6 | -0.1 | 9.0 | 9.1 | 0.1 | 10.1 | 10.5 | 0.4 |
| 30 | 6.739 | 16.8 | 16.4 | -0.4 | 13.1 | 13.2 | 0.1 | 16.3 | 15.3 | -1.0 |
|  | 7.124 | 20.0 | 18.7 | -1.3 | 15.5 | 15.0 | -0.5 | 20.8 | 19.2 | -1.6 |
| 31 | 5.82 | 11.3 | 10.6 | -0.7 | 9.8 | 9.5 | -0.3 | 10.8 | 10.3 | -0.5 |
|  | 5.82 | 10.9 | 10.3 | -0.6 | 9.8 | 9.5 | -0.3 | 11.3 | 10.5 | -0.8 |

ค Transport for Greater Manchester

| Route | Distance | AM Peak |  |  | Inter Peak |  |  | PM Peak |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Do- <br> Minimum Time (minutes) | DoSomething Time (minutes) | Difference <br> (minutes) | DoMinimum Time (minutes) | DoSomething Time (minutes) | Difference (minutes) | DoMinimum Time (minutes) | DoSomething Time (minutes) | Difference (minutes) |
| 1 | 25.3 | 64.3 | 60.8 | -3.6 | 48.8 | 46.0 | -2.8 | 64.6 | 63.2 | -1.4 |
|  | 25.3 | 52.8 | 53.9 | 1.1 | 46.5 | 47.3 | 0.7 | 53.7 | 50.6 | -3.1 |
| 2 | 16.4 | 21.0 | 21.0 | 0.0 | 19.8 | 19.8 | 0.0 | 20.7 | 20.7 | 0.0 |
|  | 16.4 | 20.4 | 20.4 | 0.0 | 19.9 | 19.9 | 0.0 | 20.6 | 20.6 | 0.0 |
| 3 | 10.2 | 14.4 | 14.4 | 0.0 | 12.7 | 12.8 | 0.0 | 14.6 | 14.6 | -0.1 |
|  | 10.2 | 13.8 | 13.8 | 0.0 | 12.6 | 12.6 | 0.0 | 14.6 | 14.6 | 0.0 |
| 4 | 6.6 | 6.9 | 6.9 | 0.0 | 6.5 | 6.5 | 0.0 | 6.9 | 6.9 | 0.0 |
|  | 6.6 | 6.8 | 6.8 | 0.0 | 6.4 | 6.4 | 0.0 | 6.8 | 6.8 | 0.0 |
| 5 | 7.7 | 9.3 | 8.8 | -0.5 | 6.8 | 6.7 | -0.1 | 9.3 | 8.8 | -0.5 |
|  | 6.6 | 7.9 | 8.0 | 0.1 | 6.0 | 5.9 | -0.1 | 7.6 | 7.8 | 0.2 |
| 6 | 9.9 | 18.0 | 16.8 | -1.3 | 14.2 | 14.2 | 0.0 | 16.6 | 16.4 | -0.3 |
|  | 8.2 | 14.0 | 13.5 | -0.5 | 11.6 | 11.6 | 0.0 | 14.8 | 14.5 | -0.3 |
| 7 | 7.9 | 8.8 | 8.7 | -0.1 | 6.0 | 5.9 | -0.1 | 8.4 | 8.4 | 0.1 |
|  | 5.3 | 5.2 | 5.2 | 0.0 | 4.2 | 4.1 | 0.0 | 8.0 | 8.0 | 0.0 |
| 8 | 6.5 | 10.5 | 10.3 | -0.2 | 8.3 | 8.3 | 0.0 | 10.7 | 10.4 | -0.3 |
|  | 6.5 | 10.7 | 10.7 | 0.0 | 8.6 | 8.6 | 0.0 | 10.1 | 10.0 | -0.1 |
| 9 | 14.3 | 26.5 | 23.2 | -3.3 | 17.8 | 16.2 | -1.6 | 26.0 | 22.8 | -3.2 |
|  | 13.5 | 25.9 | 23.6 | -2.3 | 16.5 | 15.7 | -0.8 | 25.1 | 20.0 | -5.1 |
| 10 | 10.1 | 20.5 | 20.8 | 0.4 | 16.7 | 16.8 | 0.2 | 20.9 | 20.7 | -0.2 |
|  | 10.1 | 19.7 | 19.4 | -0.3 | 15.7 | 15.6 | -0.1 | 19.5 | 19.3 | -0.3 |
| 11 | 10.6 | 18.6 | 18.3 | -0.3 | 16.4 | 16.5 | 0.2 | 19.2 | 18.7 | -0.5 |
|  | 12.6 | 21.6 | 21.4 | -0.2 | 18.5 | 18.8 | 0.3 | 22.2 | 22.4 | 0.2 |
| 12 | 22.4 | 33.8 | 33.6 | -0.2 | 29.6 | 29.6 | 0.0 | 34.8 | 33.7 | -1.0 |
|  | 22.3 | 34.5 | 34.0 | -0.5 | 29.9 | 30.0 | 0.0 | 41.4 | 40.8 | -0.7 |
| 13 | 17.0 | 18.4 | 18.4 | -0.1 | 15.8 | 15.5 | -0.3 | 20.1 | 19.8 | -0.2 |
|  | 17.8 | 18.4 | 18.2 | -0.1 | 15.6 | 15.3 | -0.2 | 16.9 | 17.1 | 0.2 |
| 14 | 5.2 | 15.0 | 13.7 | -1.3 | 10.4 | 10.2 | -0.1 | 13.1 | 12.3 | -0.8 |
|  | 5.2 | 12.5 | 11.8 | -0.7 | 10.8 | 10.9 | 0.0 | 13.2 | 12.4 | -0.8 |


| 15 | 5.8 | 10.8 | 10.7 | -0.1 | 9.1 | 9.0 | -0.1 | 10.8 | 10.6 | -0.3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.8 | 11.3 | 11.1 | -0.2 | 9.6 | 9.5 | -0.1 | 11.5 | 11.3 | -0.2 |
|  | 6.0 | 7.6 | 7.6 | 0.0 | 7.6 | 7.6 | 0.0 | 7.8 | 7.7 | 0.0 |
|  | 6.0 | 7.5 | 7.6 | 0.0 | 7.5 | 7.5 | 0.0 | 7.6 | 7.6 | 0.0 |
| 17 | 16.5 | 21.1 | 21.3 | 0.1 | 20.3 | 20.3 | 0.0 | 22.0 | 23.9 | 1.9 |
|  | 16.5 | 21.2 | 21.3 | 0.1 | 20.0 | 20.0 | 0.0 | 22.3 | 21.7 | -0.7 |
| 18 | 4.6 | 7.7 | 7.7 | 0.0 | 7.5 | 7.5 | 0.0 | 7.6 | 7.6 | 0.0 |
|  | 4.6 | 7.4 | 7.4 | 0.0 | 7.3 | 7.3 | 0.0 | 7.6 | 7.6 | 0.0 |
| 19 | 9.7 | 13.2 | 13.7 | 0.5 | 13.1 | 13.1 | 0.0 | 13.5 | 13.9 | 0.4 |
|  | 9.7 | 13.0 | 13.2 | 0.3 | 12.9 | 12.9 | 0.0 | 13.4 | 13.7 | 0.3 |
| 20 | 8.9 | 13.8 | 14.0 | 0.2 | 12.6 | 12.6 | 0.0 | 14.5 | 14.6 | 0.2 |
|  | 8.9 | 14.9 | 14.9 | 0.0 | 13.4 | 13.4 | 0.0 | 16.2 | 16.2 | 0.0 |
| 21 | 7.3 | 13.2 | 13.0 | -0.2 | 12.1 | 12.3 | 0.2 | 12.4 | 12.5 | 0.1 |
|  | 7.3 | 12.2 | 12.2 | 0.0 | 11.7 | 11.7 | 0.0 | 11.7 | 11.8 | 0.0 |
| 22 | 2.0 | 6.2 | 5.4 | -0.8 | 5.4 | 4.8 | -0.6 | 5.5 | 5.5 | 0.0 |
|  | 2.0 | 6.5 | 5.7 | -0.8 | 5.1 | 4.9 | -0.1 | 6.4 | 5.5 | -0.9 |
| 23 | 5.1 | 14.4 | 13.5 | -0.8 | 13.0 | 12.6 | -0.4 | 15.4 | 13.9 | -1.5 |
|  | 5.1 | 12.9 | 13.5 | 0.6 | 11.4 | 11.2 | -0.1 | 14.9 | 12.6 | -2.2 |
| 24 | 4.0 | 12.9 | 11.4 | -1.5 | 9.2 | 9.2 | 0.1 | 12.9 | 9.7 | -3.2 |
|  | 4.0 | 12.2 | 12.3 | 0.1 | 8.1 | 8.1 | 0.1 | 9.0 | 8.7 | -0.3 |
| 25 | 3.9 | 7.4 | 7.6 | 0.2 | 6.7 | 6.7 | 0.0 | 8.6 | 9.2 | 0.7 |
|  | 3.9 | 6.8 | 6.9 | 0.1 | 5.8 | 5.7 | 0.0 | 7.6 | 6.6 | -1.1 |
| 26 | 6.5 | 14.3 | 13.9 | -0.4 | 13.0 | 12.6 | -0.4 | 15.1 | 13.6 | -1.5 |
|  | 6.5 | 14.7 | 13.6 | -1.1 | 12.7 | 11.9 | -0.8 | 14.0 | 13.2 | -0.8 |
| 27 | 8.7 | 13.3 | 13.5 | 0.2 | 12.0 | 11.8 | -0.2 | 13.3 | 14.0 | 0.7 |
|  | 8.7 | 16.3 | 14.4 | -2.0 | 12.7 | 12.6 | -0.1 | 15.0 | 14.1 | -0.9 |
| 28 | 4.9 | 10.3 | 10.7 | 0.4 | 7.7 | 7.7 | 0.0 | 7.7 | 7.7 | 0.0 |
|  | 4.9 | 7.9 | 7.9 | 0.0 | 6.9 | 6.9 | 0.0 | 7.9 | 7.9 | -0.1 |
| 29 | 6.3 | 10.6 | 10.7 | 0.0 | 10.8 | 10.5 | -0.3 | 14.0 | 11.4 | -2.6 |
|  | 6.3 | 10.4 | 9.6 | -0.7 | 9.3 | 9.4 | 0.1 | 10.2 | 10.5 | 0.3 |
| 30 | 6.7 | 19.5 | 17.0 | -2.5 | 13.4 | 13.5 | 0.2 | 17.6 | 16.7 | -0.9 |
|  | 7.1 | 22.7 | 20.0 | -2.7 | 15.9 | 16.0 | 0.1 | 25.3 | 20.4 | -4.9 |
| 31 | 5.8 | 11.3 | 10.7 | -0.7 | 10.0 | 9.9 | -0.1 | 11.0 | 10.6 | -0.4 |
|  | 5.8 | 11.0 | 10.4 | -0.7 | 9.9 | 9.8 | -0.1 | 11.9 | 11.2 | -0.7 |

## 7. Conclusions

7.1 Transport for Greater Manchester (TfGM) has been appointed to undertake the traffic forecasting and economic appraisal of the preferred scheme option for A6 to M 60 Relief Road, in Stockport
7.2 The scheme improves access to / from M anchester Airport and its employment areas as well as Hazel Grove, Newby Road, Bramhall M oor Lane, Poynton and Stanley Green employment areas. Access to a number of regeneration areas is also improved by the scheme, including Stockport Town Centre M 60 Gateway, and Wythenshawe.
7.3 The proposed scheme consists of approximately 7.5 km of new dual 2 -lane and will include two new junctions and amendments to junctions at the A6 and at the M 6A560 roundabout at Bredbury as well as a new junction with the A6 at Stepping Hill.
7.4 Demand forecasts were derived using TEM PRO v7 and the development uncertainty logs provided by local authorities and other relevant organisations. Assumptions on population and employment growth used to derive the Core forecasts came from a variety of sources, namely :

- The relevant planning departments in High Peak, Cheshire East, M anchester, Stockport, Trafford for specific developments included in their Local Development Frameworks;
- Manchester Airport Group (MAG) for passenger and employee growth and development at and around $M$ anchester Airport;
- Local Development Framework datasets for developments elsewhere in Greater M anchester;
- The National Trip End Model (NTEM) dataset 6.2 forecasts; and
- The National Transport M odel forecasts (for freight traffic).
7.5 The methodology used to derive the Core forecasts involved:
- Application of NTEM adjusted TEM PRO growth by district to 2024 and 2039
- Addition of development growth in appropriate zone based on information provided by districts and utilising trip generation rates utilised for the A6M ARR scheme
- constraining the population and employment growth forecasts to the overall growth level implied by TEM PRO at the district level within Greater Manchester the pre-2009 district level for Cheshire East and at the county level elsewhere; and
7.6 The A6 to M 60 Relief Road SATURN model was cordoned to an identified Area of Influence (AOI) for the assessment of the proposed scheme. This 'Without Scheme' cordon model formed the base for the development of a 'With Scheme' scenario. The Do-Minimum and Do-something scenarios were assessed using a flat matrix / (i.e. without variable demand modelling)
7.7 The Core Scenario forecasts show that the proposed A6 to M 60 Relief Road provides significant additional network capacity and an improved route for trips travelling to and from M 60 J24 to Stockport and the surrounding areas. The scheme also provides relief to the A6 corridor through Stockport.
7.8 The proposed scheme provides time savings for travel in the Stockport area and this is most prominent during congested times of the day in 2039. The time savings are largely connected with the transfer of traffic from the A6 corridor and the M 60 to the proposed scheme.
7.9 The traffic forecasts demonstrate that the scheme would provide improved accessibility to the Stockport area, reduce levels of congestion on the network local to the scheme and as a result, it will help to promote economic regeneration.


[^0]:    ${ }^{1}$ GEH is an error statistic incorporating both relative and absolute errors. The form of the statistic is defined in Paragraph 7.9 of this report.

[^1]:    ${ }^{1}$ www.manchesterairport.co.uk/developmentplan
    ${ }^{2}$ UK Aviation Forecasts - Department for Transport - 2013
    ${ }^{3}$ Airports Commission - Final Report - July 2015

[^2]:    ${ }^{4}$ Economy \& Surface Access Plan - Manchester Airport 2015
    ${ }^{5}$ Land Use Plan - Manchester Airport 2015
    ${ }^{6}$ Manchester Core Strategy - Manchester City Council July 2012

[^3]:    Initial estimates are some $5 \%$ of employees that have switched from other modes to Metrolink

